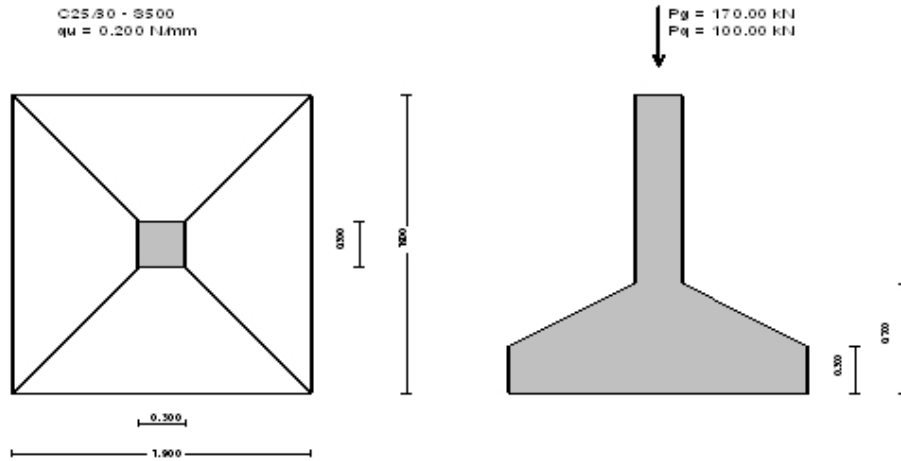


Example of footings

1. FOOTING-001

Symmetric footing with centric load

(EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002, EC7 EN1997-1-1:2004)



Concrete-Steel class: C25/30-S500
 Concrete cover : Cnom=75 mm
 Concrete weight : 25.0 kN/m³
 yc=1.50, ys=1.15

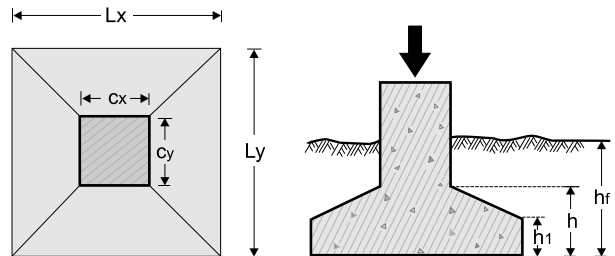
(EC2 §3)
 (EC2 §4.4.1)

(EC2 Table 2.1N)

1.1. Dimensions, materials, loads

Dimensions

Footing Lx= 1.900 m Ly= 1.900 m
 Column cx= 0.300 m cy= 0.300 m
 Heights h= 0.700 m h1= 0.300 m
 Depth of footing hf= 1.200 m
 Base area of footing A= 3.61 m²
 Volume of footing V= 1.65 m³



Materials of footing

Concrete-Steel class: C25/30-S500
 Concrete cover: Cnom=75 mm
 Effective depth of cross section d=h-d1, d1=Cnomc+(3/2)Ø=75+3x12/2=93mm, d=700-93=607mm

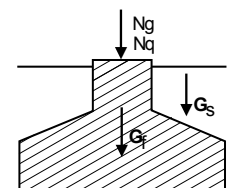
(EN1992-1-1, §3)
 (EC2 §4.4.1)

Soil

Soil bearing pressure qu= 0.200 N/mm² (MPa)
 Unit weight of soil γ=17.000 kN/m³

Loads

Self weight of footing [1.65x25.00] Gf= 41.25 kN
 Soil weight on footing [(3.61x 1.20- 1.65)x17.00] Gs= 45.59 kN
 Vertical permanent load Ng= 170.00 kN
 Vertical variable load Nq= 100.00 kN



1.2. Eurocode parameters

Check of soil bearing capacity (EC7 EN1997-1-1:2004, §6)
 Partial factors for actions and soil properties (EC7 Tables A.1-A.4, EC8-5 §3.1)
 Equilibrium limit state (EQU), Structural limit state (STR), Geotechnical limit state (GEO)

		(EQU)	(STR)	(GEO)
Actions	Permanent Unfavourable	γ_{Gdst} : 1.10	1.35	1.00
	Permanent Favourable	γ_{Gstb} : 0.90	1.00	1.00
	Variable Unfavourable	γ_{Qdst} : 1.50	1.50	1.30
	Variable Favourable	γ_{Qstb} : 0.00	0.00	0.00
Soil parameters	Angle of shearing resistance	γ_{ϕ} : 1.25	1.00	1.25
	Effective cohesion	γ_c : 1.25	1.00	1.25
	Undrained shear strength	γ_{cu} : 1.40	1.00	1.40
	Unconfined strength	γ_{qu} : 1.40	1.00	1.40
	Weight density	γ_w : 1.00	1.00	1.00

Partial safety factors for actions : $\gamma_G=1.35$, $\gamma_Q=1.50$ (EC0 Annex A1)
 Combination of accidental actions : (EC7) $\psi_2 = 0.30$
 Combination of accidental actions : (EC2) $\psi_2 = 0.30$

Design of reinforced concrete (EC2 EN1992-1-1:2004)

1.3. Check of soil bearing capacity (EC7 EN1997-1-1:2004, §6)

1.3.1. (EQU), 1.10xPermanent + 1.50xVariable (EC7 §2.4.7.2)

Design Loads

$N_{sd} = 1.10 \times 256.84 + 1.50 \times 100.00 = 432.52 \text{ kN}$

Soil pressure $q = 0.001 \times 432.52 / (1.900 \times 1.900) = 0.120 \text{ N/mm}^2 \text{ (Mpa)}$

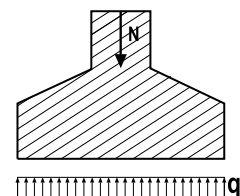
Check bearing resistance failure $V_d \leq R_d$

(EC7 EN1997-1-1:2004, §6.5.2)

Design effective foundation area $A = 1.900 \times 1.900 = 3.61 \text{ m}^2$

(EC7 Annex D)

Design bearing resistance of footing $R_d = 1000 \times 3.61 \times 0.200 / 1.40 = 515.71 \text{ kN} > V_d = 432.52 \text{ kN}$



1.3.2. (STR), 1.35xPermanent + 1.50xVariable

(EC7 §2.4.7.3)

Design Loads

$N_{sd} = 1.35 \times 256.84 + 1.50 \times 100.00 = 496.73 \text{ kN}$

Soil pressure $q = 0.001 \times 496.73 / (1.900 \times 1.900) = 0.138 \text{ N/mm}^2 \text{ (Mpa)}$

Check bearing resistance failure $V_d \leq R_d$

(EC7 EN1997-1-1:2004, §6.5.2)

Design effective foundation area $A = 1.900 \times 1.900 = 3.61 \text{ m}^2$

(EC7 Annex D)

Design bearing resistance of footing $R_d = 1000 \times 3.61 \times 1.00 = 722.00 \text{ kN} > V_d = 496.73 \text{ kN}$

1.3.3. (GEO), 1.00xPermanent + 1.30xVariable

(EC7 §2.4.7.3)

Design Loads

$N_{sd} = 1.00 \times 256.84 + 1.30 \times 100.00 = 386.84 \text{ kN}$

Soil pressure $q = 0.001 \times 386.84 / (1.900 \times 1.900) = 0.107 \text{ N/mm}^2 \text{ (Mpa)}$

Check bearing resistance failure $V_d \leq R_d$

(EC7 EN1997-1-1:2004, §6.5.2)

Design effective foundation area $A = 1.900 \times 1.900 = 3.61 \text{ m}^2$

(EC7 Annex D)

Design bearing resistance of footing $R_d = 1000 \times 3.61 \times 0.200 / 1.40 = 515.71 \text{ kN} > V_d = 386.84 \text{ kN}$

1.4. Internal actions for reinforced concrete design

1.4.1. Loading 1.35xPermanent + 1.50xVariable

Design Loads

$N_{sd} = 1.35 \times 170.00 + 1.50 \times 100.00 = 379.50 \text{ kN}$

1.5. Design for bending

(EC2 EN1992-1-1:2004, §6.1)

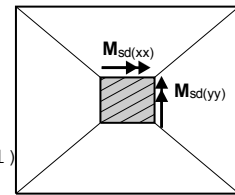
$$M_{sd}(yy) = 0.125 \times 379.50 \times 1.900 \times (1 - 0.300/1.900)^2 = 63.92 \text{ kNm}$$

$$M_{sd}(xx) = 0.125 \times 379.50 \times 1.900 \times (1 - 0.300/1.900)^2 = 63.92 \text{ kNm}$$

$$M_{sd} = 63.92 \text{ kNm}, b = 300 \text{ mm}, d = 607 \text{ mm}, K_d = 4.16, x/d = 0.07$$

$$e_c/e_s = 1.6/20.0, K_s = 2.36, \quad \mathbf{A_s = 2.49 \text{ cm}^2}$$

Minimum reinforcement $A_s \geq 0.26bd \cdot f_{ctm}/f_{yk}$ ($A_s = 5.74 \text{ cm}^2/\text{m}$) (EC2 §9.3.1)
 Minimum reinforcement $\emptyset 12/19.5$ ($5.79 \text{ cm}^2/\text{m}$)



$$M_{sd} = 63.92 \text{ kNm}, b = 300 \text{ mm}, d = 607 \text{ mm}, K_d = 4.16, x/d = 0.07$$

$$e_c/e_s = 1.6/20.0, K_s = 2.36, \quad \mathbf{A_s = 2.49 \text{ cm}^2}$$

Minimum reinforcement $A_s \geq 0.26bd \cdot f_{ctm}/f_{yk}$ ($A_s = 5.74 \text{ cm}^2/\text{m}$) (EC2 §9.3.1)
 Minimum reinforcement $\emptyset 12/19.5$ ($5.79 \text{ cm}^2/\text{m}$)

Reinforcement of footing

Steel reinforcement in x-x direction: $\emptyset 12/19.5$ ($5.79 \text{ cm}^2/\text{m}$), **11 $\emptyset 12$** (12.43 cm^2)

Steel reinforcement in y-y direction: $\emptyset 12/19.5$ ($5.79 \text{ cm}^2/\text{m}$), **11 $\emptyset 12$** (12.43 cm^2)

1.6. Design for shear

(EC2 EN1992-1-1:2004, §6.2)

The design for shear is covered by the design in punching shear because the critical rupture surface is considered at angle 45°

1.7. Design for punching shear

(EC2 EN1992-1-1:2004, §6.4)

Footing cantilevers in x-x, $L_1 = 0.800 > d = 0.607 \text{ m}$, $L_2 = 0.800 > d = 0.607 \text{ m}$
 Footing cantilevers in y-y, $L_1 = 0.800 > d = 0.607 \text{ m}$, $L_2 = 0.800 > d = 0.607 \text{ m}$

Control perimeter, at $1.0d = 0.607 \text{ m} < 2.0d$ (EC2 §6.4.2.2)

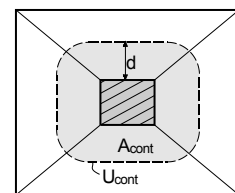
we consider rupture surface at angle 45°

$$U_{cont} = (0.300 + 0.300 + 0.300 + 0.300) + 3.14 \times (0.607 + 0.607) = 5.012 \text{ m}$$

Base area within the control perimeter

$$A_{cont} = 0.300 \times 0.300 + 0.300 \times 1.214 + 0.300 \times 1.214 + 3.14 \times 0.607 \times 0.607 = 1.98 \text{ m}^2$$

Minimum effective height of footing at control section $d_m = 303 \text{ mm}$



Applied shear force at control perimeter $V_{ed} = N_{sd} - \sigma \cdot A_{cont}$, $v_{ed} = V_{ed} \cdot \beta / U_{cont}$

$$\sigma = 379.50 / (1.900 \times 1.900) = 105.12 \text{ kN/m}^2, \quad \beta = 1.15$$

(EC2 §6.4.3 Fig.6.21N)

$$v_{ed} = (379.50 - 105.12 \times 1.98) \times 1.15 / 5.012 = 39.32 \text{ kN/m}$$

Tension reinforcement at control section $A_{sxx} = 5.79 \text{ cm}^2/\text{m}$, $A_{syy} = 5.79 \text{ cm}^2/\text{m}$

$$A_{s1^2} = (A_{sxx}) (A_{syy}) = 5.79 \times 5.79, \quad A_{s1} = 5.79 \text{ cm}^2$$

Punching shear capacity without shear reinforcement V_{rdc}

(EC2 §6.4.4)

$$V_{rdc} = [C_{rdc} \cdot k \cdot (100 \rho_1 \cdot f_{ck})^{(0.333)} \cdot (2d/a)] \cdot b_w \cdot d \quad (\text{EC2 Eq.6.50})$$

$$V_{rdc} \geq [v_{min} \cdot 2d/a] \cdot b_w \cdot d, \quad d = d_m = 303 \text{ mm}, \quad a = 607 \text{ mm}$$

$$C_{rdc} = 0.18 / \gamma_c = 0.18 / 1.50 = 0.120, \quad f_{ck} = 25.00 \text{ MPa}$$

$$k = 1 + (200/d)^{1/2} \leq 2, \quad k = 1.81$$

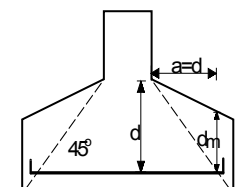
$$\rho_1 = A_{s1} / (b_w \cdot d) = 579 / (1000 \times 303) = 0.0019$$

$$v_{min} = 0.035 \cdot k^{(1.50)} \cdot f_{ck}^{1/2} = 0.43 \text{ N/mm}^2 \quad (\text{EC2 Eq.6.3N})$$

$$V_{rd,c}(\text{min}) = 0.001 \times (0.43 \times 2 \times 303 / 607) \times 1000 \times 303 = 130.08 \text{ kN/m}$$

$$V_{rdc} = 0.001 \times [0.120 \times 1.81 \times (0.19 \times 25.00)^{(0.333)} \times 2 \times 303 / 607] \times 1000 \times 303 = 110.45, \quad V_{rdc} = V_{rdc}(\text{min}) = 130.08 \text{ kN/m}$$

$V_{sd} = 39.32 \text{ kN/m} \leq V_{rdc} = 130.08 \text{ kN/m}$, shear and punching shear OK



1.8. Reinforcement anchorage

(EC2 EN1992-1-1:2004, §9.8.2.2, §8.4)

$x=h/2=0.150m$, $R=1000 \times 0.138 \times 0.150 \times 1.900=39.33 \text{ kN}$
 $e=0.15b=0.045m$ $z_e=0.770 \text{ m}$, $z_i=0.900d=0.546m$
 $F_s=R \cdot z_e/z_i=39.33 \times 0.770/0.546=55.43 \text{ kN}$
 $\sigma_{sd}=F_s/A_s=1000 \times 55.43/1243=45 \text{ MPa}$

Basic required anchorage length (EC2 Eq.8.3)

$l_{b,rqd}=(\Phi/4)(\sigma_{sd}/f_{bd})=(12/4) \times (45/2.70)=50mm$

$f_{bd}=2.25 \times 1.00 \times (f_{ctk}0.05/\gamma_c)=2.70 \text{ MPa}$ (EC2 §8.4.2)

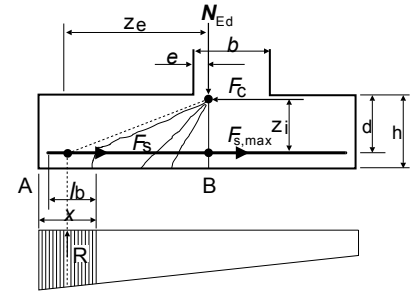
Design anchorage length (EC2 §8.4.4, T.8.2)

$l_{bd}=0.70 \times 50=35mm$, $C_{nom}=75mm > 3\Phi=36mm$

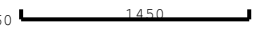
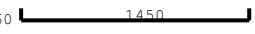
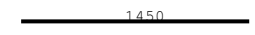
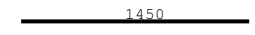
Minimum anchorage length $l_{b,min}=\max(0.30l_{b,rqd}, 10\Phi, 100mm)=120mm$

Necessary anchorage length of longitudinal reinforcement $L_{bd}=120mm =0.120m$

$l_{bd}=120mm > (x-C_{nom})=75.00$. Necessary bends 60mm at bar ends for anchorage

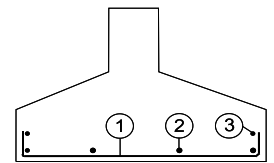


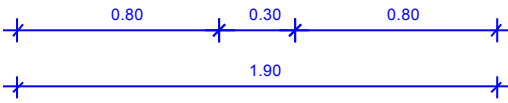
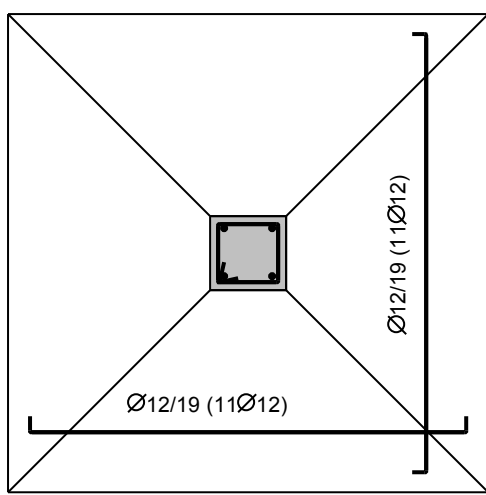
1.9. Reinforcing bar schedule

Num	type	reinforcing bar [mm]	items	∅	g/m [kg/m]	length [m]	weight [kg]
1	①	60  60	7	12	0.888	1.570	9.76
2	②	60  60	7	12	0.888	1.570	9.76
3	③		2	8	0.395	1.450	1.15
4	③		2	8	0.395	1.450	1.15

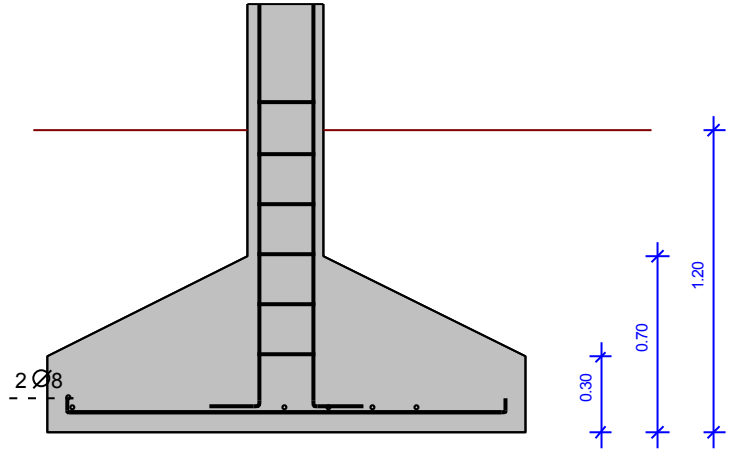
Total weight [kg]

21.82





Ng=170.00 kN
Nq=100.00 kN



Soil bearing pressure: 0.20 [N/mm²]

General information

Symmetric footing with centric load
Concrete and steel class: C25/30 - S500
Concrete cover: C_{nom}=75 mm
Soil bearing pressure: 0.20 [N/mm²]

Design codes

Eurocode 0 EN1991-1-1, Basis of structural design
Eurocode 1 EN1991-1-1, Actions on structures
Eurocode 2 EN1992-1-1, Design of concrete structures
Eurocode 7 EN1997-1-1, Geotechnical design
Eurocode 8 EN1998-5, Earthquake design

Loads

Dead load Ng=170.00 kN
Live load Nq=100.00 kN

Reinforcing bar schedule

#		reinforcing bar [mm]	items	∅ [mm]	g/m [kg/m]	length [m]	weight [kg]
1	F1	60 1750 60	11	12	0.888	1.870	18.27
2	F2	60 1750 60	11	12	0.888	1.870	18.27
3	F3	1750	2	8	0.395	1.750	1.38
4	F3	1750	2	8	0.395	1.750	1.38

Total weight [kg]

39.30

Concrete volume of footing V= 1.65 [m³]
Reinforcement weight G=39.30 [kg]

Project: Example of footings

FOOTING-001

Scale : 1:30

Date: 12/03/2007

Designer:

Draw.No.:

Filename: Example of footings

Sign:

RUNET Norway as

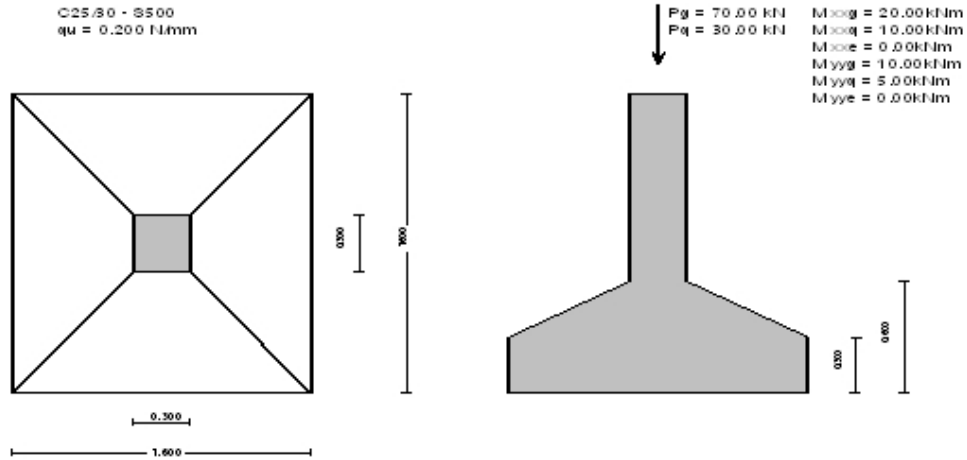
BETONexpress

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2. FOOTING-003

Symmetric footing with eccentric load

(EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002, EC7 EN1997-1-1:2004)



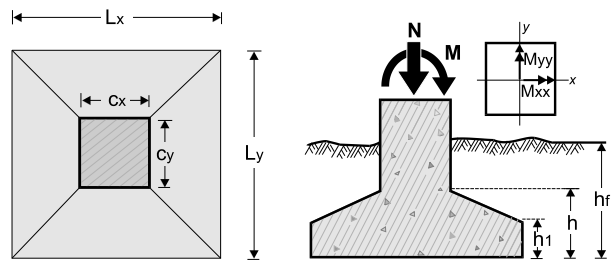
Concrete-Steel class: C25/30-S500
 Concrete cover : Cnom=75 mm
 Concrete weight : 25.0 kN/m³
 γc=1.50, γs=1.15

(EC2 §3)
 (EC2 §4.4.1)
 (EC2 Table 2.1N)

2.1. Dimensions, materials, loads

Dimensions

Footing Lx= 1.600 m Ly= 1.600 m
 Column cx= 0.300 m cy= 0.300 m
 Heights h= 0.600 m h1= 0.300 m
 Depth of footing hf= 1.200 m
 Base area of footing A= 2.56 m²
 Volume of footing V= 1.08 m³



Materials of footing

Concrete-Steel class: C25/30-S500
 Concrete cover: Cnom=75 mm
 Effective depth of cross section d=h-d1, d1=Cnom+(3/2)∅=75+3x12/2=93mm, d=600-93=507mm

(EN1992-1-1, §3)
 (EC2 §4.4.1)

Soil

Soil bearing pressure qu= 0.200 N/mm² (MPa)
 Unit weight of soil γ=17.000 kN/m³

Loads

		permanent	variable
Self weight	kN	[1.08x25.00]	27.00
Soil weight	kN	[(2.56x 1.20- 1.08)x17.00]	33.86
Vertical load	kN		70.00 30.00
Moment Mxx	kNm		20.00 10.00
Moment Myy	kNm		10.00 5.00

2.2. Eurocode parameters

Check of soil bearing capacity (EC7 EN1997-1-1:2004, §6)
 Partial factors for actions and soil properties (EC7 Tables A.1-A.4, EC8-5 §3.1)
 Equilibrium limit state (EQU), Structural limit state (STR), Geotechnical limit state (GEO)

		(EQU)	(STR)	(GEO)
Actions	Permanent Unfavourable	γ_{Gdst} : 1.10	1.35	1.00
	Permanent Favourable	γ_{Gstb} : 0.90	1.00	1.00
	Variable Unfavourable	γ_{Qdst} : 1.50	1.50	1.30
	Variable Favourable	γ_{Qstb} : 0.00	0.00	0.00
Soil parameters	Angle of shearing resistance	γ_{ϕ} : 1.25	1.00	1.25
	Effective cohesion	γ_c : 1.25	1.00	1.25
	Undrained shear strength	γ_{cu} : 1.40	1.00	1.40
	Unconfined strength	γ_{qu} : 1.40	1.00	1.40
	Weight density	γ_w : 1.00	1.00	1.00

Partial safety factors for actions : $\gamma_G=1.35$, $\gamma_Q=1.50$ (EC0 Annex A1)
 Combination of accidental actions : (EC7) $\psi_2 = 0.30$
 Combination of accidental actions : (EC2) $\psi_2 = 0.30$

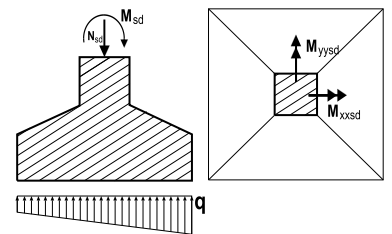
Design of reinforced concrete (EC2 EN1992-1-1:2004)

2.3. Check of soil bearing capacity (EC7 EN1997-1-1:2004, §6)

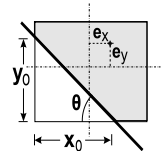
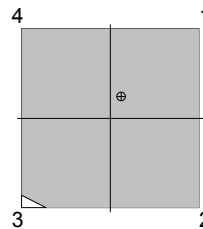
2.3.1. (EQU), 1.10xPermanent + 1.50xVariable (EC7 §2.4.7.2)

Design Loads

$N_{sd} = 1.10 \times 130.86 + 1.50 \times 30.00 = 188.95$ kN
 $M_{xxsd} = 1.10 \times 20.00 + 1.50 \times 10.00 = 37.00$ kNm
 $M_{yysd} = 1.10 \times 10.00 + 1.50 \times 5.00 = 18.50$ kNm



Eccentricities, soil pressures, footing area
 relative eccentricity $e_x/L_x = M_{yy} / (N \cdot L_x) = 0.061$
 relative eccentricity $e_y/L_y = M_{xx} / (N \cdot L_y) = 0.122$
 soil pressure $q_1 = 0.155$ N/mm²
 soil pressure $q_2 = 0.047$ N/mm²
 soil pressure $q_3 = 0.000$ N/mm²
 soil pressure $q_4 = 0.101$ N/mm²
 zero pressure line $x_0 = 0.22$ m, $y_0 = 0.11$ m, $\theta = 27^\circ$
 effective footing area 99.51%



Check bearing resistance failure $V_d \leq R_d$ (EC7 EN1997-1-1:2004, §6.5.2)

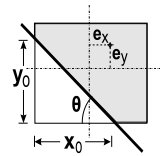
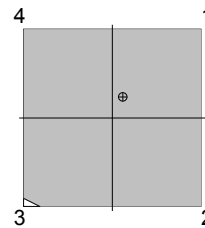
relative load eccentricities $e_x/L_x = M_{yy} / (N \cdot L_x) = 0.061$, $e_y/L_y = M_{xx} / (N \cdot L_y) = 0.122$
 relative load eccentricities ≤ 0.333 (EC7 §6.5.4)
 effective design length of footing $L' = 1.600 \times (1 - 2 \times 0.061) = 1.405$ m (EC7 Annex D)
 effective design width of footing $B' = 1.600 \times (1 - 2 \times 0.122) = 1.210$ m
 effective design area of footing $L' \cdot B' = 1.405 \times 1.210 = 1.70$ m²
 Design bearing resistance of footing $R_d = 1000 \times 1.70 \times 0.200 / 1.40 = 242.86$ kN $> V_d = 188.95$ kN
 Effective footing area 99.51% $> 50.00\%$ (EC7 §6.5.4)

2.3.2. (STR), 1.35xPermanent + 1.50xVariable (EC7 §2.4.7.3)

Design Loads

$N_{sd} = 1.35 \times 130.86 + 1.50 \times 30.00 = 221.66$ kN
 $M_{xxsd} = 1.35 \times 20.00 + 1.50 \times 10.00 = 42.00$ kNm
 $M_{yysd} = 1.35 \times 10.00 + 1.50 \times 5.00 = 21.00$ kNm

Eccentricities, soil pressures, footing area
 relative eccentricity $e_x/L_x = M_{yy}/(N \cdot L_x) = 0.059$
 relative eccentricity $e_y/L_y = M_{xx}/(N \cdot L_y) = 0.118$
 soil pressure $q_1 = 0.179 \text{ N/mm}^2$
 soil pressure $q_2 = 0.056 \text{ N/mm}^2$
 soil pressure $q_3 = 0.000 \text{ N/mm}^2$
 soil pressure $q_4 = 0.117 \text{ N/mm}^2$
 zero pressure line $x_0 = 0.15\text{m}$, $y_0 = 0.07\text{m}$, $\theta = 27^\circ$
 effective footing area 99.80%

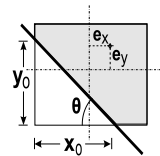
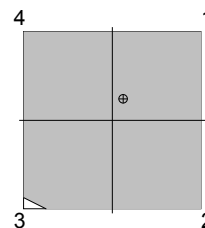


Check bearing resistance failure $V_d \leq R_d$ (EC7 EN1997-1-1:2004, §6.5.2)
 relative load eccentricities $e_x/L_x = M_{yy}/(N \cdot L_x) = 0.059$, $e_y/L_y = M_{xx}/(N \cdot L_y) = 0.118$
 relative load eccentricities ≤ 0.333 (EC7 §6.5.4)
 effective design length of footing $L' = 1.600 \times (1 - 2 \times 0.059) = 1.411 \text{ m}$ (EC7 Annex D)
 effective design width of footing $B' = 1.600 \times (1 - 2 \times 0.118) = 1.222 \text{ m}$
 effective design area of footing $L'B' = 1.411 \times 1.222 = 1.72 \text{ m}^2$
 Design bearing resistance of footing $R_d = 1000 \times 1.72 \times 0.200 / 1.00 = 344.00 \text{ kN} > V_d = 221.66 \text{ kN}$
 Effective footing area 99.80% > 50.00% (EC7 §6.5.4)

2.3.3. (GEO), 1.00xPermanent + 1.30xVariable (EC7 §2.4.7.3)

Design Loads
 $N_{sd} = 1.00 \times 130.86 + 1.30 \times 30.00 = 169.86 \text{ kN}$
 $M_{xxsd} = 1.00 \times 20.00 + 1.30 \times 10.00 = 33.00 \text{ kNm}$
 $M_{yyd} = 1.00 \times 10.00 + 1.30 \times 5.00 = 16.50 \text{ kNm}$

Eccentricities, soil pressures, footing area
 relative eccentricity $e_x/L_x = M_{yy}/(N \cdot L_x) = 0.061$
 relative eccentricity $e_y/L_y = M_{xx}/(N \cdot L_y) = 0.121$
 soil pressure $q_1 = 0.139 \text{ N/mm}^2$
 soil pressure $q_2 = 0.042 \text{ N/mm}^2$
 soil pressure $q_3 = 0.000 \text{ N/mm}^2$
 soil pressure $q_4 = 0.090 \text{ N/mm}^2$
 zero pressure line $x_0 = 0.21\text{m}$, $y_0 = 0.10\text{m}$, $\theta = 27^\circ$
 effective footing area 99.58%



Check bearing resistance failure $V_d \leq R_d$ (EC7 EN1997-1-1:2004, §6.5.2)
 relative load eccentricities $e_x/L_x = M_{yy}/(N \cdot L_x) = 0.061$, $e_y/L_y = M_{xx}/(N \cdot L_y) = 0.121$
 relative load eccentricities ≤ 0.333 (EC7 §6.5.4)
 effective design length of footing $L' = 1.600 \times (1 - 2 \times 0.061) = 1.405 \text{ m}$ (EC7 Annex D)
 effective design width of footing $B' = 1.600 \times (1 - 2 \times 0.121) = 1.213 \text{ m}$
 effective design area of footing $L'B' = 1.405 \times 1.213 = 1.70 \text{ m}^2$
 Design bearing resistance of footing $R_d = 1000 \times 1.70 \times 0.200 / 1.40 = 242.86 \text{ kN} > V_d = 169.86 \text{ kN}$
 Effective footing area 99.58% > 50.00% (EC7 §6.5.4)

2.4. Internal actions for reinforced concrete design

Moments M and shearing forces V , are computed at column faces.
 Shearing forces V^* are computed at distance $d = 0.507\text{m}$ from the column face.
 They are computed, by numerical integration of the soil pressure under the footing.

2.4.1. Loading 1.35xPermanent + 1.50xVariable

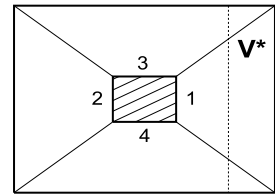
Design Loads
 $N_{sd} = 1.35 \times 130.86 + 1.50 \times 30.00 = 221.66 \text{ kN}$
 $M_{xxsd} = 1.35 \times 20.00 + 1.50 \times 10.00 = 42.00 \text{ kNm}$
 $M_{yyd} = 1.35 \times 10.00 + 1.50 \times 5.00 = 21.00 \text{ kNm}$

Eccentricities, soil pressures, footing area

relative load eccentricities $e_x/L_x=M_{yy}/(N \cdot L_x)=0.059$, $e_y/L_y=M_{xx}/(N \cdot L_y)=0.118$
 soil pressures $q_1=0.179$, $q_2=0.056$, $q_3=0.000$, $q_4=0.117 \text{ N/mm}^2$
 zero pressure line $x_0=0.15\text{m}$, $y_0=0.07\text{m}$, $\theta=27^\circ$
 pressure due to self weight+soil weight $q_g=0.001 \times 1.35 \times (27.00+33.86)/2.56=0.032 \text{ N/mm}^2$
 Shear at critical section + (self weight+soil weight) $q \cdot A_{cont}+q_g \cdot A=165.24 \text{ kN}$

Internal actions (bending moments, shearing forces)

$M_{yy}(1)= 25.99 \text{ kNm}$, $V(1)= 76.23 \text{ kN}$, $V^*(1)= 19.00 \text{ kN}$
 $M_{yy}(2)= 12.07 \text{ kNm}$, $V(2)= 41.05 \text{ kN}$, $V^*(2)= 7.25 \text{ kN}$
 $M_{xx}(3)= 33.57 \text{ kNm}$, $V(3)= 95.28 \text{ kN}$, $V^*(3)= 25.45 \text{ kN}$
 $M_{xx}(4)= 4.85 \text{ kNm}$, $V(4)= 22.12 \text{ kN}$, $V^*(4)= 1.62 \text{ kN}$

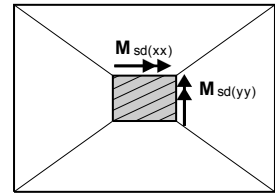


2.5. Design for bending

(EC2 EN1992-1-1:2004, §6.1)

Maximum design moments

$M_{sd}(yy)= 25.99 \text{ kNm}$, $b= 300 \text{ mm}$, $d= 507 \text{ mm}$
 $M_{sd}(xx)= 33.57 \text{ kNm}$, $b= 300 \text{ mm}$, $d= 507 \text{ mm}$



$M_{sd}=25.99\text{kNm}$, $b=300\text{mm}$, $d=507\text{mm}$, $K_d=5.45$, $x/d=0.05$
 $e_c/e_s=1.1/20.0$, $K_s=2.34$, **$A_s= 1.20\text{cm}^2$**

Minimum reinforcement $A_s \geq 0.26bd \cdot f_{ctm}/f_{yk}$ ($A_s= 4.11\text{cm}^2/\text{m}$) (EC2 §9.3.1)
 Minimum reinforcement $\emptyset 12/27.5$ ($4.11\text{cm}^2/\text{m}$)

$M_{sd}=33.57\text{kNm}$, $b=300\text{mm}$, $d=507\text{mm}$, $K_d=4.79$, $x/d=0.06$
 $e_c/e_s=1.3/20.0$, $K_s=2.35$, **$A_s= 1.56\text{cm}^2$**

Minimum reinforcement $A_s \geq 0.26bd \cdot f_{ctm}/f_{yk}$ ($A_s= 4.11\text{cm}^2/\text{m}$) (EC2 §9.3.1)
 Minimum reinforcement $\emptyset 12/27.5$ ($4.11\text{cm}^2/\text{m}$)

Reinforcement of footing

Steel reinforcement in x-x direction: $\emptyset 12/27.5$ ($4.11\text{cm}^2/\text{m}$), **$7\emptyset 12$ (7.91cm^2)**

Steel reinforcement in y-y direction: $\emptyset 12/27.5$ ($4.11\text{cm}^2/\text{m}$), **$7\emptyset 12$ (7.91cm^2)**

2.6. Design for shear

(EC2 EN1992-1-1:2004, §6.2)

The design for shear is covered by the design in punching shear because the critical rupture surface is considered at angle 45°

2.7. Design for punching shear

(EC2 EN1992-1-1:2004, §6.4)

Footing cantilevers in x-x, $L_1=0.650>d=0.507\text{m}$, $L_2=0.650>d=0.507\text{m}$
 Footing cantilevers in y-y, $L_1=0.650>d=0.507\text{m}$, $L_2=0.650>d=0.507\text{m}$

Control perimeter, at $1.0d=0.507\text{m}<2.0d$ (EC2 §6.4.2.2)

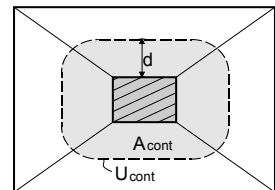
we consider rupture surface at angle 45°

$U_{cont}=(0.300+0.300+0.300+0.300)+3.14 \times (0.507+0.507)=4.384\text{m}$

Base area within the control perimeter

$A_{cont}=0.300 \times 0.300+0.300 \times 1.014+0.300 \times 1.014+3.14 \times 0.507 \times 0.507=1.51\text{m}^2$

Minimum effective height of footing at control section $d_m= 273\text{mm}$



Applied shear force at control perimeter $V_{ed}=N_{sd}-\sigma \cdot A_{cont}$, $ved=V_{ed} \cdot \beta/U_{cont}$

$ved=(221.66-165.24) \times 1.50/4.38=19.31 \text{ kN/m}$, $\beta=1.50$

(EC2 §6.4.3 Fig.6.21N)

Tension reinforcement at control section $A_{sxx}= 4.11\text{cm}^2/\text{m}$, $A_{syy}= 4.11\text{cm}^2/\text{m}$

$A_{s1^2}=(A_{sxx})(A_{syy})=4.11 \times 4.11$, $A_{s1}=4.11 \text{ cm}^2$

Punching shear capacity without shear reinforcement V_{rdc}

(EC2 §6.4.4)

$$V_{rdc} = [C_{rdc} \cdot k \cdot (100 \rho_1 \cdot f_{ck})^{0.333} \cdot (2d/a)] \cdot b_w \cdot d \quad (EC2 \text{ Eq.6.50})$$

$$V_{rdc} >= [v_{min} \cdot 2d/a] \cdot b_w \cdot d, \quad d = d_m = 273 \text{ mm}, \quad a = 507 \text{ mm}$$

$$C_{rdc} = 0.18 / \gamma_c = 0.18 / 1.50 = 0.120, \quad f_{ck} = 25.00 \text{ MPa}$$

$$k = 1 + (200/d)^{1/2} \leq 2, \quad k = 1.86$$

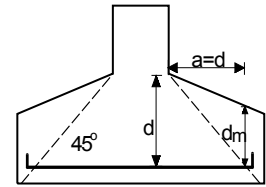
$$\rho_1 = A_{s1} / (b_w \cdot d) = 411 / (1000 \times 273) = 0.0015$$

$$v_{min} = 0.035 \cdot k^{1.50} \cdot f_{ck}^{1/2} = 0.44 \text{ N/mm}^2 \quad (EC2 \text{ Eq.6.3N})$$

$$V_{rd,c(\min)} = 0.0015 \times (0.44 \times 2 \times 273 / 507) \times 1000 \times 273 = 129.36 \text{ kN/m}$$

$$V_{rdc} = 0.0015 \times [0.120 \times 1.86 \times (0.15 \times 25.00)^{0.333} \times 2 \times 273 / 507] \times 1000 \times 273 = 101.95, \quad V_{rdc} = V_{rdc(\min)} = 129.36 \text{ kN/m}$$

$$V_{sd} = 19.31 \text{ kN/m} \leq V_{rdc} = 129.36 \text{ kN/m}, \text{ shear and punching shear OK}$$



2.8. Reinforcement anchorage

(EC2 EN1992-1-1:2004, §9.8.2.2, §8.4)

$$x = h/2 = 0.150 \text{ m}, \quad R = 1000 \times 0.179 \times 0.150 \times 1.600 = 42.93 \text{ kN}$$

$$e = 0.15b = 0.045 \text{ m}, \quad z_e = 0.620 \text{ m}, \quad z_i = 0.900d = 0.456 \text{ m}$$

$$F_s = R \cdot z_e / z_i = 42.93 \times 0.620 / 0.456 = 58.33 \text{ kN}$$

$$\sigma_{sd} = F_s / A_s = 1000 \times 58.33 / 791 = 74 \text{ MPa}$$

Basic required anchorage length (EC2 Eq.8.3)

$$l_{b,rqd} = (\Phi/4) (\sigma_{sd} / f_{bd}) = (12/4) \times (74 / 2.70) = 82 \text{ mm}$$

$$f_{bd} = 2.25 \times 1.00 \times (f_{ctk} 0.05 / \gamma_c) = 2.70 \text{ MPa} \quad (EC2 §8.4.2)$$

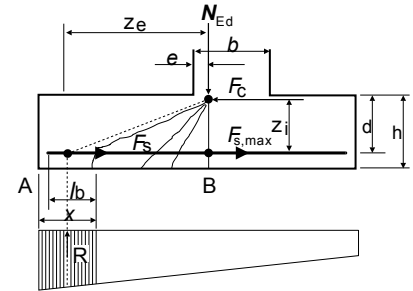
Design anchorage length (EC2 §8.4.4, T.8.2)

$$l_{bd} = 0.70 \times 82 = 58 \text{ mm}, \quad C_{nom} = 75 \text{ mm} > 3\Phi = 36 \text{ mm}$$

Minimum anchorage length $l_{b,min} = \max(0.30 l_{b,rqd}, 10\Phi, 100 \text{ mm}) = 120 \text{ mm}$

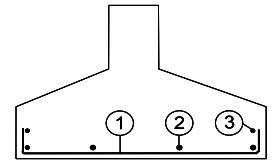
Necessary anchorage length of longitudinal reinforcement $l_{bd} = 120 \text{ mm} = 0.120 \text{ m}$

$$l_{bd} = 120 \text{ mm} > (x - C_{nom}) = 75.00. \text{ Necessary bends } 60 \text{ mm at bar ends for anchorage}$$

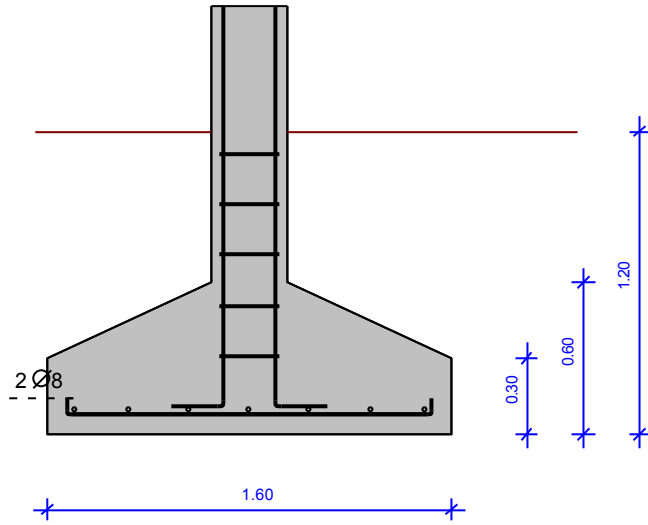
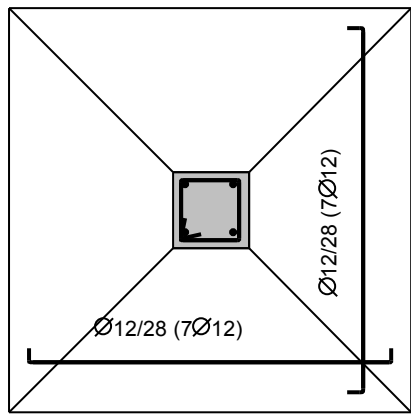


2.9. Reinforcing bar schedule

Num	type	reinforcing bar [mm]	items	∅	g/m [kg/m]	length [m]	weight [kg]
5	①	60 ┌────────── 1450 ─────────┐ 60	7	12	0.888	1.570	9.76
6	②	60 ┌────────── 1450 ─────────┐ 60	7	12	0.888	1.570	9.76
7	③	────────── 1450 ─────────	2	8	0.395	1.450	1.15
8	③	────────── 1450 ─────────	2	8	0.395	1.450	1.15
Total weight [kg]							21.82



	Dead	Live	Seismic
N [kN]	70.00	30.00	0.00
Mxx [kNm]	20.00	10.00	0.00
Myy [kNm]	10.00	5.00	0.00



General information

Symmetric footing with eccentric load
 Concrete and steel class: C25/30 - S500
 Concrete cover: $C_{nom}=75$ mm
 Soil bearing pressure: 0.20 [N/mm²]

Design codes

Eurocode 0 EN1991-1-1, Basis of structural design
 Eurocode 1 EN1991-1-1, Actions on structures
 Eurocode 2 EN1992-1-1, Design of concrete structures
 Eurocode 7 EN1997-1-1, Geotechnical design
 Eurocode 8 EN1998-5, Earthquake design

Loads

	Dead	Live	Seismic
N [kN]	70.00	30.00	0.00
Mxx [kNm]	20.00	10.00	0.00
Myy [kNm]	10.00	5.00	0.00

Reinforcing bar schedule

#		reinforcing bar [mm]	items	∅ [mm]	g/m [kg/m]	length [m]	weight [kg]
1	F1	60 60	7	12	0.888	1.570	9.76
2	F2	60 60	7	12	0.888	1.570	9.76
3	F3	1450	2	8	0.395	1.450	1.15
4	F3	1450	2	8	0.395	1.450	1.15

Total weight [kg]

21.82

Concrete volume of footing $V= 1.08$ [m³]
 Reinforcement weight $G=21.82$ [kg]

Project: Example of footings 12/03/2007

FOOTING-003

Scale : 1:30

Date: 12/03/2007

Designer:

Draw.No.:

Filename: Example of footings

Sign:

RUNET Norway as

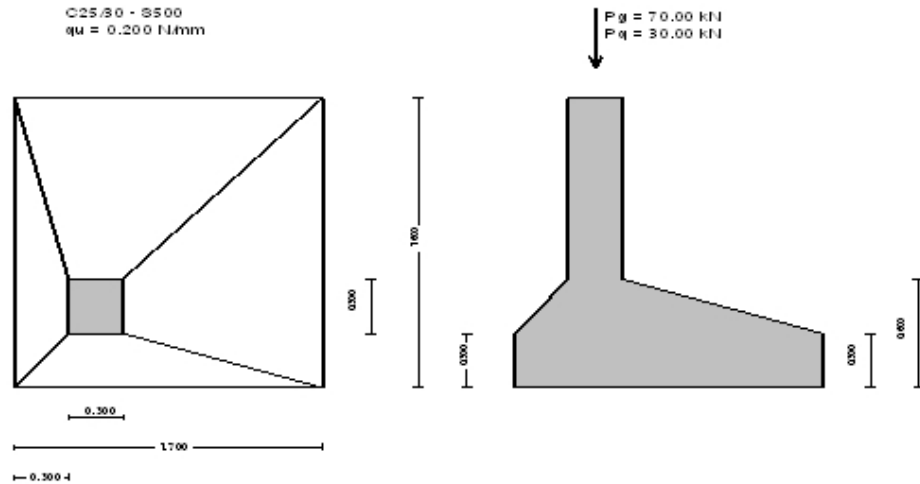
BETONexpress

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3. FOOTING-005

Asymmetric footing with eccentric load

(EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002, EC7 EN1997-1-1:2004)



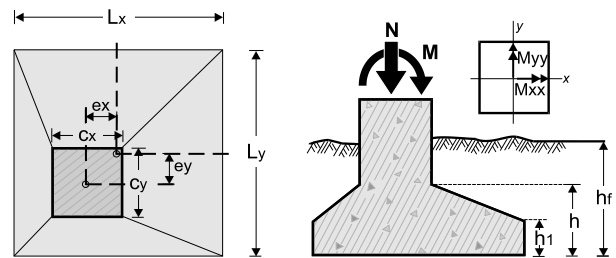
Concrete-Steel class: C25/30-S500
 Concrete cover : Cnom=75 mm
 Concrete weight : 25.0 kN/m³
 γc=1.50, γs=1.15

(EC2 §3)
 (EC2 §4.4.1)
 (EC2 Table 2.1N)

3.1. Dimensions, materials, loads

Dimensions

Footing Lx= 1.700 m Ly= 1.600 m
 Column cx= 0.300 m cy= 0.300 m
 Eccentr. ex=-0.400 m ey=-0.350 m
 Heights h= 0.600 m hf= 0.300 m
 Depth of footing hf= 1.200 m
 Base area of footing A= 2.72 m²
 Volume of footing V= 1.15 m³



Materials of footing

Concrete-Steel class: C25/30-S500
 Concrete cover: Cnom=75 mm
 Effective depth of cross section d=h-d1, d1=Cnom+(3/2)Ø=75+3x12/2=93mm, d=600-93=507mm

(EN1992-1-1, §3)
 (EC2 §4.4.1)

Soil

Soil bearing pressure qu= 0.200 N/mm² (MPa)
 Unit weight of soil γ=17.000 kN/m³

Loads

		permanent	variable
Self weight	kN	[1.15x25.00]	28.75
Soil weight	kN	[(2.72x 1.20- 1.15)x17.00]	35.94
Vertical load	kN	70.00	30.00
Moment Mxx	kNm	0.00	0.00
Moment Myy	kNm	0.00	0.00

3.2. Eurocode parameters

<u>Check of soil bearing capacity</u>				(EC7 EN1997-1-1:2004, §6)	
Partial factors for actions and soil properties				(EC7 Tables A.1-A.4, EC8-5 §3.1)	
Equilibrium limit state (EQU), Structural limit state (STR), Geotechnical limit state (GEO)					
			(EQU)	(STR)	(GEO)
Actions	Permanent Unfavourable	γ_{Gdst} :	1.10	1.35	1.00
	Permanent Favourable	γ_{Gstb} :	0.90	1.00	1.00
	Variable Unfavourable	γ_{Qdst} :	1.50	1.50	1.30
	Variable Favourable	γ_{Qstb} :	0.00	0.00	0.00
Soil parameters	Angle of shearing resistance	γ_{ϕ} :	1.25	1.00	1.25
	Effective cohesion	γ_c :	1.25	1.00	1.25
	Undrained shear strength	γ_{cu} :	1.40	1.00	1.40
	Unconfined strength	γ_{qu} :	1.40	1.00	1.40
	Weight density	γ_w :	1.00	1.00	1.00

Partial safety factors for actions : $\gamma_G=1.35, \gamma_Q=1.50$ (EC0 Annex A1)
 Combination of accidental actions : (EC7) $\psi_2 = 0.30$
 Combination of accidental actions : (EC2) $\psi_2 = 0.30$

Design of reinforced concrete (EC2 EN1992-1-1:2004)

3.3. Check of soil bearing capacity (EC7 EN1997-1-1:2004, §6)

3.3.1. (EQU), 1.10xPermanent + 1.50xVariable (EC7 §2.4.7.2)

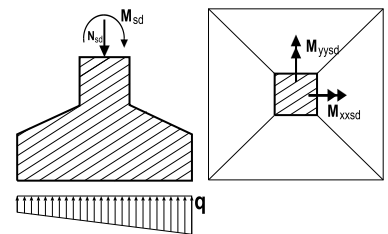
Design Loads

$$N_{sd} = 1.10 \times 134.69 + 1.50 \times 30.00 = 193.16 \text{ kN}$$

$$M_{xxsd} = 1.10 \times 0.00 + 1.50 \times (0.00 + (-0.35) \times 122.00) = -42.70 \text{ kNm}$$

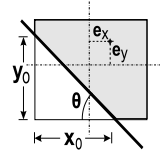
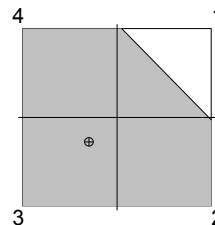
$$M_{yy sd} = 1.10 \times 0.00 + 1.50 \times (0.00 + (-0.40) \times 122.00) = -48.80 \text{ kNm}$$

($1.10 \times 70.00 + 1.50 \times 30.00 = 122.00$)



Eccentricities, soil pressures, footing area

relative eccentricity $e_x/L_x = M_{yy} / (N \cdot L_x) = -0.149$
 relative eccentricity $e_y/L_y = M_{xx} / (N \cdot L_y) = -0.138$
 soil pressure $q_1 = 0.000 \text{ N/mm}^2$
 soil pressure $q_2 = 0.063 \text{ N/mm}^2$
 soil pressure $q_3 = 0.204 \text{ N/mm}^2$
 soil pressure $q_4 = 0.074 \text{ N/mm}^2$
 zero pressure line $x_0 = 2.46\text{m}, y_0 = 2.51\text{m}, \theta = 46^\circ$
 effective footing area 87.52%



Check bearing resistance failure $V_d \leq R_d$

(EC7 EN1997-1-1:2004, §6.5.2)

relative load eccentricities $e_x/L_x = M_{yy} / (N \cdot L_x) = 0.149, e_y/L_y = M_{xx} / (N \cdot L_y) = 0.138$
 relative load eccentricities ≤ 0.333 (EC7 §6.5.4)
 effective design length of footing $L' = 1.700 \times (1 - 2 \times 0.149) = 1.193 \text{ m}$ (EC7 Annex D)
 effective design width of footing $B' = 1.600 \times (1 - 2 \times 0.138) = 1.158 \text{ m}$
 effective design area of footing $L' \cdot B' = 1.193 \times 1.158 = 1.38 \text{ m}^2$
 Design bearing resistance of footing $R_d = 1000 \times 1.38 \times 0.200 / 1.40 = 197.14 \text{ kN} > V_d = 193.16 \text{ kN}$
 Effective footing area 87.52% > 50.00% (EC7 §6.5.4)

3.3.2. (STR), 1.35xPermanent + 1.50xVariable

(EC7 §2.4.7.3)

Design Loads

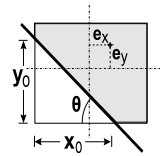
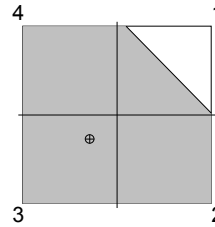
$$N_{sd} = 1.35 \times 134.69 + 1.50 \times 30.00 = 226.83 \text{ kN}$$

$$M_{xxsd} = 1.35 \times 0.00 + 1.50 \times (0.00 + (-0.35) \times 139.50) = -48.82 \text{ kNm}$$

$$M_{yy sd} = 1.35 \times 0.00 + 1.50 \times (0.00 + (-0.40) \times 139.50) = -55.80 \text{ kNm}$$

($1.35 \times 70.00 + 1.50 \times 30.00 = 139.50$)

Eccentricities, soil pressures, footing area
 relative eccentricity $e_x/L_x = M_{yy}/(N \cdot L_x) = -0.145$
 relative eccentricity $e_y/L_y = M_{xx}/(N \cdot L_y) = -0.135$
 soil pressure $q_1 = 0.000 \text{ N/mm}^2$
 soil pressure $q_2 = 0.075 \text{ N/mm}^2$
 soil pressure $q_3 = 0.234 \text{ N/mm}^2$
 soil pressure $q_4 = 0.087 \text{ N/mm}^2$
 zero pressure line $x_0 = 2.50\text{m}$, $y_0 = 2.55\text{m}$, $\theta = 46^\circ$
 effective footing area 88.66%

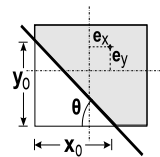
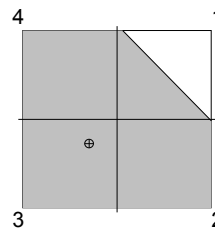


Check bearing resistance failure $V_d \leq R_d$ (EC7 EN1997-1-1:2004, §6.5.2)
 relative load eccentricities $e_x/L_x = M_{yy}/(N \cdot L_x) = 0.145$, $e_y/L_y = M_{xx}/(N \cdot L_y) = 0.135$
 relative load eccentricities ≤ 0.333 (EC7 §6.5.4)
 effective design length of footing $L' = 1.700 \times (1 - 2 \times 0.145) = 1.207 \text{ m}$ (EC7 Annex D)
 effective design width of footing $B' = 1.600 \times (1 - 2 \times 0.135) = 1.168 \text{ m}$
 effective design area of footing $L'B' = 1.207 \times 1.168 = 1.41 \text{ m}^2$
 Design bearing resistance of footing $R_d = 1000 \times 1.41 \times 0.200 / 1.00 = 282.00 \text{ kN} > V_d = 226.83 \text{ kN}$
 Effective footing area 88.66% > 50.00% (EC7 §6.5.4)

3.3.3. (GEO), 1.00xPermanent + 1.30xVariable (EC7 §2.4.7.3)

Design Loads
 $N_{sd} = 1.00 \times 134.69 + 1.30 \times 30.00 = 173.69 \text{ kN}$
 $M_{xxsd} = 1.00 \times 0.00 + 1.30 \times (0.00 + (-0.35) \times 109.00) = -38.15 \text{ kNm}$
 $M_{yyd} = 1.00 \times 0.00 + 1.30 \times (0.00 + (-0.40) \times 109.00) = -43.60 \text{ kNm}$
 (1.00x70.00+1.30x30.00=109.00)

Eccentricities, soil pressures, footing area
 relative eccentricity $e_x/L_x = M_{yy}/(N \cdot L_x) = -0.148$
 relative eccentricity $e_y/L_y = M_{xx}/(N \cdot L_y) = -0.137$
 soil pressure $q_1 = 0.000 \text{ N/mm}^2$
 soil pressure $q_2 = 0.057 \text{ N/mm}^2$
 soil pressure $q_3 = 0.183 \text{ N/mm}^2$
 soil pressure $q_4 = 0.067 \text{ N/mm}^2$
 zero pressure line $x_0 = 2.47\text{m}$, $y_0 = 2.52\text{m}$, $\theta = 46^\circ$
 effective footing area 87.80%



Check bearing resistance failure $V_d \leq R_d$ (EC7 EN1997-1-1:2004, §6.5.2)
 relative load eccentricities $e_x/L_x = M_{yy}/(N \cdot L_x) = 0.148$, $e_y/L_y = M_{xx}/(N \cdot L_y) = 0.137$
 relative load eccentricities ≤ 0.333 (EC7 §6.5.4)
 effective design length of footing $L' = 1.700 \times (1 - 2 \times 0.148) = 1.197 \text{ m}$ (EC7 Annex D)
 effective design width of footing $B' = 1.600 \times (1 - 2 \times 0.137) = 1.162 \text{ m}$
 effective design area of footing $L'B' = 1.197 \times 1.162 = 1.39 \text{ m}^2$
 Design bearing resistance of footing $R_d = 1000 \times 1.39 \times 0.200 / 1.40 = 198.57 \text{ kN} > V_d = 173.69 \text{ kN}$
 Effective footing area 87.80% > 50.00% (EC7 §6.5.4)

3.4. Internal actions for reinforced concrete design

Moments M and shearing forces V , are computed at column faces.
 Shearing forces V^* are computed at distance $d = 0.507\text{m}$ from the column face.
 They are computed, by numerical integration of the soil pressure under the footing.

3.4.1. Loading 1.35xPermanent + 1.50xVariable

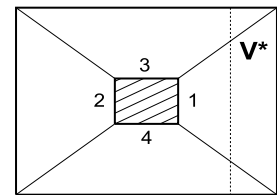
Design Loads
 $N_{sd} = 1.35 \times 134.69 + 1.50 \times 30.00 = 226.83 \text{ kN}$
 $M_{xxsd} = 1.35 \times 0.00 + 1.50 \times (0.00 + (-0.35) \times 139.50) = -48.82 \text{ kNm}$
 $M_{yyd} = 1.35 \times 0.00 + 1.50 \times (0.00 + (-0.40) \times 139.50) = -55.80 \text{ kNm}$
 (1.35x70.00+1.50x30.00=139.50)

Eccentricities, soil pressures, footing area

relative load eccentricities $e_x/L_x = M_{yy}/(N \cdot L_x) = -0.145$, $e_y/L_y = M_{xx}/(N \cdot L_y) = -0.135$
 soil pressures $q_1 = 0.000$, $q_2 = 0.075$, $q_3 = 0.234$, $q_4 = 0.087$ N/mm²
 zero pressure line $x_0 = 2.50$ m, $y_0 = 2.55$ m, $\theta = 46^\circ$
 pressure due to self weight+soil weight $q_g = 0.001 \times 1.35 \times (28.75 + 35.94) / 2.72 = 0.032$ N/mm²
 Shear at critical section + (self weight+soil weight) $q \cdot A_{cont} + q_g \cdot A = 206.05$ kN

Internal actions (bending moments, shearing forces)

$M_{yy}(1) = 21.55$ kNm, $V(1) = 59.07$ kN, $V^*(1) = 16.85$ kN
 $M_{yy}(2) = 8.34$ kNm, $V(2) = 55.50$ kN, $V^*(2) = 0.00$ kN
 $M_{xx}(3) = 20.71$ kNm, $V(3) = 58.80$ kN, $V^*(3) = 16.38$ kN
 $M_{xx}(4) = 8.63$ kNm, $V(4) = 55.87$ kN, $V^*(4) = 0.00$ kN

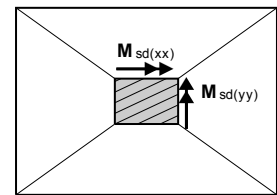


3.5. Design for bending

(EC2 EN1992-1-1:2004, §6.1)

Maximum design moments

$M_{sd}(yy) = 21.55$ kNm, $b = 300$ mm, $d = 507$ mm
 $M_{sd}(xx) = 20.71$ kNm, $b = 300$ mm, $d = 507$ mm



$M_{sd} = 21.55$ kNm, $b = 300$ mm, $d = 507$ mm, $K_d = 5.98$, $x/d = 0.05$
 $e_c/e_s = 1.0/20.0$, $K_s = 2.34$, **$A_s = 0.99$ cm²**

Minimum reinforcement $A_s \geq 0.26bd \cdot f_{ctm}/f_{yk}$ ($A_s = 4.11$ cm²/m) (EC2 §9.3.1)
 Minimum reinforcement $\emptyset 12/27.5$ (4.11 cm²/m)

$M_{sd} = 20.71$ kNm, $b = 300$ mm, $d = 507$ mm, $K_d = 6.10$, $x/d = 0.05$
 $e_c/e_s = 1.0/20.0$, $K_s = 2.34$, **$A_s = 0.95$ cm²**

Minimum reinforcement $A_s \geq 0.26bd \cdot f_{ctm}/f_{yk}$ ($A_s = 4.11$ cm²/m) (EC2 §9.3.1)
 Minimum reinforcement $\emptyset 12/27.5$ (4.11 cm²/m)

Reinforcement of footing

Steel reinforcement in x-x direction: $\emptyset 12/27.5$ (4.11 cm²/m), 7 $\emptyset 12$ (7.91 cm²)
Steel reinforcement in y-y direction: $\emptyset 12/27.5$ (4.11 cm²/m), 7 $\emptyset 12$ (7.91 cm²)

3.6. Design for shear

(EC2 EN1992-1-1:2004, §6.2)

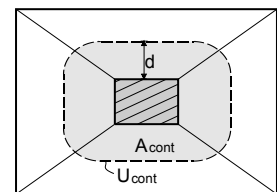
The design for shear is covered by the design in punching shear because the critical rupture surface is considered at angle 45°

3.7. Design for punching shear

(EC2 EN1992-1-1:2004, §6.4)

Footing cantilevers in x-x, $L_1 = 1.100 > d = 0.507$ m, $L_2 = 0.300 < d = 0.507$ m
 Footing cantilevers in y-y, $L_1 = 1.000 > d = 0.507$ m, $L_2 = 0.300 < d = 0.507$ m

Control perimeter, at $1.0d = 0.507$ m $< 2.0d$ (EC2 §6.4.2.2)
 we consider rupture surface at angle 45°
 $U_{cont} = (0.300 + 0.000 + 0.000 + 0.300) + 3.14 \times (0.254 + 0.254) = 2.192$ m
 Base area within the control perimeter
 $A_{cont} = 0.300 \times 0.300 + 0.300 \times 0.507 + 0.300 \times 0.507 + 3.14 \times 0.254 \times 0.254 = 0.60$ m²
 Minimum effective height of footing at control section $d_m = 207$ mm



Applied shear force at control perimeter $V_{ed} = N_{sd} - \sigma \cdot A_{cont}$, $ved = V_{ed} \beta / U_{cont}$
 $ved = (226.83 - 206.05) \times 1.50 / 2.19 = 14.22$ kN/m, $\beta = 1.50$

(EC2 §6.4.3 Fig.6.21N)

Tension reinforcement at control section $A_{sxx} = 4.11$ cm²/m, $A_{syy} = 4.11$ cm²/m
 $A_{s1^2} = (A_{sxx})(A_{syy}) = 4.11 \times 4.11$, $A_{s1} = 4.11$ cm²

Punching shear capacity without shear reinforcement V_{rdc}

(EC2 §6.4.4)

$$V_{rdc} = [C_{rdc} \cdot k \cdot (100 \rho_1 \cdot f_{ck})^{0.333} \cdot (2d/a)] \cdot b_w \cdot d \quad (EC2 \text{ Eq.6.50})$$

$$V_{rdc} >= [v_{min} \cdot 2d/a] \cdot b_w \cdot d, \quad d = d_m = 207 \text{ mm}, \quad a = 507 \text{ mm}$$

$$C_{rdc} = 0.18 / \gamma_c = 0.18 / 1.50 = 0.120, \quad f_{ck} = 25.00 \text{ MPa}$$

$$k = 1 + (200/d)^{1/2} \leq 2, \quad k = 1.98$$

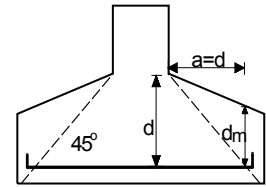
$$\rho_1 = A_{s1} / (b_w \cdot d) = 411 / (1000 \times 207) = 0.0020$$

$$v_{min} = 0.035 \cdot k^{1.50} \cdot f_{ck}^{1/2} = 0.49 \text{ N/mm}^2 \quad (EC2 \text{ Eq.6.3N})$$

$$V_{rd,c(\min)} = 0.001 \times (0.49 \times 2 \times 207 / 507) \times 1000 \times 207 = 82.82 \text{ kN/m}$$

$$V_{rdc} = 0.001 \times [0.120 \times 1.98 \times (0.20 \times 25.00)^{0.333} \times 2 \times 207 / 507] \times 1000 \times 207 = 68.68, \quad V_{rdc} = V_{rdc(\min)} = 82.82 \text{ kN/m}$$

$$V_{sd} = 14.22 \text{ kN/m} \leq V_{rdc} = 82.82 \text{ kN/m}, \text{ shear and punching shear OK}$$



3.8. Reinforcement anchorage

(EC2 EN1992-1-1:2004, §9.8.2.2, §8.4)

$$x = h/2 = 0.150 \text{ m}, \quad R = 1000 \times 0.234 \times 0.150 \times 1.600 = 56.25 \text{ kN}$$

$$e = 0.15b = 0.045 \text{ m}, \quad z_e = 0.670 \text{ m}, \quad z_i = 0.900d = 0.456 \text{ m}$$

$$F_s = R \cdot z_e / z_i = 56.25 \times 0.670 / 0.456 = 82.59 \text{ kN}$$

$$\sigma_{sd} = F_s / A_s = 1000 \times 82.59 / 791 = 104 \text{ MPa}$$

Basic required anchorage length (EC2 Eq.8.3)

$$l_{b,rqd} = (\Phi/4) (\sigma_{sd} / f_{bd}) = (12/4) \times (104 / 2.70) = 116 \text{ mm}$$

$$f_{bd} = 2.25 \times 1.00 \times (f_{ctk} \cdot 0.05 / \gamma_c) = 2.70 \text{ MPa} \quad (EC2 §8.4.2)$$

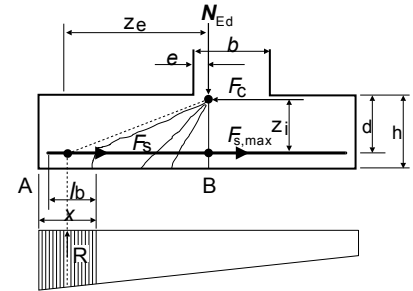
Design anchorage length (EC2 §8.4.4, T.8.2)

$$l_{bd} = 0.70 \times 116 = 81 \text{ mm}, \quad C_{nom} = 75 \text{ mm} > 3\Phi = 36 \text{ mm}$$

Minimum anchorage length $l_{b,min} = \max(0.30 l_{b,rqd}, 10\Phi, 100 \text{ mm}) = 120 \text{ mm}$

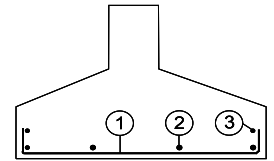
Necessary anchorage length of longitudinal reinforcement $l_{bd} = 120 \text{ mm} = 0.120 \text{ m}$

$$l_{bd} = 120 \text{ mm} > (x - C_{nom}) = 75.00. \text{ Necessary bends } 60 \text{ mm at bar ends for anchorage}$$

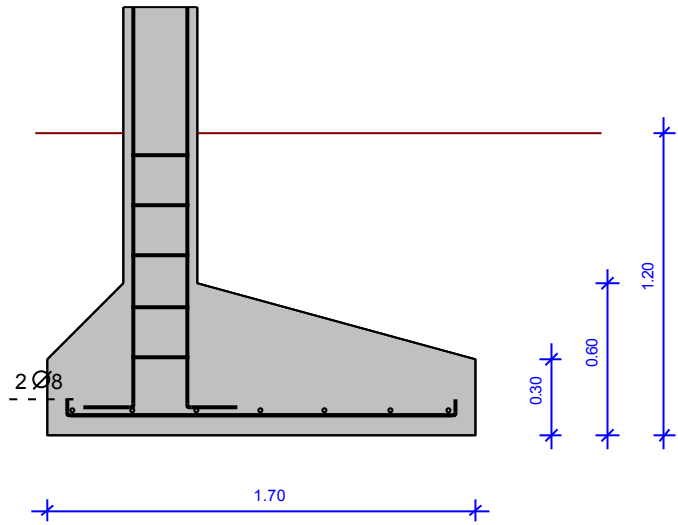
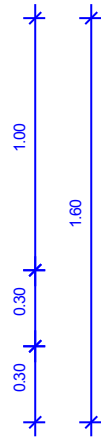
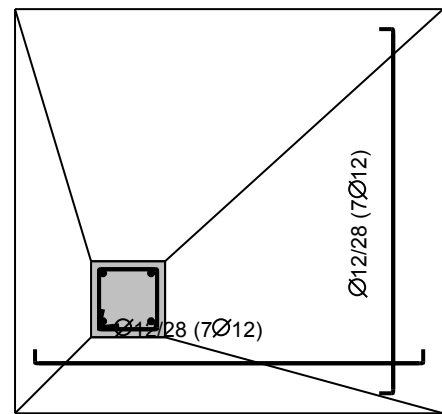


3.9. Reinforcing bar schedule

Num	type	reinforcing bar [mm]	items	∅	g/m [kg/m]	length [m]	weight [kg]
9	①	60 ┌────────── 1550 ─────────┐ 60	7	12	0.888	1.670	10.38
10	②	60 ┌────────── 1450 ─────────┐ 60	7	12	0.888	1.570	9.76
11	③	────────── 1550 ─────────	2	8	0.395	1.550	1.22
12	③	────────── 1450 ─────────	2	8	0.395	1.450	1.15
Total weight [kg]							22.51



	Dead	Live	Seismic
N [kN]	70.00	30.00	0.00
Mxx [kNm]	0.00	0.00	0.00
Myy [kNm]	0.00	0.00	0.00



General information

Asymmetric footing with eccentric load
 Concrete and steel class: C25/30 - S500
 Concrete cover: $C_{nom}=75$ mm
 Soil bearing pressure: 0.20 [N/mm²]

Design codes

Eurocode 0 EN1991-1-1, Basis of structural design
 Eurocode 1 EN1991-1-1, Actions on structures
 Eurocode 2 EN1992-1-1, Design of concrete structures
 Eurocode 7 EN1997-1-1, Geotechnical design
 Eurocode 8 EN1998-5, Earthquake design

Loads

	Dead	Live	Seismic
N [kN]	70.00	30.00	0.00
Mxx [kNm]	0.00	0.00	0.00
Myy [kNm]	0.00	0.00	0.00

Reinforcing bar schedule

#		reinforcing bar [mm]	items	∅ [mm]	g/m [kg/m]	length [m]	weight [kg]
1	F1	60 60	7	12	0.888	1.670	10.38
2	F2	60 60	7	12	0.888	1.570	9.76
3	F3	1550	2	8	0.395	1.550	1.22
4	F3	1450	2	8	0.395	1.450	1.15

Total weight [kg]

22.51

Concrete volume of footing $V= 1.15$ [m³]
 Reinforcement weight $G=22.51$ [kg]

Project: Example of footings 12/03/2007

FOOTING-005

Scale : 1:30

Date: 12/03/2007

Designer:

Draw.No.:

Filename: Example of footings **Sign:**

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