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Example of retaining walls

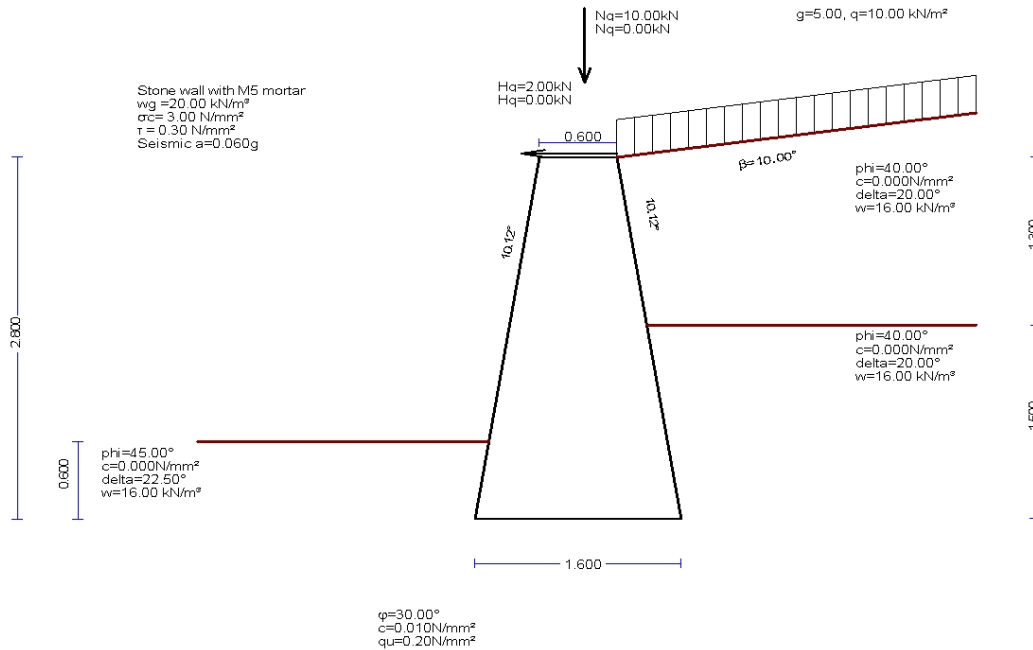
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Example of retaining walls

1. G. WALL-001

Gravity retaining wall

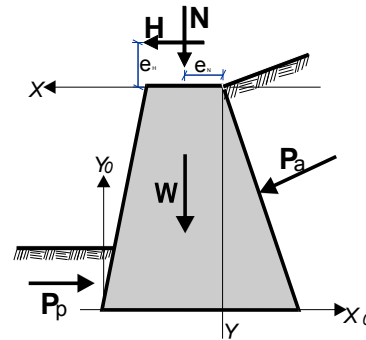
(EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002, EC7 EN1997-1-1:2004, EC8 EN1998-5:2004)



1.1. Wall properties-Parameters-Code requirements

Dimensions

Height of wall	$h = 2.800 \text{ m}$
Transverse length of wall	$L = 10.000 \text{ m}$
Width of wall at top	$B1 = 0.600 \text{ m}$
Width of wall at base	$B = 1.600 \text{ m}$
Slope (batter) at frontface	$10.125^\circ (1:5.60)$
Slope (batter) at backface	$10.125^\circ (1:5.60)$



Loads on wall top

Vertical permanent load	$Ng = 10.00 \text{ kN/m}$
Vertical variable load	$Nq = 0.00 \text{ kN/m}$
Eccentricity of vertical load	$eN = 0.25 \text{ kN/m}$
Horizontal permanent load	$Hg = 2.00 \text{ kN/m}$
Horizontal variable load	$Hq = 0.00 \text{ kN/m}$
Eccentricity of horizontal load	$eH = 0.00 \text{ kN/m}$

Weight of wall

Unit weight of wall material	$\gamma_g = 20.000 \text{ kN/m}^3$
Cross section area of wall	$A = 3.080 \text{ m}^2$
Self weight per meter of wall	$W = 3.080 \times 20.000 = 61.60 \text{ kN/m}$
Center of gravity of wall at	$x = 0.300 \text{ m}, y = 1.612 \text{ m} (x_o = 0.800 \text{ m}, y_o = 1.188 \text{ m})$

Wall materials

Allowable compressive stress	3.00 N/mm ²
Allowable tensile stress	0.00 N/mm ²
Allowable shear stress	0.30 N/mm ²

1.2. Partial factors for actions and soil properties

(EC7 Tables A.1-A.4, EC8-5 §3.1)

Equilibrium limit state (EQU), Structural limit state (STR), Geotechnical limit state (GEO)		(EQU)	(STR)	(GEO)	(SEISMIC)
Actions	Permanent Unfavourable	γ_{Gdst} : 1.10	1.35	1.00	1.00
	Permanent Favourable	γ_{Gstb} : 0.90	1.00	1.00	1.00
	Variable Unfavourable	γ_{Qdst} : 1.50	1.50	1.30	1.00
	Variable Favourable	γ_{Qstb} : 0.00	0.00	0.00	0.00
Soil parameters	Angle of shearing resistance	γ_{ϕ} : 1.25	1.00	1.25	1.25
	Effective cohesion	γ_c : 1.25	1.00	1.25	1.25
	Undrained shear strength	γ_{cu} : 1.40	1.00	1.40	1.40
	Unconfined strength	γ_{qu} : 1.40	1.00	1.40	1.40
	Weight density	γ_w : 1.00	1.00	1.00	1.00

1.3. Properties of foundation soil

Bearing capacity of foundation soil	$q_u=0.20$ N/mm ²
Friction angle between wall footing and soil	$\phi=30.00^\circ$, friction coefficient $\tan(\phi)=0.577$
Cohesion between wall footing and soil	$c=0.010$ N/mm ²

1.4. Seismic coefficients

(EC8 EN1998-5:2004, §7.3.2)

Design ground acceleration ratio	$gh=ax_g$, $a=0.06$	(EC8-5 §7.3.2)
Reduction factor for seismic coefficient	$r=1.50$	(EC8-5 Table 7.1)
Coefficient for horizontal seismic force	$k_h=0.06/1.500=0.040$	(EC8-5 Eq.7.1)
Coefficient for vertical seismic force	$k_v=0.50 \times 0.040=0.020$	(EC8-5 Eq.7.2)

Forces due to seismic load (except from earth pressure)

Horizontal seismic force due to self weight	$F_{wx}= 61.60 \times 0.040=$	2.46 kN/m
Vertical seismic force due to self weight	$F_{wy}= 61.60 \times 0.020=$	1.23 kN/m
Horizontal seismic force of top loading N_g	$F_{gx}= 10.00 \times 0.040=$	0.40 kN/m
Vertical seismic force of top loading N_g	$F_{gy}= 10.00 \times 0.020=$	0.20 kN/m

1.5. Computation of active earth pressure (Coulomb theory)

1.5.1. Wall part from $y=0.000$ m to $y=1.300$ m, $H_s=1.300$ m

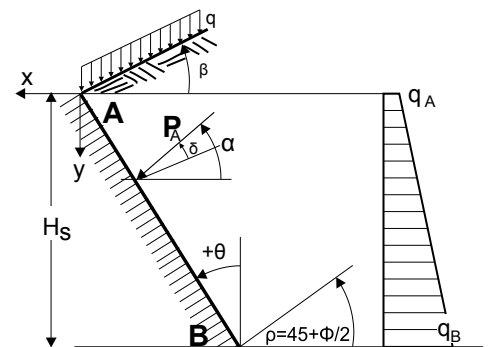
Top point A $x= 0.000$ m $y= 0.000$ m
 Bottom point B $x=-0.232$ m $y= 1.300$ m

Soil properties

Soil type	Mean gravel
Unit weight of soil	$\gamma =16.00$ kN/m ³
Unit weight of soil (saturated)	$\gamma_s=20.00$ kN/m ³
Unit weight of water	$\gamma_w=10.00$ kN/m ³
Angle of shearing resistance of ground	$\phi=40.00^\circ$
Cohesion of ground	$c=0.000$ N/mm ²
Slope angle of ground surface	$\beta=10.00^\circ$
Inclination angle of the wall backface	$\theta=10.12^\circ$
Angle of shear resist. between ground-wall	$\delta=20.00^\circ$

Loads on soil surface

Permanent uniform load	$g= 5.00$ kN/m ²
Variable uniform load	$q= 10.00$ kN/m ²



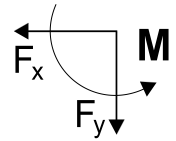
Earth pressure according to Coulomb theory

Angle of rupture plane $\rho=45^\circ+\varphi/2 = 61.00$ EQU STR GEO
 Coefficient of active earth pressure $K_a = 0.408$ 0.308 0.408
 Earth pressure $q(y)=q_A+\gamma \cdot y \cdot K_a$

$$K_A = \frac{\cos^2(\varphi-\theta)}{\cos^2\theta \cos(\theta+\delta) \left[1 + \sqrt{\frac{\sin(\theta+\delta)\sin(\theta-\beta)}{\cos(\theta+\delta)\cos(\theta-\beta)}} \right]^2}$$

Permanent actions

	EQU	STR	GEO
Earth pressure at the top (y=yA)	qA= 1.98	1.49	1.98 kN/m ²
Earth pressure at the bottom (y=yA+ 1.30m)	qB= 10.47	7.90	10.47 kN/m ²
Earth force $Pa=\frac{1}{2}(qA+qB)H$	Pa= 8.09	6.10	8.09 kN/m
Angle of earth force	$\alpha = 24.10$	30.12	24.10 °
Earth force in x direction	Pax= 7.00	5.28	7.00 kN/m
Earth force in y direction	Pay= 4.06	3.06	4.06 kN/m
Moment of earth force at top point (x=0,y=0)	M = -6.16	-4.65	-6.16 kNm/m
Point of application of earth force	x= -0.142 m,	y= 0.798 m	



Variable actions

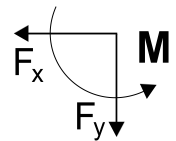
	EQU	STR	GEO
Earth pressure at the top (y=yA)	qA= 3.96	2.99	3.96 kN/m ²
Earth pressure at the bottom (y=yA+ 1.30m)	qB= 3.96	2.99	3.96 kN/m ²
Earth force $Pa=\frac{1}{2}(qA+qB)H$	Pa= 5.15	3.89	5.15 kN/m
Angle of earth force	$\alpha = 24.10$	30.12	24.10 °
Earth force in x direction	Pax= 4.45	3.36	4.45 kN/m
Earth force in y direction	Pay= 2.58	1.95	2.58 kN/m
Moment of earth force at top point (x=0,y=0)	M = -3.19	-2.41	-3.19 kNm/m
Point of application of earth force	x= -0.116 m,	y= 0.650 m	

Total forces and moments

Forces and moments at bottom point B (x=-0.232 m, y=1.300 m)

Permanent actions

	EQU	STR	GEO
Total horizontal earth force F_{sx}	7.00	5.28	7.00 kN/m
Total vertical earth force F_{sy}	4.06	3.06	4.06 kN/m
Total moment of earth force M_s	3.88	2.93	3.88 kNm/m



Variable actions

	EQU	STR	GEO
Total horizontal earth force F_{sx}	4.45	3.36	4.45 kN/m
Total vertical earth force F_{sy}	2.58	1.95	2.58 kN/m
Total moment of earth force M_s	3.19	2.41	3.19 kNm/m

Seismic loading

(EC8 EN1998-5:2004, §7.3.2, Annex E)

Horizontal seismic coefficient $k_h=0.06/1.500=0.040$ (EC8-5 Eq.7.1, T.7.1)
 Vertical seismic coefficient $k_v=0.50 \times 0.040=0.020$ (EC8-5 Eq.7.2)
 Soil above the water table (EC8-5 Annex E.5)
 $\tan(\omega)=k_h/(1-k_v)=0.040/(1-0.020)=0.041$, $\omega=2.34^\circ$

Method Mononobe-Okabe (EC8-5 Annex E.4)
 for active earth force during seismic loading
 Coefficient of active earth pressure, $K_e^* = 0.437$
 Additional earth pressure due to seismic load
 over STR load case $\xi=(K_e^*/K_e-1)=(0.437/0.308-1)=0.419$

$$K_E = \frac{\cos^2(\varphi-\omega-\theta)}{\cos\omega \cos^2\theta \cos(\delta+\theta+\omega) \left[1 + \sqrt{\frac{\sin(\varphi+\delta)\sin(\varphi-\omega-\beta)}{\cos(\theta+\omega+\delta)\cos(\theta-\beta)}} \right]^2}$$

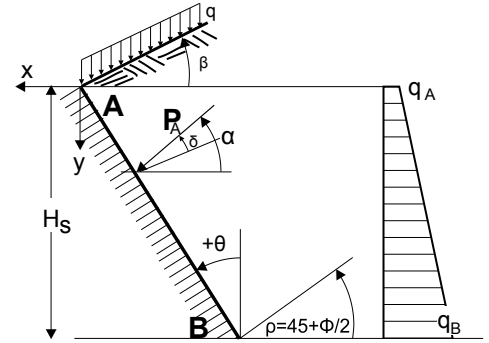
Earth force due to seismic load (Permanent actions) $F_x=1.419 \times 5.28 = 7.49$ kN/m
 Earth force due to seismic load (Variable actions) $F_x=1.419 \times 3.36 = 4.77$ kN/m

1.5.2. Wall part from y=1.300 m to y=2.800 m, Hs=1.500 m

Top point A x=-0.232 m y= 1.300 m
 Bottom point B x=-0.500 m y= 2.800 m

Soil properties

Soil type : Mean gravel
 Unit weight of soil $\gamma = 16.00 \text{ kN/m}^3$
 Unit weight of soil (saturated) $\gamma_s = 20.00 \text{ kN/m}^3$
 Unit weight of water $\gamma_w = 10.00 \text{ kN/m}^3$
 Angle of shearing resistance of ground $\phi = 40.00^\circ$
 Cohesion of ground $c = 0.000 \text{ N/mm}^2$
 Slope angle of ground surface $\beta = 0.00^\circ$
 Inclination angle of the wall backface $\theta = 10.12^\circ$
 Angle of shear resist. between ground-wall $\delta = 20.00^\circ$



Loads on soil surface

Permanent uniform load $g = 25.80 \text{ kN/m}^2$
 Variable uniform load $q = 10.00 \text{ kN/m}^2$

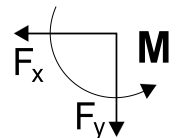
Earth pressure according to Coulomb theory

	EQU	STR	GEO
Angle of rupture plane $\rho = 45^\circ + \phi/2$	= 61.00	65.00	61.00°
Coefficient of active earth pressure K_a	0.356	0.274	0.356
Earth pressure $q(y) = q_A + \gamma \cdot y \cdot K_a$			

$$K_A = \frac{\cos^2(\phi - \theta)}{\cos^2\theta \cos(\theta + \delta)} \left[1 + \sqrt{\frac{\sin(\theta + \delta) \sin(\theta - \beta)}{\cos(\theta + \delta) \cos(\theta - \beta)}} \right]^2$$

Permanent actions

	EQU	STR	GEO
Earth pressure at the top ($y=y_A$)	$q_A = 9.18$	7.07	9.18 kN/m ²
Earth pressure at the bottom ($y=y_A + 1.50\text{m}$)	$q_B = 17.72$	13.65	17.72 kN/m ²
Earth force $P_a = \frac{1}{2}(q_A + q_B)H$	$P_a = 20.17$	15.54	20.17 kN/m
Angle of earth force	$\alpha = 24.10$	30.12	24.10 °
Earth force in x direction	$P_{ax} = 17.45$	13.44	17.45 kN/m
Earth force in y direction	$P_{ay} = 10.12$	7.80	10.12 kN/m
Moment of earth force at top point ($x=0, y=0$)	$M = -41.00$	-31.58	-41.00 kNm/m
Point of application of earth force	$x = -0.380 \text{ m}$,	$y = 2.129 \text{ m}$	



Variable actions

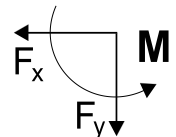
	EQU	STR	GEO
Earth pressure at the top ($y=y_A$)	$q_A = 3.56$	2.74	3.56 kN/m ²
Earth pressure at the bottom ($y=y_A + 1.50\text{m}$)	$q_B = 3.56$	2.74	3.56 kN/m ²
Earth force $P_a = \frac{1}{2}(q_A + q_B)H$	$P_a = 5.34$	4.11	5.34 kN/m
Angle of earth force	$\alpha = 24.10$	30.12	24.10 °
Earth force in x direction	$P_{ax} = 4.62$	3.55	4.62 kN/m
Earth force in y direction	$P_{ay} = 2.68$	2.06	2.68 kN/m
Moment of earth force at top point ($x=0, y=0$)	$M = -10.45$	-8.03	-10.45 kNm/m
Point of application of earth force	$x = -0.366 \text{ m}$,	$y = 2.050 \text{ m}$	

Total forces and moments

Forces and moments at bottom point B ($x=-0.500 \text{ m}$, $y=2.800 \text{ m}$)

Permanent actions

	EQU	STR	GEO
Total horizontal earth force F_{sx}	24.45	18.72	24.45 kN/m
Total vertical earth force F_{sy}	14.18	10.86	14.18 kN/m
Total moment of earth force M_s	28.39	21.62	28.39 kNm/m



Variable actions

	EQU	STR	GEO
Total horizontal earth force F_{sx}	9.07	6.91	9.07 kN/m
Total vertical earth force F_{sy}	5.26	4.01	5.26 kN/m
Total moment of earth force M_s	14.38	10.91	14.38 kNm/m

Seismic loading

(EC8 EN1998-5:2004, §7.3.2, Annex E)

Horizontal seismic coefficient $k_h=0.06/1.500=0.040$ (EC8-5 Eq.7.1, T.7.1)
 Vertical seismic coefficient $k_v=0.50 \times 0.040=0.020$ (EC8-5 Eq.7.2)
 Soil above the water table (EC8-5 Annex E.5)
 $\tan(\omega)=k_h/(1-k_v)=0.040/(1-0.020)=0.041, \omega=2.34^\circ$

Method Mononobe-Okabe (EC8-5 Annex E.4)
 for active earth force during seismic loading
 Coefficient of active earth pressure, $K_e^*=0.377$
 Additional earth pressure due to seismic load
 over STR load case $\xi=(K_e^*/K_e-1)=(0.377/0.274-1)=0.376$

$$K_E = \frac{\cos^2(\varphi-\omega-\theta)}{\cos\omega \cos^2\theta \cos(\delta+\theta+\omega) \left[1 + \sqrt{\frac{\sin(\varphi+\delta)\sin(\varphi-\beta)}{\cos(\theta+\omega+\delta)\cos(\theta-\beta)}} \right]^2}$$

Earth force due to seismic load (Permanent actions) $F_x=1.376 \times 13.44=18.49$ kN/m
 Earth force due to seismic load (Variable actions) $F_x=1.376 \times 3.55= 4.88$ kN/m

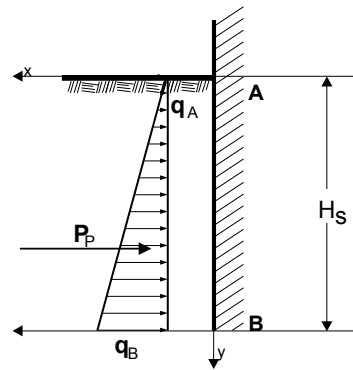
1.6. Computation of passive earth pressure (Rankine theory)

1.6.1. Wall part from $y=2.200$ m to $y=2.800$ m, $H_s=0.600$ m

Top point A $x= 0.993$ m $y= 2.200$ m
 Bottom point B $x= 0.993$ m $y= 2.800$ m

Soil properties

Soil type : Large gravel
 Unit weight of soil $\gamma =16.00$ kN/m³
 Unit weight of soil (saturated) $\gamma_s=20.00$ kN/m³
 Unit weight of water $\gamma_w=10.00$ kN/m³
 Angle of shearing resistance of ground $\varphi=45.00^\circ$
 Cohesion of ground $c=0.000$ N/mm²
 Slope angle of ground surface $\beta= 0.00^\circ$
 Earth pressure on vertical surface $\theta= 0.00^\circ$
 Angle of shear resist. between ground-wall $\delta= 0.00^\circ$



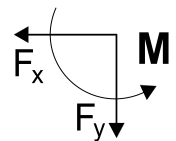
Earth pressure according to Coulomb theory

	EQU	STR	GEO
Angle of rupture plane $\rho=45^\circ-\varphi/2$	= 27.00	22.50	27.00°
Coefficient of passive earth pressure K_p	= 3.852	5.828	3.852
Earth pressure $q(y)=q_A+\gamma \cdot y \cdot K_p$			

$$K_p = \frac{\cos^2(\varphi+\theta)}{\cos^2\theta \cos(\theta-\delta) \left[1 - \sqrt{\frac{\sin(\theta+\delta)\sin(\theta+\beta)}{\cos(\theta-\delta)\cos(\theta-\beta)}} \right]^2}$$

Permanent actions

	EQU	STR	GEO
Earth pressure at the top ($y=y_A$)	$q_A= 0.00$	0.00	0.00 kN/m ²
Earth pressure at the bottom ($y=y_A+ 0.60$ m)	$q_B=-36.98$	-55.95	-36.98 kN/m ²
Earth force $P_a=\frac{1}{2}(q_A+q_B)H$	$P_p= 11.09$	16.78	11.09 kN/m
Angle of earth force α	0.00	0.00	0.00°
Earth force in x direction	$P_{px}=-11.09$	-16.78	-11.09 kN/m
Earth force in y direction	$P_{py}= 0.00$	0.00	0.00 kN/m
Moment of earth force at top point ($x=0, y=0$)	$M = 28.83$	43.63	28.83 kNm/m
Point of application of earth force	$x= 0.993$ m,	$y= 2.600$ m	

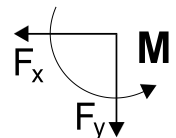


Total forces and moments

Forces and moments at bottom point B ($x=0.993$ m, $y=2.800$ m)

Permanent actions

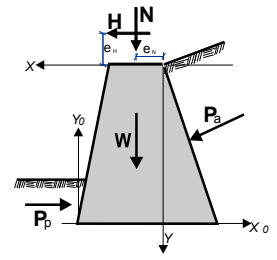
	EQU	STR	GEO
Total horizontal earth force F_{sx}	-11.09	-16.78	-11.09 kN/m
Total vertical earth force F_{sy}	0.00	0.00	0.00 kN/m
Total moment of earth force M_s	-2.22	-3.36	-2.22 kNm/m



1.7. Checks of wall stability (EQU)

1.7.1. Forces (driving and resisting) on the wall (EQU)

Action		y1 - y2	Fx	Fy	x	y
			[kN/m]	[kN/m]	[kN/m]	[m]
Active earth pressure	Pa	0.00- 1.30	7.00	4.06	-0.142	0.798
Backfill surcharge (live)	Pq	0.00- 1.30	4.45	2.58	-0.116	0.650
Active earth pressure	Pa	1.30- 2.80	17.45	10.12	-0.380	2.129
Backfill surcharge (live)	Pq	1.30- 2.80	4.62	2.68	-0.366	2.050
Passive earth pressure	Pp	2.20- 2.80	-11.09	0.00	0.993	2.600
Wall weight	W		0.00	61.60	0.300	1.612
Vert. load on top (dead)	Ng		0.00	10.00	0.250	0.000
Horiz. load on top (dead)	Hg		2.00	0.00	0.300	0.000

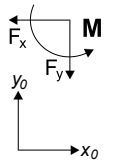


1.7.2. Check of soil bearing capacity (EQU)

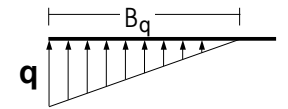
(EC7 EN1997-1-1:2004, §6.5.2)

Check for 0.90x(self weight+top vertical dead load)+0.00x(top vertical live load)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M
			[kN/m]	[kN/m]	[kN/m]	[m]	[kNm/m]
Active earth pressure	Pax1.10	0.00- 1.30	7.70	4.47	1.242	2.002	9.87
Backfill surcharge (live)	Pqx1.50	0.00- 1.30	6.68	3.87	1.216	2.150	9.64
Active earth pressure	Pax1.10	1.30- 2.80	19.20	11.13	1.480	0.671	-3.60
Backfill surcharge (live)	Pqx1.50	1.30- 2.80	6.93	4.02	1.466	0.750	-0.70
Wall weight	W x0.90		0.00	55.44	0.800	1.188	-44.35
Vert. load on top (dead)	Ngx0.90		0.00	9.00	0.850	2.800	-7.65
Horiz. load on top (dead)	Hgx1.10		2.20	0.00	0.800	2.800	6.16
			Sum=	87.93			-30.63



Sum of vertical forces = 87.93 kN/m
 Sum of moments at front toe = -30.63 kNm/m
 Sum of moments at middle of base = 39.71 kNm/m
 Eccentricity $ec = 39.71 / 87.93 = 0.452m$, $ec > 1.600 / 6 = 0.267m$
 Soil pressure $q = 0.168 \text{ N/mm}^2$ $Bq = 1.045 \text{ m}$
 Effective footing $L = 1.600 - 2 \times 0.452 = 0.697 \text{ m}$
 Soil bearing capacity $Rd = L \cdot qu / \gamma M = 0.697 \times (1000 \times 0.20) / 1.40 = 99.57 \text{ kN/m}$
 Bearing resistance check $Vd = 87.93 < Rd = 99.57 \text{ kN/m}$, Check is verified



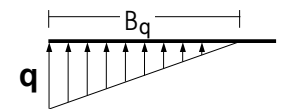
(EC7 Annex D)

Bearing resistance check $Vd = 87.93 < Rd = 99.57 \text{ kN/m}$, Check is verified (EC7 Eq.2.2, Eq.6.1)

Check for 1.10x(self weight+top vertical dead load)+1.50x(top vertical live load)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M
			[kN/m]	[kN/m]	[kN/m]	[m]	[kNm/m]
Active earth pressure	Pax1.10	0.00- 1.30	7.70	4.47	1.242	2.002	9.87
Backfill surcharge (live)	Pqx1.50	0.00- 1.30	6.68	3.87	1.216	2.150	9.64
Active earth pressure	Pax1.10	1.30- 2.80	19.20	11.13	1.480	0.671	-3.60
Backfill surcharge (live)	Pqx1.50	1.30- 2.80	6.93	4.02	1.466	0.750	-0.70
Wall weight	W x1.10		0.00	67.76	0.800	1.188	-54.21
Vert. load on top (dead)	Ngx1.10		0.00	11.00	0.850	2.800	-9.35
Horiz. load on top (dead)	Hgx1.10		2.20	0.00	0.800	2.800	6.16
			Sum=	102.25			-42.19

Sum of vertical forces = 102.25 kN/m
 Sum of moments at front toe = -42.19 kNm/m
 Sum of moments at middle of base = 39.61 kNm/m
 Eccentricity $ec = 39.61 / 102.25 = 0.387m$, $ec > 1.600 / 6 = 0.267m$
 Soil pressure $q = 0.165 \text{ N/mm}^2$ $Bq = 1.238 \text{ m}$
 Effective footing $L = 1.600 - 2 \times 0.387 = 0.825 \text{ m}$
 Soil bearing capacity $Rd = L \cdot qu / \gamma M = 0.825 \times (1000 \times 0.20) / 1.40 = 117.86 \text{ kN/m}$
 Bearing resistance check $Vd = 102.25 < Rd = 117.86 \text{ kN/m}$, Check is verified



(EC7 Annex D)

Bearing resistance check $Vd = 102.25 < Rd = 117.86 \text{ kN/m}$, Check is verified (EC7 Eq.2.2, Eq.6.1)

1.7.3. Failure check due to overturning (EQU)

(EC7 EN1997-1-1:2004, §9.7.4)

Overturning with respect to the toe ($x_0=0, y_0=0$) ($x=1.100, y=2.800$ m)

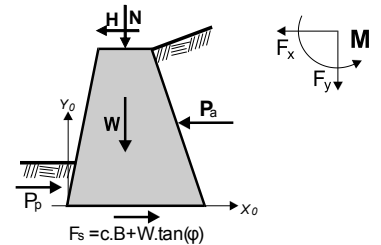
Action	(γ)	$y_1 - y_2$	F_x	F_y	x_0	y_0	M_{o+}	M_{o-}		
			[kN/m]	[kN/m]	[m]	[m]	[kNm/m]	[kNm/m]		
Active earth pressure	Pax1.10	0.00- 1.30	7.70	4.47	1.242	2.002	15.41	5.54		
Backfill surcharge (live)	Pqx1.50	0.00- 1.30	6.68	3.87	1.216	2.150	14.36	4.71		
Active earth pressure	Pax1.10	1.30- 2.80	19.20	11.13	1.480	0.671	12.88	16.48		
Backfill surcharge (live)	Pqx1.50	1.30- 2.80	6.93	4.02	1.466	0.750	5.19	5.90		
Wall weight	W x0.90		0.00	55.44	0.800	1.188	0.00	44.35		
Vert. load on top (dead)	Ngx0.90		0.00	9.00	0.850	2.800	0.00	7.65		
Horiz. load on top (dead)	Hgx1.10		2.20	0.00	0.800	2.800	6.16	0.00		
							Sum=	54.00		84.63

Sum of overturning moments = 54.00 kNm/m
 Sum of moments resisting overturning = 84.63 kNm/m
 Overturning check $M_{sd}=54.00 < M_{rd}=84.63$ kNm/m, Check is verified

1.7.4. Failure check against sliding (EQU)

(EC7 EN1997-1-1:2004, §9.7.3, §6.5.3)

Action	(γ)	$y_1 - y_2$	F_{x+}	F_{x-}	F_y
			[kN/m]	[kN/m]	[kN/m]
Active earth pressure	Pax1.10	0.00- 1.30	7.70	0.00	4.47
Backfill surcharge (live)	Pqx1.50	0.00- 1.30	6.68	0.00	3.87
Active earth pressure	Pax1.10	1.30- 2.80	19.20	0.00	11.13
Backfill surcharge (live)	Pqx1.50	1.30- 2.80	6.93	0.00	4.02
Passive earth pressure	Ppx0.90	2.20- 2.80	0.00	9.98	0.00
Wall weight	W x0.90		0.00	0.00	55.44
Vert. load on top (dead)	Ngx0.90		0.00	0.00	9.00
Horiz. load on top (dead)	Hgx1.10		2.20	0.00	0.00
		Sum=	42.71	9.98	87.93



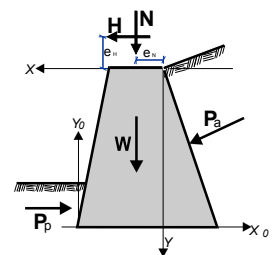
Soil friction $R_d = V_d \cdot \tan\phi / \gamma M = 87.93 \times \tan(30.00^\circ) / 1.25 = 40.61$ kN/m
 Soil cohesion $R_d = A \cdot c_u / \gamma M = 1000 \times 1.045 \times 0.010 / 1.25 = 8.36$ kN/m
 (resisting forces from effective cohesion are neglected)
 Sum of driving forces = 42.71 kN/m
 Sum of resisting forces $(9.98 + 40.61) = 50.59$ kN/m
 Sliding resistance check $H_d = 42.71 < R_d = 50.59$ kN/m, Check is verified

(EC7 §6.5.3. 10)

1.8. Checks of wall stability (STR)

1.8.1. Forces (driving and resisting) on the wall (STR)

Action	$y_1 - y_2$	F_x	F_y	x	y	
		[kN/m]	[kN/m]	[m]	[m]	
Active earth pressure	Pa	0.00- 1.30	5.28	3.06	-0.142	0.798
Backfill surcharge (live)	Pq	0.00- 1.30	3.36	1.95	-0.116	0.650
Active earth pressure	Pa	1.30- 2.80	13.44	7.80	-0.380	2.129
Backfill surcharge (live)	Pq	1.30- 2.80	3.55	2.06	-0.366	2.050
Passive earth pressure	Pp	2.20- 2.80	-16.78	0.00	0.993	2.600
Wall weight	W		0.00	61.60	0.300	1.612
Vert. load on top (dead)	Ng		0.00	10.00	0.250	0.000
Horiz. load on top (dead)	Hg		2.00	0.00	0.300	0.000

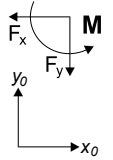


1.8.2. Check of soil bearing capacity (STR)

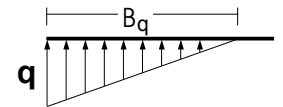
(EC7 EN1997-1-1:2004, §6.5.2)

Check for 1.00x(self weight+top vertical dead load)+0.00x(top vertical live load)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.35	0.00- 1.30	7.13	4.13	1.242	2.002	9.14	
Backfill surcharge (live)	Pqx1.50	0.00- 1.30	5.04	2.93	1.216	2.150	7.27	
Active earth pressure	Pax1.35	1.30- 2.80	18.14	10.53	1.480	0.671	-3.40	
Backfill surcharge (live)	Pqx1.50	1.30- 2.80	5.32	3.09	1.466	0.750	-0.54	
Wall weight	W x1.00		0.00	61.60	0.800	1.188	-49.28	
Vert. load on top (dead)	Ngx1.00		0.00	10.00	0.850	2.800	-8.50	
Horiz. load on top (dead)	Hgx1.35		2.70	0.00	0.800	2.800	7.56	
			Sum=	92.28				-37.75



Sum of vertical forces = 92.28 kN/m
 Sum of moments at front toe = -37.75 kNm/m
 Sum of moments at middle of base = 36.07 kNm/m
 Eccentricity $ec=36.07/92.28=0.391m$, $ec>1.600/6=0.267m$
 Soil pressure $q=0.150 N/mm^2$ $Bq=1.227 m$
 Effective footing $L=1.600-2x0.391= 0.818 m$
 Soil bearing capacity $Rd=L\cdot qu/\gamma M=0.818x(1000x0.20)/1.00= 163.60 kN/m$
 Bearing resistance check $Vd=92.28 < Rd=163.60 kN/m$, Check is verified



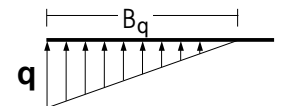
(EC7 Annex D)

(EC7 Eq.2.2, Eq.6.1)

Check for 1.35x(self weight+top vertical dead load)+1.50x(top vertical live load)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.35	0.00- 1.30	7.13	4.13	1.242	2.002	9.14	
Backfill surcharge (live)	Pqx1.50	0.00- 1.30	5.04	2.93	1.216	2.150	7.27	
Active earth pressure	Pax1.35	1.30- 2.80	18.14	10.53	1.480	0.671	-3.40	
Backfill surcharge (live)	Pqx1.50	1.30- 2.80	5.32	3.09	1.466	0.750	-0.54	
Wall weight	W x1.35		0.00	83.16	0.800	1.188	-66.53	
Vert. load on top (dead)	Ngx1.35		0.00	13.50	0.850	2.800	-11.48	
Horiz. load on top (dead)	Hgx1.35		2.70	0.00	0.800	2.800	7.56	
			Sum=	117.34				-57.98

Sum of vertical forces = 117.34 kN/m
 Sum of moments at front toe = -57.98 kNm/m
 Sum of moments at middle of base = 35.89 kNm/m
 Eccentricity $ec=35.89/117.34=0.306m$, $ec>1.600/6=0.267m$
 Soil pressure $q=0.158 N/mm^2$ $Bq=1.482 m$
 Effective footing $L=1.600-2x0.306= 0.988 m$
 Soil bearing capacity $Rd=L\cdot qu/\gamma M=0.988x(1000x0.20)/1.00= 197.60 kN/m$
 Bearing resistance check $Vd=117.34 < Rd=197.60 kN/m$, Check is verified



(EC7 Annex D)

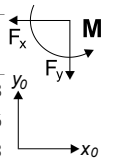
(EC7 Eq.2.2, Eq.6.1)

1.8.3. Failure check due to overturning (STR)

(EC7 EN1997-1-1:2004, §9.7.4)

Overturning with respect to the toe ($xo=0, yo=0$) ($x=1.100, y=2.800 m$)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	Mo+	Mo-	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]	[kNm/m]
Active earth pressure	Pax1.35	0.00- 1.30	7.13	4.13	1.242	2.002	14.27	5.13	
Backfill surcharge (live)	Pqx1.50	0.00- 1.30	5.04	2.93	1.216	2.150	10.83	3.55	
Active earth pressure	Pax1.35	1.30- 2.80	18.14	10.53	1.480	0.671	12.18	15.58	
Backfill surcharge (live)	Pqx1.50	1.30- 2.80	5.32	3.09	1.466	0.750	3.99	4.53	
Wall weight	W x1.00		0.00	61.60	0.800	1.188	0.00	49.28	
Vert. load on top (dead)	Ngx1.00		0.00	10.00	0.850	2.800	0.00	8.50	
Horiz. load on top (dead)	Hgx1.35		2.70	0.00	0.800	2.800	7.56	0.00	
							Sum=	48.83	86.57

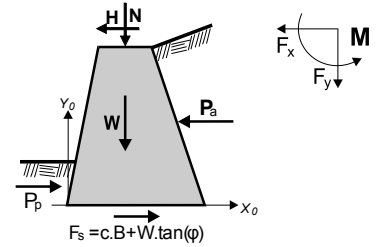


Sum of overturning moments = 48.83 kNm/m
 Sum of moments resisting overturning = 86.57 kNm/m
 Overturning check $Msd=48.83 < Mrd=86.57 kNm/m$, Check is verified

1.8.4. Failure check against sliding (STR)

(EC7 EN1997-1-1:2004, §9.7.3, §6.5.3)

Action	(γ)	y1 - y2	Fx+	Fx-	Fy
			[kN/m]	[kN/m]	[kN/m]
Active earth pressure	Pax1.35	0.00- 1.30	7.13	0.00	4.13
Backfill surcharge (live)	Pqx1.50	0.00- 1.30	5.04	0.00	2.93
Active earth pressure	Pax1.35	1.30- 2.80	18.14	0.00	10.53
Backfill surcharge (live)	Pqx1.50	1.30- 2.80	5.32	0.00	3.09
Passive earth pressure	Ppx1.00	2.20- 2.80	0.00	16.78	0.00
Wall weight	W x1.00		0.00	0.00	61.60
Vert. load on top (dead)	Ngx1.00		0.00	0.00	10.00
Horiz. load on top (dead)	Hgx1.35		2.70	0.00	0.00
		Sum=	38.33	16.78	92.28



Soil friction $Rd = Vd \cdot \tan\phi / \gamma M = 92.28 \cdot \tan(30.00^\circ) / 1.00 = 53.28$ kN/m

Soil cohesion $Rd = A \cdot cu / \gamma M = 1000 \cdot 1.227 \cdot 0.010 / 1.00 = 12.27$ kN/m

(resisting forces from effective cohesion are neglected)

(EC7 §6.5.3. 10)

Sum of driving forces = 38.33 kN/m

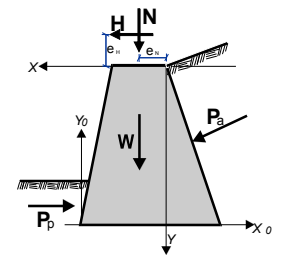
Sum of resisting forces (16.78+53.28) = 70.06 kN/m

Sliding resistance check $Hd = 38.33 < Rd = 70.06$ kN/m, Check is verified

1.9. Checks of wall stability (GEO)

1.9.1. Forces (driving and resisting) on the wall (GEO)

Action		y1 - y2	Fx	Fy	x	y
			[kN/m]	[kN/m]	[m]	[m]
Active earth pressure	Pa	0.00- 1.30	7.00	4.06	-0.142	0.798
Backfill surcharge (live)	Pq	0.00- 1.30	4.45	2.58	-0.116	0.650
Active earth pressure	Pa	1.30- 2.80	17.45	10.12	-0.380	2.129
Backfill surcharge (live)	Pq	1.30- 2.80	4.62	2.68	-0.366	2.050
Passive earth pressure	Pp	2.20- 2.80	-11.09	0.00	0.993	2.600
Wall weight	W		0.00	61.60	0.300	1.612
Vert. load on top (dead)	Ng		0.00	10.00	0.250	0.000
Horiz. load on top (dead)	Hg		2.00	0.00	0.300	0.000

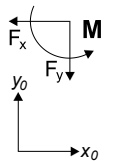


1.9.2. Check of soil bearing capacity (GEO)

(EC7 EN1997-1-1:2004, §6.5.2)

Check for $1.00x(\text{self weight} + \text{top vertical dead load}) + 0.00x(\text{top vertical live load})$

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M
			[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.00	0.00- 1.30	7.00	4.06	1.242	2.002	8.97
Backfill surcharge (live)	Pqx1.30	0.00- 1.30	5.78	3.35	1.216	2.150	8.36
Active earth pressure	Pax1.00	1.30- 2.80	17.45	10.12	1.480	0.671	-3.27
Backfill surcharge (live)	Pqx1.30	1.30- 2.80	6.01	3.48	1.466	0.750	-0.61
Wall weight	W x1.00		0.00	61.60	0.800	1.188	-49.28
Vert. load on top (dead)	Ngx1.00		0.00	10.00	0.850	2.800	-8.50
Horiz. load on top (dead)	Hgx1.00		2.00	0.00	0.800	2.800	5.60
		Sum=		92.61			-38.73



Sum of vertical forces = 92.61 kN/m
 Sum of moments at front toe = -38.73 kNm/m
 Sum of moments at middle of base = 35.36 kNm/m
 Eccentricity $ec = 35.36 / 92.61 = 0.382$ m, $ec > 1.600 / 6 = 0.267$ m

Soil pressure $q = 0.148$ N/mm² $Bq = 1.255$ m

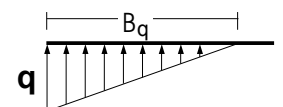
Effective footing $L = 1.600 - 2 \cdot 0.382 = 0.836$ m

(EC7 Annex D)

Soil bearing capacity $Rd = L \cdot qu / \gamma M = 0.836 \cdot (1000 \cdot 0.20) / 1.40 = 119.43$ kN/m

Bearing resistance check $Vd = 92.61 < Rd = 119.43$ kN/m, Check is verified

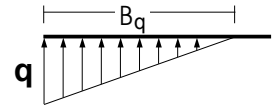
(EC7 Eq.2.2, Eq.6.1)



Check for 1.00x(self weight+top vertical dead load)+1.30x(top vertical live load)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.00	0.00- 1.30	1.30	7.00	4.06	1.242	2.002	8.97
Backfill surcharge (live)	Pqx1.30	0.00- 1.30	1.30	5.78	3.35	1.216	2.150	8.36
Active earth pressure	Pax1.00	1.30- 2.80	2.80	17.45	10.12	1.480	0.671	-3.27
Backfill surcharge (live)	Pqx1.30	1.30- 2.80	2.80	6.01	3.48	1.466	0.750	-0.61
Wall weight	W x1.00			0.00	61.60	0.800	1.188	-49.28
Vert. load on top (dead)	Ngx1.00			0.00	10.00	0.850	2.800	-8.50
Horiz. load on top (dead)	Hgx1.00			2.00	0.00	0.800	2.800	5.60
				Sum=	92.61			-38.73

Sum of vertical forces = 92.61 kN/m
 Sum of moments at front toe = -38.73 kNm/m
 Sum of moments at middle of base = 35.36 kNm/m
 Eccentricity $ec=35.36/92.61=0.382m$, $ec>1.600/6=0.267m$
 Soil pressure $q=0.148 N/mm^2$ $Bq=1.255 m$
 Effective footing $L=1.600-2x0.382= 0.836 m$
 Soil bearing capacity $Rd=L\cdot qu/\gamma M=0.836x(1000x0.20)/1.40= 119.43 kN/m$
 Bearing resistance check $Vd=92.61 < Rd=119.43 kN/m$, Check is verified



(EC7 Annex D)

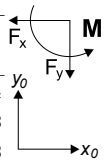
(EC7 Eq.2.2, Eq.6.1)

1.9.3. Failure check due to overturning (GEO)

(EC7 EN1997-1-1:2004, §9.7.4)

Overturning with respect to the toe ($xo=0, yo=0$) ($x=1.100, y=2.800 m$)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	Mo+	Mo-	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]	[kNm/m]
Active earth pressure	Pax1.00	0.00- 1.30	1.30	7.00	4.06	1.242	2.002	14.01	5.04
Backfill surcharge (live)	Pqx1.30	0.00- 1.30	1.30	5.78	3.35	1.216	2.150	12.44	4.08
Active earth pressure	Pax1.00	1.30- 2.80	2.80	17.45	10.12	1.480	0.671	11.71	14.98
Backfill surcharge (live)	Pqx1.30	1.30- 2.80	2.80	6.01	3.48	1.466	0.750	4.50	5.11
Wall weight	W x1.00			0.00	61.60	0.800	1.188	0.00	49.28
Vert. load on top (dead)	Ngx1.00			0.00	10.00	0.850	2.800	0.00	8.50
Horiz. load on top (dead)	Hgx1.00			2.00	0.00	0.800	2.800	5.60	0.00
						Sum=		48.26	86.99

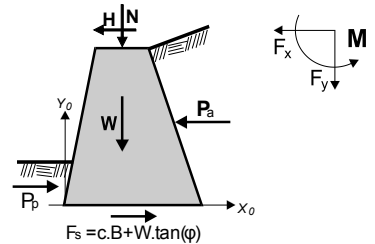


Sum of overturning moments = 48.26 kNm/m
 Sum of moments resisting overturning = 86.99 kNm/m
 Overturning check $Msd=48.26 < Mrd=86.99 kNm/m$, Check is verified

1.9.4. Failure check against sliding (GEO)

(EC7 EN1997-1-1:2004, §9.7.3, §6.5.3)

Action	(γ)	y1 - y2	Fx+	Fx-	Fy		
				[kN/m]	[kN/m]	[kN/m]	
Active earth pressure	Pax1.00	0.00- 1.30	1.30	7.00	0.00	4.06	
Backfill surcharge (live)	Pqx1.30	0.00- 1.30	1.30	5.78	0.00	3.35	
Active earth pressure	Pax1.00	1.30- 2.80	2.80	17.45	0.00	10.12	
Backfill surcharge (live)	Pqx1.30	1.30- 2.80	2.80	6.01	0.00	3.48	
Passive earth pressure	Ppx1.00	2.20- 2.80	2.80	0.00	11.09	0.00	
Wall weight	W x1.00			0.00	0.00	61.60	
Vert. load on top (dead)	Ngx1.00			0.00	0.00	10.00	
Horiz. load on top (dead)	Hgx1.00			2.00	0.00	0.00	
				Sum=	38.24	11.09	92.61



Soil friction $Rd=Vd\cdot \tan\phi/\gamma M= 92.61x\tan(30.00^\circ)/1.25= 42.77 kN/m$
 Soil cohesion $Rd=A\cdot cu/\gamma M = 1000x1.255x0.010/1.25= 10.04 kN/m$
 (resisting forces from effective cohesion are neglected)
 Sum of driving forces = 38.24 kN/m
 Sum of resisting forces (11.09+42.77) = 53.86 kN/m
 Sliding resistance check $Hd=38.24 < Rd=53.86 kN/m$, Check is verified

(EC7 §6.5.3. 10)

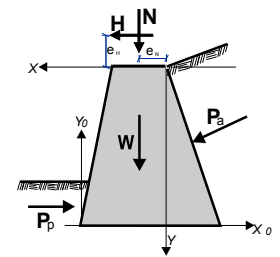
1.10. Seismic design

(EC8 EN1998-5:2004)

Checks of wall stability (with seismic loading)

1.10.1. Forces (driving and resisting) on the wall

Action		y1 - y2	Fx	Fy	x	y	
				[kN/m]	[kN/m]	[m]	[m]
Active earth pressure	Pa	0.00- 1.30	5.28	5.28	3.06	-0.142	0.798
Backfill surcharge (live)	Pq	0.00- 1.30	3.36	3.36	1.95	-0.116	0.650
Active earth pressure	Pa	1.30- 2.80	13.44	13.44	7.80	-0.380	2.129
Backfill surcharge (live)	Pq	1.30- 2.80	3.55	3.55	2.06	-0.366	2.050
Passive earth pressure	Pp	2.20- 2.80	-16.78	-16.78	0.00	0.993	2.600
Wall weight	W		0.00	61.60	61.60	0.300	1.612
Vert. load on top (dead)	Ng		0.00	10.00	10.00	0.250	0.000
Horiz. load on top (dead)	Hg		2.00	0.00	0.00	0.300	0.000



1.10.2. Additional forces due to seismic load

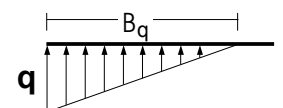
Action		y1 - y2	Fx	Fy	x	y	
				[kN/m]	[kN/m]	[m]	[m]
Active earth pressure	Pa	0.00- 1.30	2.21	2.21		-0.142	0.798
Backfill surcharge (live)	Pq	0.00- 1.30	1.41	1.41		-0.116	0.650
Active earth pressure	Pa	1.30- 2.80	5.05	5.05		-0.380	2.129
Backfill surcharge (live)	Pq	1.30- 2.80	1.33	1.33		-0.366	2.050
Wall weight	W		2.46	2.46	-1.23	0.300	1.612
Vert. load on top (dead)	Ng		0.40	0.40	-0.20	0.250	0.000

1.10.3. Check of soil bearing capacity (with seismic loading)

(EC7 §6.5.2)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.00	0.00- 1.30	7.49	7.49	3.06	1.242	2.002	11.20
Backfill surcharge (live)	Pqx1.00	0.00- 1.30	4.77	4.77	1.95	1.216	2.150	7.88
Active earth pressure	Pax1.00	1.30- 2.80	18.49	18.49	7.80	1.480	0.671	0.87
Backfill surcharge (live)	Pqx1.00	1.30- 2.80	4.88	4.88	2.06	1.466	0.750	0.64
Wall weight	W x1.00		2.46	2.46	60.37	0.800	1.188	-45.37
Vert. load on top (dead)	Ngx1.00		0.40	0.40	9.80	0.850	2.800	-7.21
Horiz. load on top (dead)	Hgx1.00		2.00	2.00	0.00	0.800	2.800	5.60
			Sum=	85.04				-26.39

Sum of vertical forces = 85.04 kN/m
 Sum of moments at front toe = -26.39 kNm/m
 Sum of moments at middle of base = 41.64 kNm/m
 Eccentricity $ec = 41.64 / 85.04 = 0.490m$, $ec > 1.600 / 6 = 0.267m$
 Soil pressure $q = 0.183 \text{ N/mm}^2$ $Bq = 0.931 \text{ m}$
 Effective footing $L = 1.600 - 2 \times 0.490 = 0.621 \text{ m}$
 Soil bearing capacity $Rd = L \cdot qu / \gamma M = 0.621 \times (1000 \times 0.20) / 1.00 = 124.20 \text{ kN/m}$
 Bearing resistance check $Vd = 85.04 < Rd = 124.20 \text{ kN/m}$, Check is verified



(EC7 Annex D)

(EC7 Eq.2.2, Eq.6.1)

1.10.4. Failure check due to overturning (with seismic loading)

(EC7 §9.7.4)

Overturning with respect to the toe (xo=0,yo=0) (x=1.100,y=2.800 m)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	Mo+	Mo-
			[kN/m]	[kN/m]	[m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.00	0.00- 1.30	7.49	3.06	1.242	2.002	15.00	3.80
Backfill surcharge (live)	Pqx1.00	0.00- 1.30	4.77	1.95	1.216	2.150	10.25	2.37
Active earth pressure	Pax1.00	1.30- 2.80	18.49	7.80	1.480	0.671	12.41	11.54
Backfill surcharge (live)	Pqx1.00	1.30- 2.80	4.88	2.06	1.466	0.750	3.66	3.02
Wall weight	W x1.00		2.46	60.37	0.800	1.188	3.91	49.28*
Vert. load on top (dead)	Ngx1.00		0.40	9.80	0.850	2.800	1.29	8.50*
Horiz. load on top (dead)	Hgx1.00		2.00	0.00	0.800	2.800	5.60	0.00
							Sum=	52.12 78.51

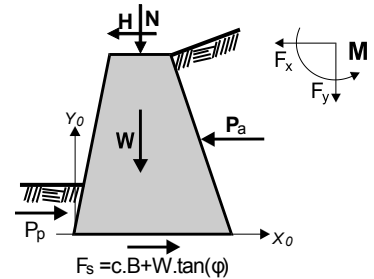
(*moments of negative seismic vertical loads, are added to the overturning moments)

Sum of overturning moments = 52.12 kNm/m
 Sum of moments resisting overturning = 78.51 kNm/m
 Overturning check Msd=52.12 < Mrd=78.51 kNm/m, Check is verified

1.10.5. Failure check against sliding (with seismic loading)

(EC7 §9.7.3, §6.5.3)

Action	(γ)	y1 - y2	Fx+	Fx-	Fy
			[kN/m]	[kN/m]	[kN/m]
Active earth pressure	Pax1.00	0.00- 1.30	7.49	0.00	3.06
Backfill surcharge (live)	Pqx1.00	0.00- 1.30	4.77	0.00	1.95
Active earth pressure	Pax1.00	1.30- 2.80	18.49	0.00	7.80
Backfill surcharge (live)	Pqx1.00	1.30- 2.80	4.88	0.00	2.06
Passive earth pressure	Ppx1.00	2.20- 2.80	0.00	16.78	0.00
Wall weight	W x1.00		2.46	0.00	60.37
Vert. load on top (dead)	Ngx1.00		0.40	0.00	9.80
Horiz. load on top (dead)	Hgx1.00		2.00	0.00	0.00
			Sum=	40.49	16.78 85.04



Soil friction $Rd = Vd \cdot \tan\phi / \gamma M = 85.04 \times \tan(30.00^\circ) / 1.00 = 49.10$ kN/m
 Soil cohesion $Rd = A \cdot cu / \gamma M = 1000 \times 0.931 \times 0.010 / 1.00 = 9.31$ kN/m
 (resisting forces from effective cohesion are neglected)
 Sum of driving forces = 40.49 kN/m
 Sum of resisting forces (16.78+49.10) = 65.88 kN/m
 Sliding resistance check $Hd = 40.49 < Rd = 65.88$ kN/m, Check is verified

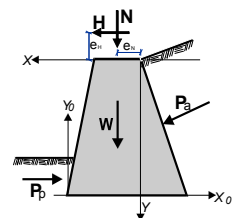
(EC7 §6.5.3. 10)

1.11. Design of wall steam

1.11.1. Loading 1.35x(permanent unfavourable)+1.00x(permanent favourable)+1.50x(variable unfav.)

Forces (at centroid of cross section) and stresses at wall steam
 x, y: cross section centroid, b: cross section width, e: eccentricity
 Fx: horizontal force, Fy: vertical force, M: moment, e/b: relative eccentricity
 σ1, σ2: cross section normal stresses, τ: shear stress, Bq: effective cross section width

y	x	b	Fx	Fy	M	e/b	σ1	σ2	Bq/B	τ
[m]	[m]	[m]	[kN/m]	[kN/m]	[kNm/m]		[N/mm ²]	[N/mm ²]		[N/mm ²]
0.50	0.300	0.779	6.23	18.94	0.97	-0.066	-0.034	-0.015	1.000	0.008
1.00	0.300	0.957	11.22	30.51	4.01	-0.137	-0.058	-0.006	1.000	0.012
1.50	0.300	1.136	17.34	44.52	9.26	-0.183	-0.082	0.000	0.951	0.015
2.00	0.300	1.314	24.39	60.86	17.12	-0.214	-0.108	0.000	0.858	0.019
2.80	0.300	1.600	38.34	92.28	36.09	-0.244	-0.150	0.000	0.767	0.024



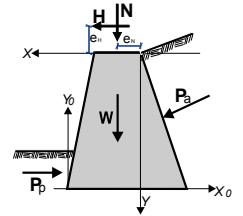
1.11.2. Strength check with allowable stresses

Compression $\sigma_{max} = 0.150 \leq \sigma(\text{allowable}) = 3.000$ N/mm²
 Tension $\sigma_{max} = 0.000 \leq \sigma(\text{allowable}) = 0.000$ N/mm²
 Shear $\tau_{max} = 0.024 \leq \tau(\text{allowable}) = 0.300$ N/mm²

1.11.3. Loading 1.00x(permanent unfav.)+1.00x(permanent favour.)+1.00x(variable)+1.00x(seismic)

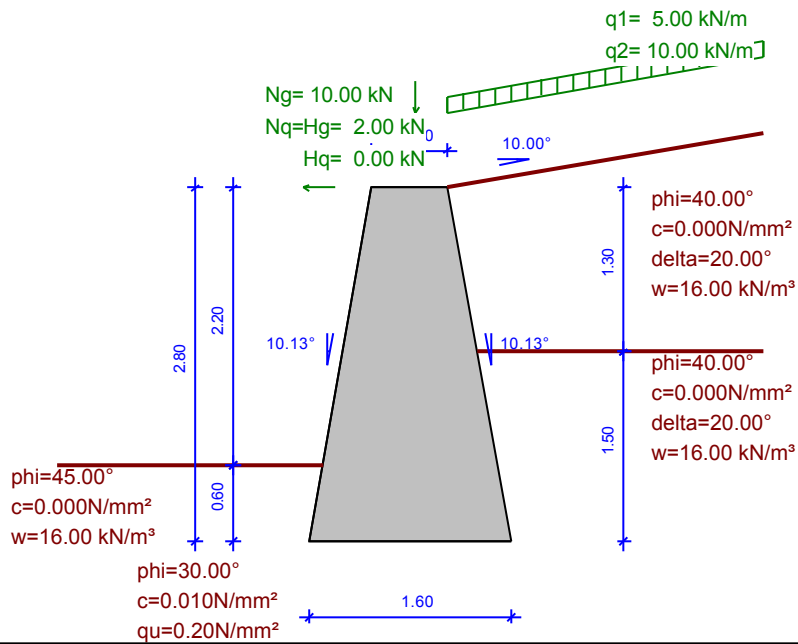
Forces (at centroid of cross section) and stresses at wall stem (with seismic loading)
 x, y:cross section centroid, b:cross section width, e:eccentricity
 Fx:horizontal force, Fy:vertical force, M:moment, e/b:relative eccentricity
 σ1, σ2: cross section normal stresses, τ:shear stress, Bq:effective cross section width

y	x	b	Fx	Fy	M	e/b	σ1	σ2	Bq/B	τ	
[m]	[m]	[m]	[kN/m]	[kN/m]	[kNm/m]			[N/mm ²]	[N/mm ²]		[N/mm ²]
0.50	0.300	0.779	6.18	17.99	1.10	-0.074	-0.035	-0.013	1.000	0.008	
1.00	0.300	0.957	11.57	28.55	4.57	-0.157	-0.062	-0.002	1.000	0.012	
1.50	0.300	1.136	16.74	41.36	9.44	-0.187	-0.083	0.000	0.940	0.015	
2.00	0.300	1.314	24.23	56.31	17.81	-0.223	-0.111	0.000	0.832	0.018	
2.80	0.300	1.600	39.09	85.04	38.62	-0.262	-0.161	0.000	0.715	0.024	



1.11.4. Strength check with allowable stresses (with seismic loading)

Compression σ max= 0.161 <= σ(allowable)= 3.000 N/mm²
 Tension σ max= 0.000 <= σ(allowable)= 0.000 N/mm²
 Shear τ max= 0.024 <= τ(allowable)= 0.300 N/mm²



General information

Wall type : Gravity wall

Wall materials

Allowable compressive stress 3.00 N/mm²

Allowable tensile stress 0.00 N/mm²

Allowable shear stress 0.30 N/mm²

Design codes

Eurocode 0 EN1991-1-1, Basis of structural design

Eurocode 1 EN1991-1-1, Actions on structures

Eurocode 2 EN1992-1-1, Design of concrete structures

Eurocode 7 EN1997-1-1, Geotechnical design

Eurocode 8 EN1998-5, Earthquake design

Loads

Vertical : dead Ng=10.00kN, live Nq=0.00kN

Horizontal: dead Hg=2.00kN, live Hq=0.00kN

Surcharge : dead g=5.00kN/m², live q=10.00kN/m²

Seismic coefficients

Design ground acceleration ratio a =0.060

Coefficient for horizontal seismic force kh=0.040

Coefficient for vertical seismic force kv=0.020

Soil properties back-1

phi=40.00°

c=0.000N/mm²

delta=20.00°

w=16.00 kN/m³

Soil properties back-2

phi=40.00°

c=0.000N/mm²

delta=20.00°

w=16.00 kN/m³

Soil properties front

phi=45.00°

c=0.000N/mm²

w=16.00 kN/m³

Foundation soil properties

phi=30.00°

c=0.010N/mm²

qu=0.20N/mm²

Concrete volume V= 30.80 [m³]

Project: Example of retaining walls 12/0

G. WALL-001

Scale : 1:60

Date: 12/03/2007

Designer:

Draw.No.:

Filename: Example of retaining wall **Sign:**

RUNET Norway as

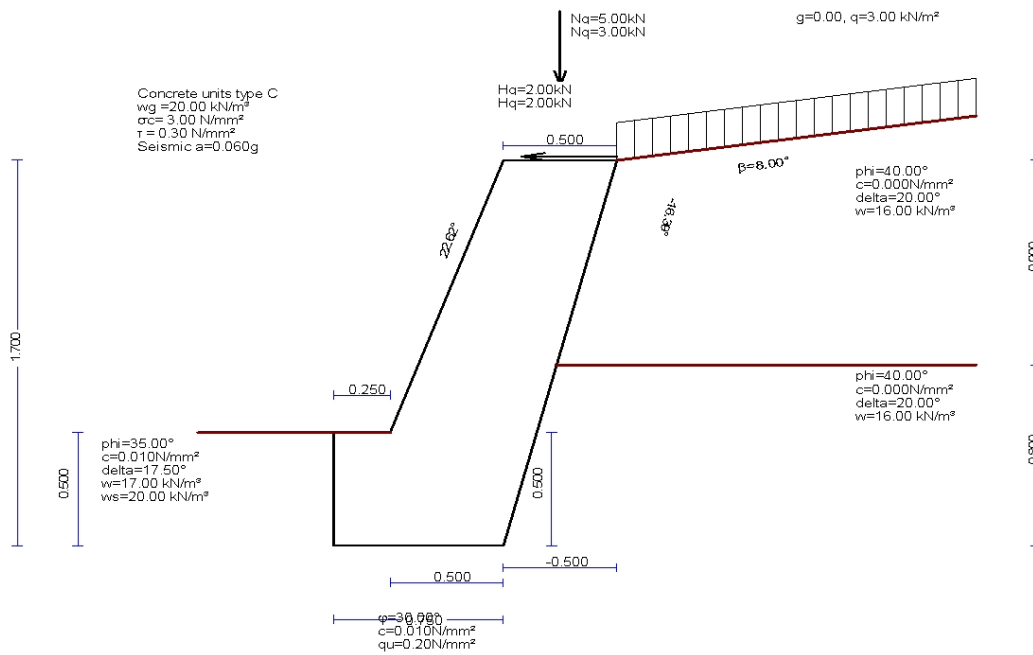
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2. G. WALL-002

Gravity retaining wall

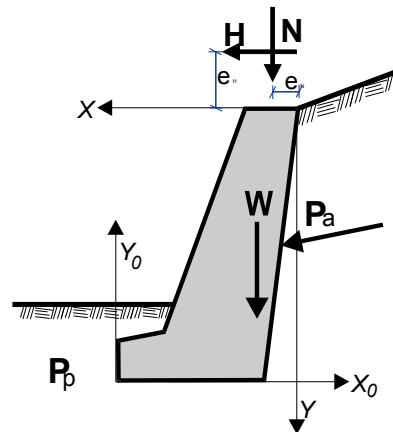
(EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002, EC7 EN1997-1-1:2004, EC8 EN1998-5:2004)



2.1. Wall properties-Parameters-Code requirements

Dimensions

Height of wall	$h = 1.700 \text{ m}$
Transverse length of wall	$L = 10.000 \text{ m}$
Steam thickness at top	$B1 = 0.500 \text{ m}$
Steam thickness at bottom	$B2 = 0.647 \text{ m}$
Width of wall base	$B = 0.750 \text{ m}$
Width of wall toe	0.250 m
Height of wall steam	1.200 m
Thickness of wall footing	0.500 m
Front thickness of wall toe	0.500 m
Slope (batter) at frontface	$22.620^\circ \text{ (1:2.40)}$
Slope (batter) at backface	$-16.390^\circ \text{ (1:3.40)}$



Loads on wall top

Vertical permanent load	$Ng = 5.00 \text{ kN/m}$
Vertical variable load	$Nq = 3.00 \text{ kN/m}$
Eccentricity of vertical load	$eN = 0.25 \text{ kN/m}$
Horizontal permanent load	$Hg = 2.00 \text{ kN/m}$
Horizontal variable load	$Hq = 2.00 \text{ kN/m}$
Eccentricity of horizontal load	$eH = 0.00 \text{ kN/m}$

Weight of wall

Unit weight of wall material	$\gamma_g = 20.000 \text{ kN/m}^3$
Cross section area of wall	$A = 1.100 \text{ m}^2$
Self weight per meter of wall	$W = 1.100 \times 20.000 = 22.00 \text{ kN/m}$
Center of gravity of wall at	$x = 0.609 \text{ m}, y = 0.931 \text{ m} \text{ (} x_o = 0.641 \text{ m}, y_o = 0.769 \text{ m)}$

Wall materials

Allowable compressive stress	3.00 N/mm ²
Allowable tensile stress	0.00 N/mm ²
Allowable shear stress	0.30 N/mm ²

2.2. Partial factors for actions and soil properties

(EC7 Tables A.1-A.4, EC8-5 §3.1)

Equilibrium limit state (EQU), Structural limit state (STR), Geotechnical limit state (GEO)		(EQU)	(STR)	(GEO)	(SEISMIC)
Actions	Permanent Unfavourable	γ_{Gdst} : 1.10	1.35	1.00	1.00
	Permanent Favourable	γ_{Gstb} : 0.90	1.00	1.00	1.00
	Variable Unfavourable	γ_{Qdst} : 1.50	1.50	1.30	1.00
	Variable Favourable	γ_{Qstb} : 0.00	0.00	0.00	0.00
Soil parameters	Angle of shearing resistance	γ_{ϕ} : 1.25	1.00	1.25	1.25
	Effective cohesion	γ_c : 1.25	1.00	1.25	1.25
	Undrained shear strength	γ_{cu} : 1.40	1.00	1.40	1.40
	Unconfined strength	γ_{qu} : 1.40	1.00	1.40	1.40
	Weight density	γ_w : 1.00	1.00	1.00	1.00

2.3. Properties of foundation soil

Bearing capacity of foundation soil	$q_u=0.20$ N/mm ²
Friction angle between wall footing and soil	$\phi=30.00^\circ$, friction coefficient $\tan(\phi)=0.577$
Cohesion between wall footing and soil	$c=0.010$ N/mm ²

2.4. Seismic coefficients

(EC8 EN1998-5:2004, §7.3.2)

Design ground acceleration ratio	$gh=ax_g$, $a=0.06$	(EC8-5 §7.3.2)
Reduction factor for seismic coefficient	$r=1.50$	(EC8-5 Table 7.1)
Coefficient for horizontal seismic force	$kh=0.06/1.500=0.040$	(EC8-5 Eq.7.1)
Coefficient for vertical seismic force	$kv=0.50 \times 0.040=0.020$	(EC8-5 Eq.7.2)

Forces due to seismic load (except from earth pressure)

Horizontal seismic force due to self weight	$F_{wx}= 22.00 \times 0.040=$	0.88 kN/m
Vertical seismic force due to self weight	$F_{wy}= 22.00 \times 0.020=$	0.44 kN/m
Horizontal seismic force of top loading N_g	$F_{gx}= 5.00 \times 0.040=$	0.20 kN/m
Vertical seismic force of top loading N_g	$F_{gy}= 5.00 \times 0.020=$	0.10 kN/m
Horizontal seismic force of top loading N_q	$F_{qx}= 3.00 \times 0.040=$	0.12 kN/m
Vertical seismic force of top loading N_q	$F_{qy}= 3.00 \times 0.020=$	0.06 kN/m

2.5. Computation of active earth pressure (Coulomb theory)

2.5.1. Wall part from $y=0.000$ m to $y=0.900$ m, $H_s=0.900$ m

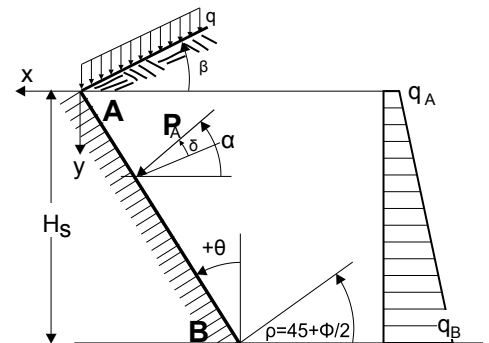
Top point A $x= 0.000$ m $y= 0.000$ m
 Bottom point B $x= 0.265$ m $y= 0.900$ m

Soil properties

Soil type	: Mean gravel
Unit weight of soil	$\gamma =16.00$ kN/m ³
Unit weight of soil (saturated)	$\gamma_s=20.00$ kN/m ³
Unit weight of water	$\gamma_w=10.00$ kN/m ³
Angle of shearing resistance of ground	$\phi=40.00^\circ$
Cohesion of ground	$c=0.000$ N/mm ²
Slope angle of ground surface	$\beta= 8.00^\circ$
Inclination angle of the wall backface	$\theta=-16.39^\circ$
Angle of shear resist. between ground-wall	$\delta=20.00^\circ$

Loads on soil surface

Permanent uniform load	$g= 0.00$ kN/m ²
Variable uniform load	$q= 3.00$ kN/m ²



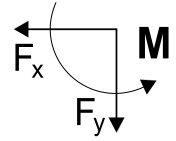
Earth pressure according to Coulomb theory

Angle of rupture plane $\rho=45^\circ+\phi/2 = 61.00$ EQU STR GEO
 Coefficient of active earth pressure $K_a= 0.193$ 0.114 0.193
 Earth pressure $q(y)=q_A+\gamma \cdot y \cdot K_a$

$$K_A = \frac{\cos^2(\varphi-\theta)}{\cos^2\theta \cos(\theta+\delta) \left[1 + \sqrt{\frac{\sin(\theta+\delta)\sin(\theta-\beta)}{\cos(\theta+\delta)\cos(\theta-\beta)}} \right]^2}$$

Permanent actions

	EQU	STR	GEO
Earth pressure at the top (y=yA)	qA= 0.00	0.00	0.00 kN/m ²
Earth pressure at the bottom (y=yA+ 0.90m)	qB= 2.78	1.64	2.78 kN/m ²
Earth force $P_a=\frac{1}{2}(q_A+q_B)H$	Pa= 1.25	0.74	1.25 kN/m
Angle of earth force	$\alpha = 2.89$	3.61	2.89 °
Earth force in x direction	Pax= 1.25	0.74	1.25 kN/m
Earth force in y direction	Pay= 0.08	0.05	0.08 kN/m
Moment of earth force at top point (x=0,y=0)	M = -0.74	-0.44	-0.74 kNm/m
Point of application of earth force x= 0.176 m, y= 0.600 m			



Variable actions

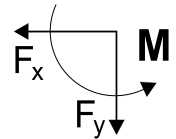
	EQU	STR	GEO
Earth pressure at the top (y=yA)	qA= 0.60	0.36	0.60 kN/m ²
Earth pressure at the bottom (y=yA+ 0.90m)	qB= 0.60	0.36	0.60 kN/m ²
Earth force $P_a=\frac{1}{2}(q_A+q_B)H$	Pa= 0.54	0.32	0.54 kN/m
Angle of earth force	$\alpha = 2.89$	3.61	2.89 °
Earth force in x direction	Pax= 0.54	0.32	0.54 kN/m
Earth force in y direction	Pay= 0.03	0.02	0.03 kN/m
Moment of earth force at top point (x=0,y=0)	M = -0.24	-0.14	-0.24 kNm/m
Point of application of earth force x= 0.132 m, y= 0.450 m			

Total forces and moments

Forces and moments at bottom point B (x=0.265 m, y=0.900 m)

Permanent actions

	EQU	STR	GEO
Total horizontal earth force $F_{sx} =$	1.25	0.74	1.25 kN/m
Total vertical earth force $F_{sy} =$	0.08	0.05	0.08 kN/m
Total moment of earth force $M_s =$	0.37	0.22	0.37 kNm/m



Variable actions

	EQU	STR	GEO
Total horizontal earth force $F_{sx} =$	0.54	0.32	0.54 kN/m
Total vertical earth force $F_{sy} =$	0.03	0.02	0.03 kN/m
Total moment of earth force $M_s =$	0.24	0.14	0.24 kNm/m

Seismic loading

(EC8 EN1998-5:2004, §7.3.2, Annex E)

Horizontal seismic coefficient $k_h=0.06/1.500=0.040$ (EC8-5 Eq.7.1, T.7.1)
 Vertical seismic coefficient $k_v=0.50 \times 0.040=0.020$ (EC8-5 Eq.7.2)
 Soil above the water table (EC8-5 Annex E.5)
 $\tan(\omega)=k_h/(1-k_v)=0.040/(1-0.020)=0.041, \omega=2.34^\circ$

Method Mononobe-Okabe (EC8-5 Annex E.4)
 for active earth force during seismic loading
 Coefficient of active earth pressure, $K_e^* = 0.213$
 Additional earth pressure due to seismic load
 over STR load case $\xi=(K_e^*/K_e-1)=(0.213/0.114-1)=0.868$

$$K_E = \frac{\cos^2(\varphi-\omega-\theta)}{\cos\omega \cos^2\theta \cos(\delta+\theta+\omega) \left[1 + \sqrt{\frac{\sin(\varphi+\delta)\sin(\varphi-\omega-\beta)}{\cos(\theta+\omega+\delta)\cos(\theta-\beta)}} \right]^2}$$

Earth force due to seismic load (Permanent actions) $F_x=1.868 \times 0.74 = 1.38$ kN/m
 Earth force due to seismic load (Variable actions) $F_x=1.868 \times 0.32 = 0.60$ kN/m

Seismic loading

(EC8 EN1998-5:2004, §7.3.2, Annex E)

Horizontal seismic coefficient $k_h=0.06/1.500=0.040$
 Vertical seismic coefficient $k_v=0.50 \times 0.040=0.020$
 Soil above the water table
 $\tan(\omega)=k_h/(1-k_v)=0.040/(1-0.020)=0.041, \omega=2.34^\circ$

(EC8-5 Eq.7.1, T.7.1)
 (EC8-5 Eq.7.2)
 (EC8-5 Annex E.5)

Method Mononobe-Okabe (EC8-5 Annex E.4)
 for active earth force during seismic loading
 Coefficient of active earth pressure, $K_e^*=0.195$
 Additional earth pressure due to seismic load
 over STR load case $\xi=(K_e^*/K_e-1)=(0.195/0.107-1)=0.822$

$$K_E = \frac{\cos^2(\varphi-\omega-\theta)}{\cos\omega \cos^2\theta \cos(\delta+\theta+\omega) \left[1 + \sqrt{\frac{\sin(\varphi+\delta)\sin(\varphi-\omega-\beta)}{\cos(\theta+\omega+\delta)\cos(\theta-\beta)}} \right]^2}$$

Earth force due to seismic load (Permanent actions) $F_x=1.822 \times 1.78= 3.24 \text{ kN/m}$
 Earth force due to seismic load (Variable actions) $F_x=1.822 \times 0.26= 0.47 \text{ kN/m}$

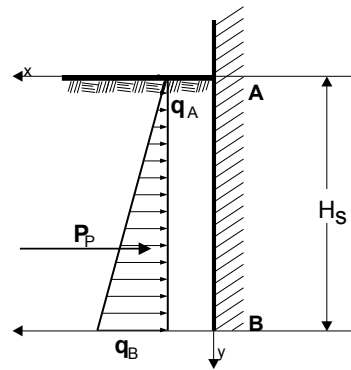
2.6. Computation of passive earth pressure (Rankine theory)

2.6.1. Wall part from $y=1.200 \text{ m}$ to $y=1.700 \text{ m}$, $H_s=0.500 \text{ m}$

Top point A $x= 1.250 \text{ m}$ $y= 1.200 \text{ m}$
 Bottom point B $x= 1.250 \text{ m}$ $y= 1.700 \text{ m}$

Soil properties

Soil type : Dense sand
 Unit weight of soil $\gamma = 17.00 \text{ kN/m}^3$
 Unit weight of soil (saturated) $\gamma_s = 20.00 \text{ kN/m}^3$
 Unit weight of water $\gamma_w = 10.00 \text{ kN/m}^3$
 Soil under the water table lever
 Soil weight suspended in water $\gamma_o = 10.00 \text{ kN/m}^3$
 Angle of shearing resistance of ground $\varphi = 35.00^\circ$
 Cohesion of ground $c = 0.010 \text{ N/mm}^2$
 Slope angle of ground surface $\beta = 0.00^\circ$
 Earth pressure on vertical surface $\theta = 0.00^\circ$
 Angle of shear resist. between ground-wall $\delta = 0.00^\circ$



Loads on soil surface

Permanent uniform load $g = 0.00 \text{ kN/m}^2$
 Variable uniform load $q = 0.00 \text{ kN/m}^2$
 Water pressure at the top $q_w = 0.00 \text{ kN/m}^2$

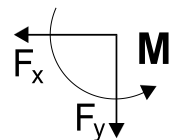
Earth pressure according to Coulomb theory

Angle of rupture plane $\rho = 45^\circ - \varphi/2 = 31.00$ EQU STR GEO 31.00°
 Coefficient of passive earth pressure $K_p = 2.770$ 3.690 2.770
 Earth pressure $q(y) = q_A + \gamma \cdot y \cdot K_p$

$$K_p = \frac{\cos^2(\varphi+\theta)}{\cos^2\theta \cos(\theta-\delta) \left[1 - \sqrt{\frac{\sin(\theta+\delta)\sin(\theta+\beta)}{\cos(\theta-\delta)\cos(\theta-\beta)}} \right]^2}$$

Permanent actions

	EQU	STR	GEO
Earth pressure at the top ($y=y_A$)	$q_A = 0.00$	0.00	0.00 kN/m^2
Earth pressure at the bottom ($y=y_A + 0.50\text{m}$)	$q_B = -13.85$	-18.45	-13.85 kN/m^2
Earth force $P_a = \frac{1}{2}(q_A + q_B)H$	$P_p = 3.46$	4.61	3.46 kN/m
Angle of earth force	$\alpha = 0.00$	0.00	0.00°
Earth force in x direction	$P_{px} = -3.46$	-4.61	-3.46 kN/m
Earth force in y direction	$P_{py} = 0.00$	0.00	0.00 kN/m
Moment of earth force at top point ($x=0, y=0$)	$M = 5.30$	7.07	5.30 kNm/m
Point of application of earth force $x= 1.250 \text{ m}$, $y= 1.533 \text{ m}$			



Hydrostatic pressure

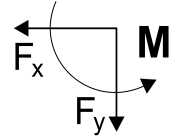
Hydrostatic pressure $q_w = q_wA + \gamma_w \cdot H_w / \cos\theta$
 Hydrostatic pressure at the top ($y=yA$) $q_wA = 0.00 \text{ kN/m}^2$
 Hydrostatic pressure at the bottom ($y=yA + 0.50\text{m}$) $q_wB = 5.00 \text{ kN/m}^2$
 Hydrostatic force $P_w = \frac{1}{2}(q_wA + q_wB)H$ $P_w = 1.25 \text{ kN/m}$
 Angle of hydrostatic force $\alpha = 0.00^\circ$
 Hydrostatic force in x direction $P_{wx} = 1.25 \text{ kN/m}$
 Hydrostatic force in y direction $P_{wy} = 0.00 \text{ kN/m}$
 Moment of hydrostatic force at top point ($x=0, y=0$) $M = -1.92 \text{ kNm/m}$
 Point of application of hydrostatic force $x = 1.250 \text{ m}, y = 1.533 \text{ m}$

Total forces and moments

Forces and moments at bottom point B ($x=1.250 \text{ m}, y=1.700 \text{ m}$)

Permanent actions

	EQU	STR	GEO
Total horizontal earth force $F_{sx} =$	-3.46	-4.61	-3.46 kN/m
Total vertical earth force $F_{sy} =$	0.00	0.00	0.00 kN/m
Total moment of earth force $M_s =$	-0.58	-0.77	-0.58 kNm/m



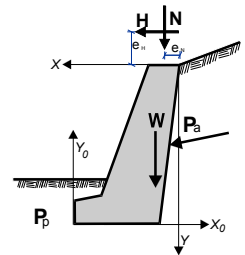
Hydrostatic pressure

Total horizontal hydrostatic force $F_{wx} = 1.25 \text{ kN/m}$
 Total vertical hydrostatic force $F_{wy} = 0.00 \text{ kN/m}$
 Total moment of hydrostatic force $M_w = 0.21 \text{ kNm/m}$

2.7. Checks of wall stability (EQU)

2.7.1. Forces (driving and resisting) on the wall (EQU)

Action	$y1 - y2$	F_x	F_y	x	y	
		[kN/m]		[kN/m]	[m]	[m]
Active earth pressure	Pa 0.00- 0.90	1.25	0.00	0.08	0.176	0.600
Backfill surcharge (live)	Pq 0.00- 0.90	0.54	0.00	0.03	0.132	0.450
Active earth pressure	Pa 0.90- 1.70	2.95	0.00	0.19	0.395	1.341
Backfill surcharge (live)	Pq 0.90- 1.70	0.42	0.00	0.03	0.383	1.300
Passive earth pressure	Pp 1.20- 1.70	-3.46	0.00	1.250	1.533	
Wall weight	W	0.00	22.00	0.609	0.931	
Vert. load on top (dead)	Ng	0.00	5.00	0.250	0.000	
Vert. load on top (live)	Nq	0.00	3.00	0.250	0.000	
Horiz. load on top (dead)	Hg	2.00	0.00	0.250	0.000	
Horiz. load on top (live)	Hq	2.00	0.00	0.250	0.000	

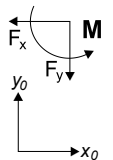


2.7.2. Check of soil bearing capacity (EQU)

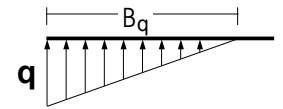
(EC7 EN1997-1-1:2004, §6.5.2)

Check for $0.90 \times (\text{self weight} + \text{top vertical dead load}) + 0.00 \times (\text{top vertical live load})$

Action	(γ)	$y1 - y2$	F_x	F_y	x_0	y_0	M
			[kN/m]		[kN/m]	[m]	[kNm/m]
Active earth pressure	Pax1.10	0.00- 0.90	1.38	0.00	1.074	1.100	1.42
Backfill surcharge (live)	Pqx1.50	0.00- 0.90	0.81	0.00	1.118	1.250	0.98
Active earth pressure	Pax1.10	0.90- 1.70	3.25	0.00	0.855	0.359	0.99
Backfill surcharge (live)	Pqx1.50	0.90- 1.70	0.63	0.00	0.867	0.400	0.21
Wall weight	W x0.90		0.00	19.80	0.641	0.769	-12.69
Vert. load on top (dead)	Ngx0.90		0.00	4.50	1.000	1.700	-4.50
Horiz. load on top (dead)	Hgx1.10		2.20	0.00	1.000	1.700	3.74
Horiz. load on top (live)	Hqx1.50		3.00	0.00	1.000	1.700	5.10
			Sum=		24.68		-4.75



Sum of vertical forces = 24.68 kN/m
 Sum of moments at front toe = -4.75 kNm/m
 Sum of moments at middle of base = 4.50 kNm/m
 Eccentricity $ec=4.50/24.68=0.182m$, $ec>0.750/6=0.125m$
 Soil pressure $q=0.085 \text{ N/mm}^2$ $Bq=0.578 \text{ m}$
 Effective footing $L=0.750-2 \times 0.182= 0.385 \text{ m}$
 Soil bearing capacity $Rd=L \cdot qu/\gamma M=0.385 \times (1000 \times 0.20)/1.40= 55.00 \text{ kN/m}$
 Bearing resistance check $Vd=24.68 < Rd=55.00 \text{ kN/m}$, Check is verified



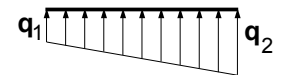
(EC7 Annex D)

(EC7 Eq.2.2, Eq.6.1)

Check for 1.10x(self weight+top vertical dead load)+1.50x(top vertical live load)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.10	0.00- 0.90		1.38	0.09	1.074	1.100	1.42
Backfill surcharge (live)	Pqx1.50	0.00- 0.90		0.81	0.04	1.118	1.250	0.98
Active earth pressure	Pax1.10	0.90- 1.70		3.25	0.21	0.855	0.359	0.99
Backfill surcharge (live)	Pqx1.50	0.90- 1.70		0.63	0.04	0.867	0.400	0.21
Wall weight	W x1.10			0.00	24.20	0.641	0.769	-15.51
Vert. load on top (dead)	Ngx1.10			0.00	5.50	1.000	1.700	-5.50
Vert. load on top (live)	Nqx1.50			0.00	4.50	1.000	1.700	-4.50
Horiz. load on top (dead)	Hgx1.10			2.20	0.00	1.000	1.700	3.74
Horiz. load on top (live)	Hqx1.50			3.00	0.00	1.000	1.700	5.10
				Sum=	34.58			-13.07

Sum of vertical forces = 34.58 kN/m
 Sum of moments at front toe = -13.07 kNm/m
 Sum of moments at middle of base = -0.10 kNm/m
 Eccentricity $ec=-0.10/34.58=-0.003m$, $ec \leq 0.750/6=0.125m$
 Soil pressure $q1=0.045 \text{ N/mm}^2$ $q2=0.047 \text{ N/mm}^2$
 Effective footing $L=0.750-2 \times 0.003= 0.744 \text{ m}$
 Soil bearing capacity $Rd=L \cdot qu/\gamma M=0.744 \times (1000 \times 0.20)/1.40= 106.29 \text{ kN/m}$
 Bearing resistance check $Vd=34.58 < Rd=106.29 \text{ kN/m}$, Check is verified



(EC7 Annex D)

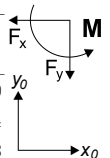
(EC7 Eq.2.2, Eq.6.1)

2.7.3. Failure check due to overturning (EQU)

(EC7 EN1997-1-1:2004, §9.7.4)

Overturning with respect to the toe ($xo=0, yo=0$) ($x=1.250, y=1.700 \text{ m}$)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	Mo+	Mo-	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]	[kNm/m]
Active earth pressure	Pax1.10	0.00- 0.90		1.38	0.09	1.074	1.100	1.52	0.10
Backfill surcharge (live)	Pqx1.50	0.00- 0.90		0.81	0.04	1.118	1.250	1.02	0.04
Active earth pressure	Pax1.10	0.90- 1.70		3.25	0.21	0.855	0.359	1.17	0.18
Backfill surcharge (live)	Pqx1.50	0.90- 1.70		0.63	0.04	0.867	0.400	0.26	0.04
Wall weight	W x0.90			0.00	19.80	0.641	0.769	0.00	12.69
Vert. load on top (dead)	Ngx0.90			0.00	4.50	1.000	1.700	0.00	4.50
Horiz. load on top (dead)	Hgx1.10			2.20	0.00	1.000	1.700	3.74	0.00
Horiz. load on top (live)	Hqx1.50			3.00	0.00	1.000	1.700	5.10	0.00
							Sum=	12.81	17.55

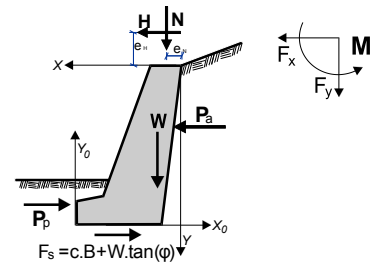


Sum of overturning moments = 12.81 kNm/m
 Sum of moments resisting overturning = 17.55 kNm/m
 Overturning check $Msd=12.81 < Mrd=17.55 \text{ kNm/m}$, Check is verified

2.7.4. Failure check against sliding (EQU)

(EC7 EN1997-1-1:2004, §9.7.3, §6.5.3)

Action	(γ)	y1 - y2	Fx+	Fx-	Fy
			[kN/m]	[kN/m]	[kN/m]
Active earth pressure	Pax1.10	0.00- 0.90	1.38	0.00	0.09
Backfill surcharge (live)	Pqx1.50	0.00- 0.90	0.81	0.00	0.04
Active earth pressure	Pax1.10	0.90- 1.70	3.25	0.00	0.21
Backfill surcharge (live)	Pqx1.50	0.90- 1.70	0.63	0.00	0.04
Passive earth pressure	Ppx0.90	1.20- 1.70	0.00	3.11	0.00
Wall weight	W x0.90		0.00	0.00	19.80
Vert. load on top (dead)	Ngx0.90		0.00	0.00	4.50
Horiz. load on top (dead)	Hgx1.10		2.20	0.00	0.00
Horiz. load on top (live)	Hqx1.50		3.00	0.00	0.00
Sum=			11.27	3.11	24.68



Soil friction $Rd = Vd \cdot \tan\phi / \gamma M = 24.68 \times \tan(30.00^\circ) / 1.25 = 11.40$ kN/m

Soil cohesion $Rd = A \cdot cu / \gamma M = 1000 \times 0.578 \times 0.010 / 1.25 = 4.62$ kN/m

(resisting forces from effective cohesion are neglected)

Sum of driving forces = 11.27 kN/m

Sum of resisting forces (3.11+11.40) = 14.51 kN/m

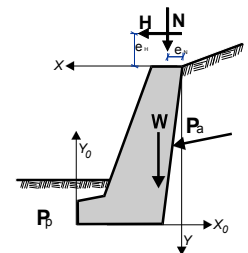
Sliding resistance check $Hd = 11.27 < Rd = 14.51$ kN/m, Check is verified

(EC7 §6.5.3. 10)

2.8. Checks of wall stability (STR)

2.8.1. Forces (driving and resisting) on the wall (STR)

Action	y1 - y2	Fx	Fy	x	y
		[kN/m]	[kN/m]	[m]	[m]
Active earth pressure	Pa 0.00- 0.90	0.74	0.05	0.176	0.600
Backfill surcharge (live)	Pq 0.00- 0.90	0.32	0.02	0.132	0.450
Active earth pressure	Pa 0.90- 1.70	1.78	0.11	0.395	1.341
Backfill surcharge (live)	Pq 0.90- 1.70	0.26	0.02	0.383	1.300
Passive earth pressure	Pp 1.20- 1.70	-4.61	0.00	1.250	1.533
Wall weight	W	0.00	22.00	0.609	0.931
Vert. load on top (dead)	Ng	0.00	5.00	0.250	0.000
Vert. load on top (live)	Nq	0.00	3.00	0.250	0.000
Horiz. load on top (dead)	Hg	2.00	0.00	0.250	0.000
Horiz. load on top (live)	Hq	2.00	0.00	0.250	0.000

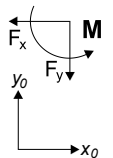


2.8.2. Check of soil bearing capacity (STR)

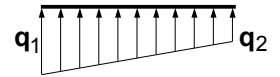
(EC7 EN1997-1-1:2004, §6.5.2)

Check for $1.00 \times (\text{self weight} + \text{top vertical dead load}) + 0.00 \times (\text{top vertical live load})$

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M
			[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.35	0.00- 0.90	1.00	0.07	1.074	1.100	1.03
Backfill surcharge (live)	Pqx1.50	0.00- 0.90	0.48	0.03	1.118	1.250	0.57
Active earth pressure	Pax1.35	0.90- 1.70	2.40	0.15	0.855	0.359	0.74
Backfill surcharge (live)	Pqx1.50	0.90- 1.70	0.39	0.03	0.867	0.400	0.12
Wall weight	W x1.00		0.00	22.00	0.641	0.769	-14.10
Vert. load on top (dead)	Ngx1.00		0.00	5.00	1.000	1.700	-5.00
Horiz. load on top (dead)	Hgx1.35		2.70	0.00	1.000	1.700	4.59
Horiz. load on top (live)	Hqx1.50		3.00	0.00	1.000	1.700	5.10
Sum=				27.28			-6.95



Sum of vertical forces = 27.28 kN/m
 Sum of moments at front toe = -6.95 kNm/m
 Sum of moments at middle of base = 3.28 kNm/m
 Eccentricity $ec=3.28/27.28=0.120m$, $ec<=0.750/6=0.125m$
 Soil pressure $q_1=0.071$ N/mm² $q_2=0.001$ N/mm²
 Effective footing $L=0.750-2x0.120= 0.510$ m
 Soil bearing capacity $Rd=L \cdot q_u / \gamma M = 0.510x(1000x0.20) / 1.00 = 102.00$ kN/m
 Bearing resistance check $Vd=27.28 < Rd=102.00$ kN/m, Check is verified



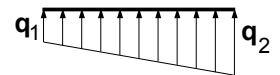
(EC7 Annex D)

(EC7 Eq.2.2, Eq.6.1)

Check for 1.35x(self weight+top vertical dead load)+1.50x(top vertical live load)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.35	0.00- 0.90		1.00	0.07	1.074	1.100	1.03
Backfill surcharge (live)	Pqx1.50	0.00- 0.90		0.48	0.03	1.118	1.250	0.57
Active earth pressure	Pax1.35	0.90- 1.70		2.40	0.15	0.855	0.359	0.74
Backfill surcharge (live)	Pqx1.50	0.90- 1.70		0.39	0.03	0.867	0.400	0.12
Wall weight	W x1.35			0.00	29.70	0.641	0.769	-19.04
Vert. load on top (dead)	Ngx1.35			0.00	6.75	1.000	1.700	-6.75
Vert. load on top (live)	Nqx1.50			0.00	4.50	1.000	1.700	-4.50
Horiz. load on top (dead)	Hgx1.35			2.70	0.00	1.000	1.700	4.59
Horiz. load on top (live)	Hqx1.50			3.00	0.00	1.000	1.700	5.10
				Sum=	41.23			-18.14

Sum of vertical forces = 41.23 kN/m
 Sum of moments at front toe = -18.14 kNm/m
 Sum of moments at middle of base = -2.68 kNm/m
 Eccentricity $ec=-2.68/41.23=-0.065m$, $ec<=0.750/6=0.125m$
 Soil pressure $q_1=0.026$ N/mm² $q_2=0.084$ N/mm²
 Effective footing $L=0.750-2x0.065= 0.620$ m
 Soil bearing capacity $Rd=L \cdot q_u / \gamma M = 0.620x(1000x0.20) / 1.00 = 124.00$ kN/m
 Bearing resistance check $Vd=41.23 < Rd=124.00$ kN/m, Check is verified



(EC7 Annex D)

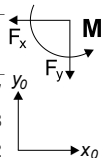
(EC7 Eq.2.2, Eq.6.1)

2.8.3. Failure check due to overturning (STR)

(EC7 EN1997-1-1:2004, §9.7.4)

Overturning with respect to the toe ($x_o=0, y_o=0$) ($x=1.250, y=1.700$ m)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	Mo+	Mo-	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]	[kNm/m]
Active earth pressure	Pax1.35	0.00- 0.90		1.00	0.07	1.074	1.100	1.09	0.07
Backfill surcharge (live)	Pqx1.50	0.00- 0.90		0.48	0.03	1.118	1.250	0.60	0.03
Active earth pressure	Pax1.35	0.90- 1.70		2.40	0.15	0.855	0.359	0.86	0.12
Backfill surcharge (live)	Pqx1.50	0.90- 1.70		0.39	0.03	0.867	0.400	0.15	0.03
Wall weight	W x1.00			0.00	22.00	0.641	0.769	0.00	14.10
Vert. load on top (dead)	Ngx1.00			0.00	5.00	1.000	1.700	0.00	5.00
Horiz. load on top (dead)	Hgx1.35			2.70	0.00	1.000	1.700	4.59	0.00
Horiz. load on top (live)	Hqx1.50			3.00	0.00	1.000	1.700	5.10	0.00
							Sum=	12.39	19.35

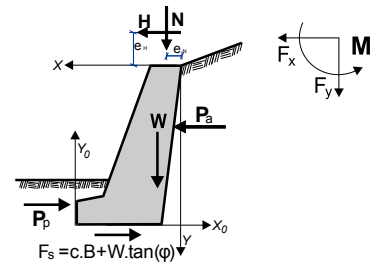


Sum of overturning moments = 12.39 kNm/m
 Sum of moments resisting overturning = 19.35 kNm/m
 Overturning check $Msd=12.39 < Mrd=19.35$ kNm/m, Check is verified

2.8.4. Failure check against sliding (STR)

(EC7 EN1997-1-1:2004, §9.7.3, §6.5.3)

Action	(γ)	y1 - y2	Fx+	Fx-	Fy
			[kN/m]	[kN/m]	[kN/m]
Active earth pressure	Pax1.35	0.00- 0.90	1.00	0.00	0.07
Backfill surcharge (live)	Pqx1.50	0.00- 0.90	0.48	0.00	0.03
Active earth pressure	Pax1.35	0.90- 1.70	2.40	0.00	0.15
Backfill surcharge (live)	Pqx1.50	0.90- 1.70	0.39	0.00	0.03
Passive earth pressure	Ppx1.00	1.20- 1.70	0.00	4.61	0.00
Wall weight	W x1.00		0.00	0.00	22.00
Vert. load on top (dead)	Ngx1.00		0.00	0.00	5.00
Horiz. load on top (dead)	Hgx1.35		2.70	0.00	0.00
Horiz. load on top (live)	Hqx1.50		3.00	0.00	0.00
Sum=			9.97	4.61	27.28



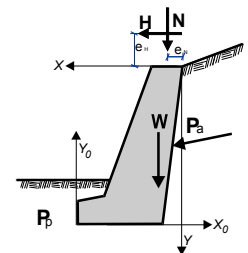
Soil friction $Rd = Vd \cdot \tan\phi / \gamma M = 27.28 \times \tan(30.00^\circ) / 1.00 = 15.75 \text{ kN/m}$
 Soil cohesion $Rd = A \cdot cu / \gamma M = 1000 \times 0.750 \times 0.010 / 1.00 = 7.50 \text{ kN/m}$
 (resisting forces from effective cohesion are neglected)
 Sum of driving forces = 9.97 kN/m
 Sum of resisting forces (4.61+15.75) = 20.36 kN/m
 Sliding resistance check $Hd = 9.97 < Rd = 20.36 \text{ kN/m}$, Check is verified

(EC7 §6.5.3. 10)

2.9. Checks of wall stability (GEO)

2.9.1. Forces (driving and resisting) on the wall (GEO)

Action		y1 - y2	Fx	Fy	x	y
			[kN/m]	[kN/m]	[m]	[m]
Active earth pressure	Pa	0.00- 0.90	1.25	0.08	0.176	0.600
Backfill surcharge (live)	Pq	0.00- 0.90	0.54	0.03	0.132	0.450
Active earth pressure	Pa	0.90- 1.70	2.95	0.19	0.395	1.341
Backfill surcharge (live)	Pq	0.90- 1.70	0.42	0.03	0.383	1.300
Passive earth pressure	Pp	1.20- 1.70	-3.46	0.00	1.250	1.533
Wall weight	W		0.00	22.00	0.609	0.931
Vert. load on top (dead)	Ng		0.00	5.00	0.250	0.000
Vert. load on top (live)	Nq		0.00	3.00	0.250	0.000
Horiz. load on top (dead)	Hg		2.00	0.00	0.250	0.000
Horiz. load on top (live)	Hq		2.00	0.00	0.250	0.000

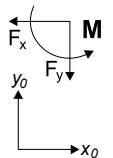


2.9.2. Check of soil bearing capacity (GEO)

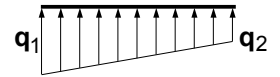
(EC7 EN1997-1-1:2004, §6.5.2)

Check for $1.00 \times (\text{self weight} + \text{top vertical dead load}) + 0.00 \times (\text{top vertical live load})$

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M
			[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.00	0.00- 0.90	1.25	0.08	1.074	1.100	1.29
Backfill surcharge (live)	Pqx1.30	0.00- 0.90	0.70	0.04	1.118	1.250	0.84
Active earth pressure	Pax1.00	0.90- 1.70	2.95	0.19	0.855	0.359	0.90
Backfill surcharge (live)	Pqx1.30	0.90- 1.70	0.55	0.04	0.867	0.400	0.18
Wall weight	W x1.00		0.00	22.00	0.641	0.769	-14.10
Vert. load on top (dead)	Ngx1.00		0.00	5.00	1.000	1.700	-5.00
Horiz. load on top (dead)	Hgx1.00		2.00	0.00	1.000	1.700	3.40
Horiz. load on top (live)	Hqx1.30		2.60	0.00	1.000	1.700	4.42
Sum=				27.35			-8.07



Sum of vertical forces = 27.35 kN/m
 Sum of moments at front toe = -8.07 kNm/m
 Sum of moments at middle of base = 2.19 kNm/m
 Eccentricity $ec=2.19/27.35=0.080m$, $ec<=0.750/6=0.125m$
 Soil pressure $q1=0.060$ N/mm² $q2=0.013$ N/mm²
 Effective footing $L=0.750-2x0.080=0.590$ m
 Soil bearing capacity $Rd=L \cdot qu/\gamma M=0.590x(1000x0.20)/1.40=84.29$ kN/m
 Bearing resistance check $Vd=27.35 < Rd=84.29$ kN/m, Check is verified



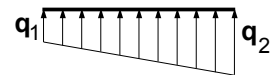
(EC7 Annex D)

(EC7 Eq.2.2, Eq.6.1)

Check for 1.00x(self weight+top vertical dead load)+1.30x(top vertical live load)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.00	0.00- 0.90		1.25	0.08	1.074	1.100	1.29
Backfill surcharge (live)	Pqx1.30	0.00- 0.90		0.70	0.04	1.118	1.250	0.84
Active earth pressure	Pax1.00	0.90- 1.70	2.95		0.19	0.855	0.359	0.90
Backfill surcharge (live)	Pqx1.30	0.90- 1.70	0.55		0.04	0.867	0.400	0.18
Wall weight	W x1.00			0.00	22.00	0.641	0.769	-14.10
Vert. load on top (dead)	Ngx1.00			0.00	5.00	1.000	1.700	-5.00
Vert. load on top (live)	Nqx1.30			0.00	3.90	1.000	1.700	-3.90
Horiz. load on top (dead)	Hgx1.00		2.00		0.00	1.000	1.700	3.40
Horiz. load on top (live)	Hqx1.30		2.60		0.00	1.000	1.700	4.42
				Sum=	31.25			-11.97

Sum of vertical forces = 31.25 kN/m
 Sum of moments at front toe = -11.97 kNm/m
 Sum of moments at middle of base = -0.25 kNm/m
 Eccentricity $ec=-0.25/31.25=-0.008m$, $ec<=0.750/6=0.125m$
 Soil pressure $q1=0.039$ N/mm² $q2=0.044$ N/mm²
 Effective footing $L=0.750-2x0.008=0.734$ m
 Soil bearing capacity $Rd=L \cdot qu/\gamma M=0.734x(1000x0.20)/1.40=104.86$ kN/m
 Bearing resistance check $Vd=31.25 < Rd=104.86$ kN/m, Check is verified



(EC7 Annex D)

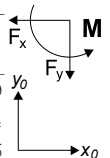
(EC7 Eq.2.2, Eq.6.1)

2.9.3. Failure check due to overturning (GEO)

(EC7 EN1997-1-1:2004, §9.7.4)

Overturning with respect to the toe ($xo=0, yo=0$) ($x=1.250, y=1.700$ m)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	Mo+	Mo-	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]	[kNm/m]
Active earth pressure	Pax1.00	0.00- 0.90		1.25	0.08	1.074	1.100	1.38	0.09
Backfill surcharge (live)	Pqx1.30	0.00- 0.90		0.70	0.04	1.118	1.250	0.88	0.04
Active earth pressure	Pax1.00	0.90- 1.70	2.95		0.19	0.855	0.359	1.06	0.16
Backfill surcharge (live)	Pqx1.30	0.90- 1.70	0.55		0.04	0.867	0.400	0.22	0.04
Wall weight	W x1.00			0.00	22.00	0.641	0.769	0.00	14.10
Vert. load on top (dead)	Ngx1.00			0.00	5.00	1.000	1.700	0.00	5.00
Horiz. load on top (dead)	Hgx1.00		2.00		0.00	1.000	1.700	3.40	0.00
Horiz. load on top (live)	Hqx1.30		2.60		0.00	1.000	1.700	4.42	0.00
							Sum=	11.36	19.43

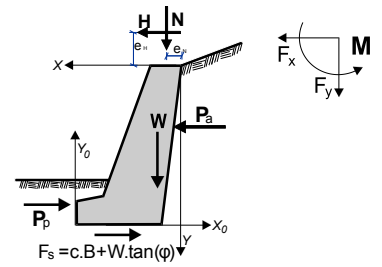


Sum of overturning moments = 11.36 kNm/m
 Sum of moments resisting overturning = 19.43 kNm/m
 Overturning check $Msd=11.36 < Mrd=19.43$ kNm/m, Check is verified

2.9.4. Failure check against sliding (GEO)

(EC7 EN1997-1-1:2004, §9.7.3, §6.5.3)

Action	(γ)	y1 - y2	Fx+	Fx-	Fy
			[kN/m]	[kN/m]	[kN/m]
Active earth pressure	Pax1.00	0.00- 0.90	1.25	0.00	0.08
Backfill surcharge (live)	Pqx1.30	0.00- 0.90	0.70	0.00	0.04
Active earth pressure	Pax1.00	0.90- 1.70	2.95	0.00	0.19
Backfill surcharge (live)	Pqx1.30	0.90- 1.70	0.55	0.00	0.04
Passive earth pressure	Ppx1.00	1.20- 1.70	0.00	3.46	0.00
Wall weight	W x1.00		0.00	0.00	22.00
Vert. load on top (dead)	Ngx1.00		0.00	0.00	5.00
Horiz. load on top (dead)	Hgx1.00		2.00	0.00	0.00
Horiz. load on top (live)	Hqx1.30		2.60	0.00	0.00
		Sum=	10.05	3.46	27.35



Soil friction $Rd = Vd \cdot \tan\phi / \gamma M = 27.35 \times \tan(30.00^\circ) / 1.25 = 12.63$ kN/m

Soil cohesion $Rd = A \cdot cu / \gamma M = 1000 \times 0.750 \times 0.010 / 1.25 = 6.00$ kN/m

(resisting forces from effective cohesion are neglected)

(EC7 §6.5.3. 10)

Sum of driving forces = 10.05 kN/m

Sum of resisting forces (3.46+12.63) = 16.09 kN/m

Sliding resistance check $Hd = 10.05 < Rd = 16.09$ kN/m, Check is verified

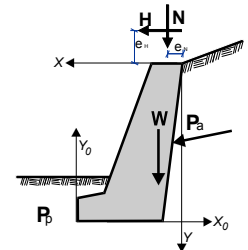
2.10. Seismic design

(EC8 EN1998-5:2004)

Checks of wall stability (with seismic loading)

2.10.1. Forces (driving and resisting) on the wall

Action		y1 - y2	Fx	Fy	x	y
			[kN/m]	[kN/m]	[m]	[m]
Active earth pressure	Pa	0.00- 0.90	0.74	0.05	0.176	0.600
Backfill surcharge (live)	Pq	0.00- 0.90	0.32	0.02	0.132	0.450
Active earth pressure	Pa	0.90- 1.70	1.78	0.11	0.395	1.341
Backfill surcharge (live)	Pq	0.90- 1.70	0.26	0.02	0.383	1.300
Passive earth pressure	Pp	1.20- 1.70	-4.61	0.00	1.250	1.533
Wall weight	W		0.00	22.00	0.609	0.931
Vert. load on top (dead)	Ng		0.00	5.00	0.250	0.000
Vert. load on top (live)	Nq		0.00	3.00	0.250	0.000
Horiz. load on top (dead)	Hg		2.00	0.00	0.250	0.000
Horiz. load on top (live)	Hq		2.00	0.00	0.250	0.000



2.10.2. Additional forces due to seismic load

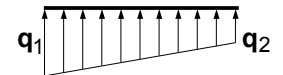
Action		y1 - y2	Fx	Fy	x	y
			[kN/m]	[kN/m]	[m]	[m]
Active earth pressure	Pa	0.00- 0.90	0.64		0.176	0.600
Backfill surcharge (live)	Pq	0.00- 0.90	0.28		0.132	0.450
Active earth pressure	Pa	0.90- 1.70	1.46		0.395	1.341
Backfill surcharge (live)	Pq	0.90- 1.70	0.21		0.383	1.300
Wall weight	W		0.88	-0.44	0.609	0.931
Vert. load on top (dead)	Ng		0.20	-0.10	0.250	0.000
Vert. load on top (live)	Nq		0.12	-0.06	0.250	0.000

2.10.3. Check of soil bearing capacity (with seismic loading)

(EC7 §6.5.2)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.00	0.00- 0.90	1.38	0.05	1.074	1.100	1.46	
Backfill surcharge (live)	Pqx1.00	0.00- 0.90	0.60	0.02	1.118	1.250	0.73	
Active earth pressure	Pax1.00	0.90- 1.70	3.24	0.11	0.855	0.359	1.08	
Backfill surcharge (live)	Pqx1.00	0.90- 1.70	0.47	0.02	0.867	0.400	0.16	
Wall weight	W x1.00		0.88	21.56	0.641	0.769	-13.14	
Vert. load on top (dead)	Ngx1.00		0.20	4.90	1.000	1.700	-4.56	
Vert. load on top (live)	Nqx1.00		0.12	2.94	1.000	1.700	-2.74	
Horiz. load on top (dead)	Hgx1.00		2.00	0.00	1.000	1.700	3.40	
Horiz. load on top (live)	Hqx1.00		2.00	0.00	1.000	1.700	3.40	
			Sum=	29.60			-10.21	

Sum of vertical forces = 29.60 kN/m
 Sum of moments at front toe = -10.21 kNm/m
 Sum of moments at middle of base = 0.89 kNm/m
 Eccentricity $ec=0.89/29.60=0.030m$, $ec\leq 0.750/6=0.125m$
 Soil pressure $q1=0.049 N/mm^2$ $q2=0.030 N/mm^2$
 Effective footing $L=0.750-2x0.030= 0.690 m$
 Soil bearing capacity $Rd=L\cdot qu/\gamma M=0.690x(1000x0.20)/1.00= 138.00 kN/m$
 Bearing resistance check $Vd=29.60 < Rd=138.00 kN/m$, Check is verified



(EC7 Annex D)

(EC7 Eq.2.2, Eq.6.1)

2.10.4. Failure check due to overturning (with seismic loading)

(EC7 §9.7.4)

Overturning with respect to the toe ($xo=0, yo=0$) ($x=1.250, y=1.700 m$)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	Mo+	Mo-
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.00	0.00- 0.90	1.38	0.05	1.074	1.100	1.51	0.05
Backfill surcharge (live)	Pqx1.00	0.00- 0.90	0.60	0.02	1.118	1.250	0.75	0.02
Active earth pressure	Pax1.00	0.90- 1.70	3.24	0.11	0.855	0.359	1.17	0.09
Backfill surcharge (live)	Pqx1.00	0.90- 1.70	0.47	0.02	0.867	0.400	0.18	0.02
Wall weight	W x1.00		0.88	21.56	0.641	0.769	0.96	14.10*
Vert. load on top (dead)	Ngx1.00		0.20	4.90	1.000	1.700	0.44	5.00*
Vert. load on top (live)	Nqx1.00		0.12	2.94	1.000	1.700	0.26	3.00*
Horiz. load on top (dead)	Hgx1.00		2.00	0.00	1.000	1.700	3.40	0.00
Horiz. load on top (live)	Hqx1.00		2.00	0.00	1.000	1.700	3.40	0.00
			Sum=				12.07	22.28

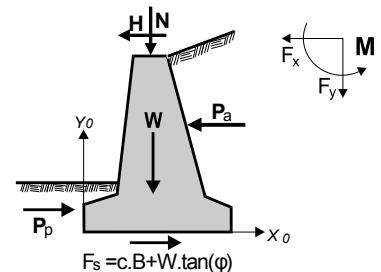
(*moments of negative seismic vertical loads, are added to the overturning moments)

Sum of overturning moments = 12.07 kNm/m
 Sum of moments resisting overturning = 22.28 kNm/m
 Overturning check $Msd=12.07 < Mrd=22.28 kNm/m$, Check is verified

2.10.5. Failure check against sliding (with seismic loading)

(EC7 §9.7.3, §6.5.3)

Action	(γ)	y1 - y2	Fx+	Fx-	Fy	
			[kN/m]	[kN/m]	[kN/m]	
Active earth pressure	Pax1.00	0.00- 0.90	1.38	0.00	0.05	
Backfill surcharge (live)	Pqx1.00	0.00- 0.90	0.60	0.00	0.02	
Active earth pressure	Pax1.00	0.90- 1.70	3.24	0.00	0.11	
Backfill surcharge (live)	Pqx1.00	0.90- 1.70	0.47	0.00	0.02	
Passive earth pressure	Ppx1.00	1.20- 1.70	0.00	4.61	0.00	
Wall weight	W x1.00		0.88	0.00	21.56	
Vert. load on top (dead)	Ngx1.00		0.20	0.00	4.90	
Vert. load on top (live)	Nqx1.00		0.12	0.00	2.94	
Horiz. load on top (dead)	Hgx1.00		2.00	0.00	0.00	
Horiz. load on top (live)	Hqx1.00		2.00	0.00	0.00	
			Sum=	10.89	4.61	29.60



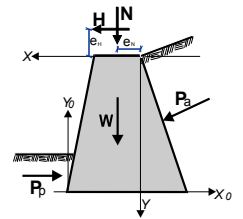
Soil friction $R_d = V_d \cdot \tan \phi / \gamma M = 29.60 \times \tan(30.00^\circ) / 1.00 = 17.09 \text{ kN/m}$
 Soil cohesion $R_d = A \cdot c_u / \gamma M = 1000 \times 0.750 \times 0.010 / 1.00 = 7.50 \text{ kN/m}$
 (resisting forces from effective cohesion are neglected) (EC7 §6.5.3. 10)
 Sum of driving forces = 10.89 kN/m
 Sum of resisting forces (4.61+17.09) = 21.70 kN/m
 Sliding resistance check $H_d = 10.89 < R_d = 21.70 \text{ kN/m}$, Check is verified

2.11. Design of wall steam

2.11.1. Loading 1.35x(permanent unfavourable)+1.00x(permanent favourable)+1.50x(variable unfav.)

Forces (at centroid of cross section) and stresses at wall steam
 x, y: cross section centroid, b: cross section width, e: eccentricity
 Fx: horizontal force, Fy: vertical force, M: moment, e/b: relative eccentricity
 σ_1, σ_2 : cross section normal stresses, τ : shear stress, Bq: effective cross section width

y	x	b	Fx	Fy	M	e/b	σ_1	σ_2	Bq/B	τ
[m]	[m]	[m]	[kN/m]	[kN/m]	[kNm/m]		[N/mm ²]	[N/mm ²]		[N/mm ²]
0.24	0.335	0.529	5.90	7.49	0.46	-0.117	-0.024	-0.004	1.000	0.011
0.48	0.421	0.559	6.24	10.11	0.78	-0.138	-0.033	-0.003	1.000	0.011
0.72	0.506	0.588	6.72	12.91	0.95	-0.125	-0.038	-0.006	1.000	0.011
0.96	0.591	0.618	7.34	15.84	1.02	-0.104	-0.042	-0.010	1.000	0.012
1.20	0.676	0.647	8.06	18.92	1.00	-0.082	-0.044	-0.015	1.000	0.012



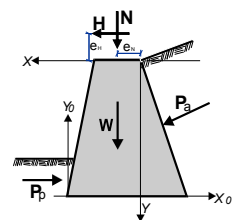
2.11.2. Strength check with allowable stresses

Compression $\sigma_{\max} = 0.044 \leq \sigma(\text{allowable}) = 3.000 \text{ N/mm}^2$
 Tension $\sigma_{\max} = 0.000 \leq \sigma(\text{allowable}) = 0.000 \text{ N/mm}^2$
 Shear $\tau_{\max} = 0.012 \leq \tau(\text{allowable}) = 0.300 \text{ N/mm}^2$

2.11.3. Loading 1.00x(permanent unfav.)+1.00x(permanent favour.)+1.00x(variable)+1.00x(seismic)

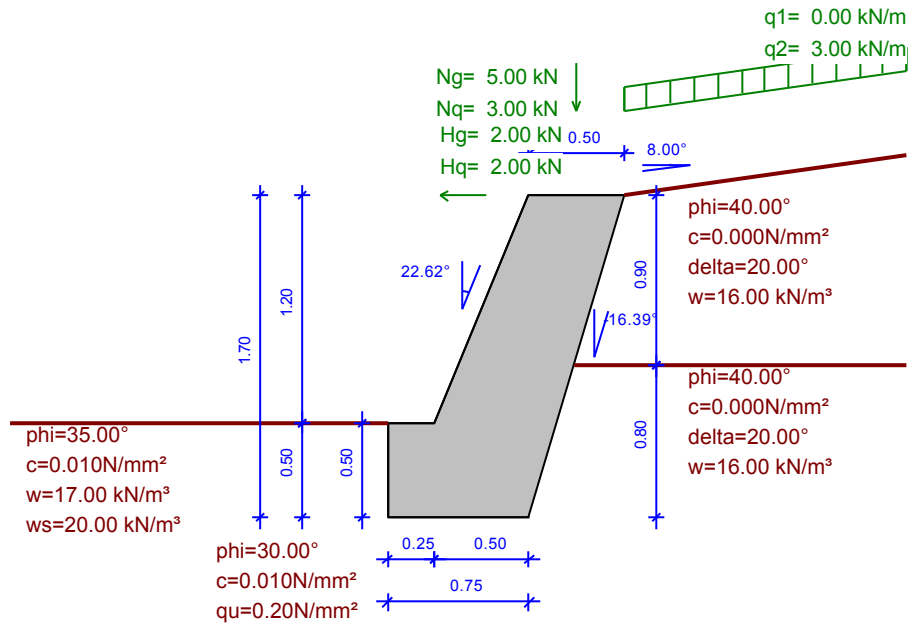
Forces (at centroid of cross section) and stresses at wall steam (with seismic loading)
 x, y: cross section centroid, b: cross section width, e: eccentricity
 Fx: horizontal force, Fy: vertical force, M: moment, e/b: relative eccentricity
 σ_1, σ_2 : cross section normal stresses, τ : shear stress, Bq: effective cross section width

y	x	b	Fx	Fy	M	e/b	σ_1	σ_2	Bq/B	τ
[m]	[m]	[m]	[kN/m]	[kN/m]	[kNm/m]		[N/mm ²]	[N/mm ²]		[N/mm ²]
0.24	0.335	0.529	4.68	10.27	0.30	-0.075	-0.020	-0.008	1.000	0.009
0.48	0.421	0.559	5.23	12.84	0.49	-0.087	-0.028	-0.009	1.000	0.009
0.72	0.506	0.588	6.00	15.57	0.61	-0.081	-0.033	-0.011	1.000	0.010
0.96	0.591	0.618	6.67	18.43	0.57	-0.058	-0.035	-0.017	1.000	0.011
1.20	0.676	0.647	7.74	21.44	0.59	-0.048	-0.038	-0.021	1.000	0.012



2.11.4. Strength check with allowable stresses (with seismic loading)

Compression $\sigma_{\max} = 0.038 \leq \sigma(\text{allowable}) = 3.000 \text{ N/mm}^2$
 Tension $\sigma_{\max} = 0.000 \leq \sigma(\text{allowable}) = 0.000 \text{ N/mm}^2$
 Shear $\tau_{\max} = 0.012 \leq \tau(\text{allowable}) = 0.300 \text{ N/mm}^2$



General information

Wall type : Gravity wall

Wall materials

Allowable compressive stress 3.00 N/mm²

Allowable tensile stress 0.00 N/mm²

Allowable shear stress 0.30 N/mm²

Design codes

Eurocode 0 EN1991-1-1, Basis of structural design

Eurocode 1 EN1991-1-1, Actions on structures

Eurocode 2 EN1992-1-1, Design of concrete structures

Eurocode 7 EN1997-1-1, Geotechnical design

Eurocode 8 EN1998-5, Earthquake design

Loads

Vertical : dead Ng=5.00kN, live Nq=3.00kN

Horizontal: dead Hg=2.00kN, live Hq=2.00kN

Surcharge : dead g=0.00kN/m², live q=3.00kN/m²

Seismic coefficients

Design ground acceleration ratio a =0.060

Coefficient for horizontal seismic force kh=0.040

Coefficient for vertical seismic force kv=0.020

Soil properties back-1

phi=40.00°

c=0.000N/mm²

delta=20.00°

w=16.00 kN/m³

Soil properties back-2

phi=40.00°

c=0.000N/mm²

delta=20.00°

w=16.00 kN/m³

Soil properties front

phi=35.00°

c=0.010N/mm²

w=17.00 kN/m³

ws=20.00 kN/m³

Foundation soil properties

phi=30.00°

c=0.010N/mm²

qu=0.20N/mm²

Concrete volume V= 11.00 [m³]

Project: Example of retaining walls

G. WALL-002

Scale : 1:40

Date: 12/03/2007

Designer:

Draw.No.:

Filename: Example of retaining walls Sign:

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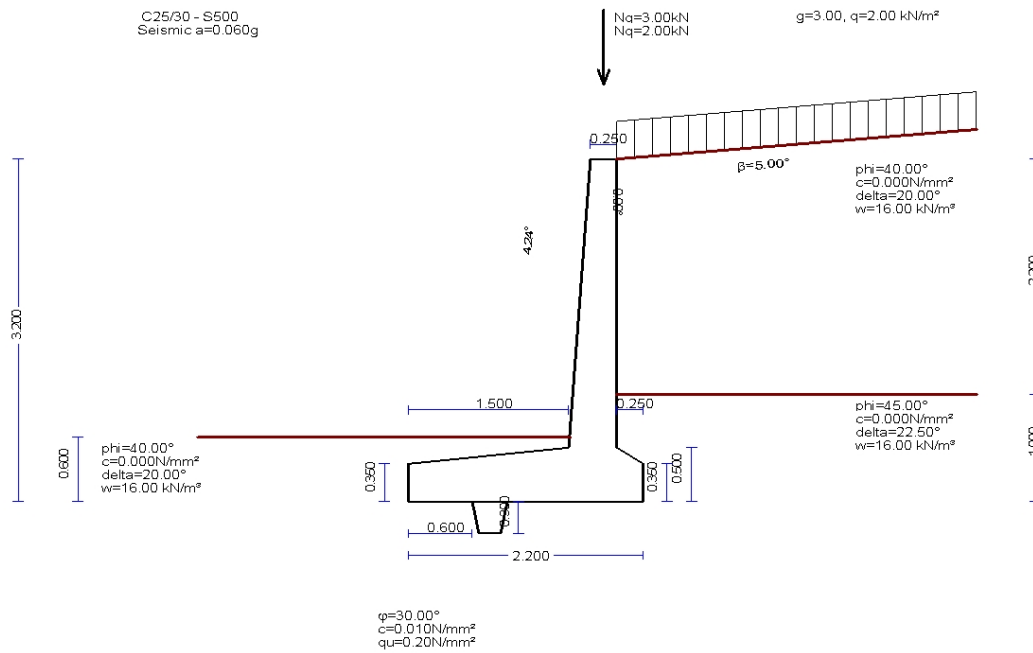
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3. C. WALL-001

Cantilever concrete wall

(EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002, EC7 EN1997-1-1:2004, EC8 EN1998-5:2004)



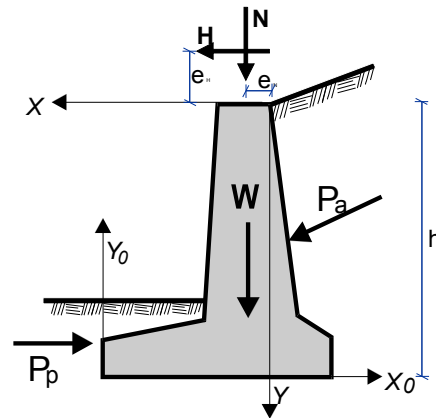
3.1. Wall properties-Parameters-Code requirements

Dimensions

Height of wall	h = 3.200 m
Transverse length of wall	L=10.000 m
Steam thickness at top	B1= 0.250 m
Steam thickness at bottom	B2= 0.450 m
Width of wall base	B= 2.200 m
Width of wall toe	1.500 m
Width of wall heel	0.250 m
Height of wall steam	2.700 m
Thickness of wall footing	0.500 m
Front thickness of wall toe	0.350 m
Back thickness of wall heel	0.350 m
Slope (batter) at frontface	4.236° (1:13.5)
Slope (batter) at backface	0.000° (0:1)
Height of wall base key	0.300 m

Loads on wall top

Vertical permanent load	Ng= 3.00 kN/m
Vertical variable load	Nq= 2.00 kN/m
Eccentricity of vertical load	eN= 0.13 kN/m
Horizontal permanent load	Hg= 0.00 kN/m
Horizontal variable load	Hq= 0.00 kN/m
Eccentricity of horizontal load	eH= 0.00 kN/m



Weight of wall

Unit weight of wall material $\gamma_g=25.000 \text{ kN/m}^3$
 Cross section area of wall $A= 1.914 \text{ m}^2$
 Self weight per meter of wall $W= 1.914 \times 25.000 = 47.85 \text{ kN/m}$
 Center of gravity of wall at $x=0.494 \text{ m}$, $y=2.237 \text{ m}$ ($x_o=1.456 \text{ m}$, $y_o=0.963 \text{ m}$)

Wall materials

Steam : Concrete-Steel class: C25/30-S500 (EN1992-1-1, §3)
 : Concrete cover: $C_{nom}=25 \text{ mm}$ (EN1992-1-1, §4.4.1)
 Footing : Concrete-Steel class: C25/30-S500
 : Concrete cover: $C_{nom}=75 \text{ mm}$

Weight of backfill

Weight of backfill per meter $W_s=11.14 \text{ kN/m}$
 Center of gravity of backfill $x=-0.125 \text{ m}$, $y=1.382 \text{ m}$

3.2. Partial factors for actions and soil properties (EC7 Tables A.1-A.4, EC8-5 §3.1)

				Equilibrium limit state (EQU), Structural limit state (STR), Geotechnical limit state (GEO)			
				(EQU)	(STR)	(GEO)	(SEISMIC)
Actions	Permanent Unfavourable	γ_{Gdst}	1.10	1.35	1.00	1.00	
	Permanent Favourable	γ_{Gstb}	0.90	1.00	1.00	1.00	
	Variable Unfavourable	γ_{Qdst}	1.50	1.50	1.30	1.00	
	Variable Favourable	γ_{Qstb}	0.00	0.00	0.00	0.00	
Soil parameters	Angle of shearing resistance	γ_{ϕ}	1.25	1.00	1.25	1.25	
	Effective cohesion	γ_c	1.25	1.00	1.25	1.25	
	Undrained shear strength	γ_{cu}	1.40	1.00	1.40	1.40	
	Unconfined strength	γ_{qu}	1.40	1.00	1.40	1.40	
	Weight density	γ_w	1.00	1.00	1.00	1.00	

3.3. Properties of foundation soil

Bearing capacity of foundation soil $q_u=0.20 \text{ N/mm}^2$
 Friction angle between wall footing and soil $\phi=30.00^\circ$, friction coefficient $\tan(\phi)=0.577$
 Cohesion between wall footing and soil $c=0.010 \text{ N/mm}^2$

3.4. Seismic coefficients

(EC8 EN1998-5:2004, §7.3.2)

Design ground acceleration ratio $g_h=a_x g$, $a=0.06$ (EC8-5 §7.3.2)
 Reduction factor for seismic coefficient $r=1.50$ (EC8-5 Table 7.1)
 Coefficient for horizontal seismic force $k_h=0.06/1.500=0.040$ (EC8-5 Eq.7.1)
 Coefficient for vertical seismic force $k_v=0.50 \times 0.040=0.020$ (EC8-5 Eq.7.2)

Forces due to seismic load (except from earth pressure)

Horizontal seismic force due to self weight $F_{wx}= 47.85 \times 0.040 = 1.91 \text{ kN/m}$
 Vertical seismic force due to self weight $F_{wy}= 47.85 \times 0.020 = 0.96 \text{ kN/m}$
 Horizontal seismic force of top loading N_g $F_{gx}= 3.00 \times 0.040 = 0.12 \text{ kN/m}$
 Vertical seismic force of top loading N_g $F_{gy}= 3.00 \times 0.020 = 0.06 \text{ kN/m}$
 Horizontal seismic force of top loading N_q $F_{qx}= 2.00 \times 0.040 = 0.08 \text{ kN/m}$
 Vertical seismic force of top loading N_q $F_{qy}= 2.00 \times 0.020 = 0.04 \text{ kN/m}$
 Horizontal seismic force of backfill $F_{wsx}= 11.14 \times 0.040 = 0.45 \text{ kN/m}$
 Vertical seismic force of backfill $F_{wsy}= 11.14 \times 0.020 = 0.22 \text{ kN/m}$

3.5. Computation of active earth pressure (Coulomb theory)

3.5.1. Wall part from y=0.000 m to y=2.200 m, Hs=2.200 m

Top point A x= 0.000 m y= 0.000 m
 Bottom point B x= 0.000 m y= 2.200 m

Soil properties

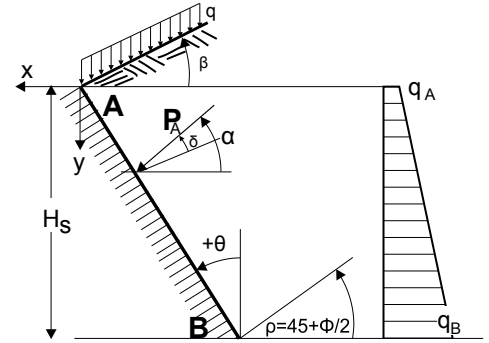
Soil type : Mean gravel
 Unit weight of soil $\gamma = 16.00 \text{ kN/m}^3$
 Unit weight of soil (saturated) $\gamma_s = 20.00 \text{ kN/m}^3$
 Unit weight of water $\gamma_w = 10.00 \text{ kN/m}^3$
 Angle of shearing resistance of ground $\phi = 40.00^\circ$
 Cohesion of ground $c = 0.000 \text{ N/mm}^2$
 Slope angle of ground surface $\beta = 5.00^\circ$
 Inclination angle of the wall backface $\theta = 0.00^\circ$
 Angle of shear resist. between ground-wall $\delta = 20.00^\circ$

Loads on soil surface

Permanent uniform load $g = 3.00 \text{ kN/m}^2$
 Variable uniform load $q = 2.00 \text{ kN/m}^2$

Earth pressure according to Coulomb theory

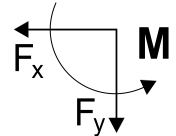
	EQU	STR	GEO
Angle of rupture plane $\rho = 45^\circ + \phi/2$	= 61.00	65.00	61.00°
Coefficient of active earth pressure K_a	= 0.295	0.209	0.295
Earth pressure $q(y) = q_A + \gamma \cdot y \cdot K_a$			



$$K_A = \frac{\cos^2(\phi - \theta)}{\cos^2\theta \cos(\theta + \delta) \left[1 + \sqrt{\frac{\sin(\theta + \delta) \sin(\theta - \beta)}{\cos(\theta + \delta) \cos(\theta - \beta)}} \right]^2}$$

Permanent actions

	EQU	STR	GEO
Earth pressure at the top (y=yA)	qA= 0.88	0.63	0.88 kN/m ²
Earth pressure at the bottom (y=yA+ 2.20m)	qB= 11.26	7.99	11.26 kN/m ²
Earth force $P_a = \frac{1}{2}(q_A + q_B)H$	Pa= 13.35	9.48	13.35 kN/m
Angle of earth force	$\alpha = 16.00$	20.00	16.00 °
Earth force in x direction	Pax= 12.54	8.91	12.54 kN/m
Earth force in y direction	Pay= 4.57	3.24	4.57 kN/m
Moment of earth force at top point (x=0, y=0)	M = -17.73	-12.59	-17.73 kNm/m
Point of application of earth force x= 0.000 m, y= 1.413 m			



Variable actions

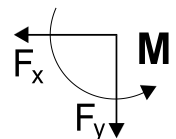
	EQU	STR	GEO
Earth pressure at the top (y=yA)	qA= 0.59	0.42	0.59 kN/m ²
Earth pressure at the bottom (y=yA+ 2.20m)	qB= 0.59	0.42	0.59 kN/m ²
Earth force $P_a = \frac{1}{2}(q_A + q_B)H$	Pa= 1.30	0.92	1.30 kN/m
Angle of earth force	$\alpha = 16.00$	20.00	16.00 °
Earth force in x direction	Pax= 1.22	0.86	1.22 kN/m
Earth force in y direction	Pay= 0.44	0.31	0.44 kN/m
Moment of earth force at top point (x=0, y=0)	M = -1.34	-0.95	-1.34 kNm/m
Point of application of earth force x= 0.000 m, y= 1.100 m			

Total forces and moments

Forces and moments at bottom point B (x=0.000 m, y=2.200 m)

Permanent actions

	EQU	STR	GEO
Total horizontal earth force F_{sx}	= 12.54	8.91	12.54 kN/m
Total vertical earth force F_{sy}	= 4.57	3.24	4.57 kN/m
Total moment of earth force M_s	= 9.86	7.01	9.86 kNm/m



Variable actions

	EQU	STR	GEO
Total horizontal earth force Fsx=	1.22	0.86	1.22 kN/m
Total vertical earth force Fsy=	0.44	0.31	0.44 kN/m
Total moment of earth force Ms =	1.34	0.95	1.34 kNm/m

Seismic loading

(EC8 EN1998-5:2004, §7.3.2, Annex E)

Horizontal seismic coefficient $k_h=0.06/1.500=0.040$ (EC8-5 Eq.7.1, T.7.1)
 Vertical seismic coefficient $k_v=0.50 \times 0.040=0.020$ (EC8-5 Eq.7.2)
 Soil above the water table (EC8-5 Annex E.5)
 $\tan(\omega)=k_h/(1-k_v)=0.040/(1-0.020)=0.041$, $\omega=2.34^\circ$

Method Mononobe-Okabe (EC8-5 Annex E.4)
 for active earth force during seismic loading
 Coefficient of active earth pressure, $K_e^*=0.316$
 Additional earth pressure due to seismic load over STR load case $\xi=(K_e^*/K_e-1)=(0.316/0.209-1)=0.512$

$$K_E = \frac{\cos^2(\varphi-\omega-\theta)}{\cos\omega \cos^2\theta \cos(\delta+\theta+\omega) \left[1 + \sqrt{\frac{\sin(\varphi+\delta)\sin(\varphi-\omega-\beta)}{\cos(\theta+\omega+\delta)\cos(\theta-\beta)}} \right]^2}$$

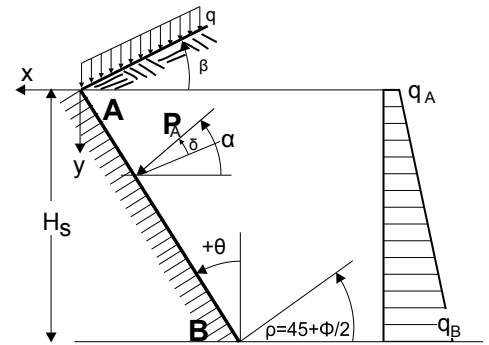
Earth force due to seismic load (Permanent actions) $F_x=1.512 \times 8.91=13.47$ kN/m
 Earth force due to seismic load (Variable actions) $F_x=1.512 \times 0.86=1.30$ kN/m

3.5.2. Wall part from y=2.200 m to y=3.200 m, Hs=1.000 m

Top point A x= 0.000 m y= 2.200 m
 Bottom point B x= 0.000 m y= 3.200 m

Soil properties

Soil type : Large gravel
 Unit weight of soil $\gamma = 16.00$ kN/m³
 Unit weight of soil (saturated) $\gamma_s = 20.00$ kN/m³
 Unit weight of water $\gamma_w = 10.00$ kN/m³
 Angle of shearing resistance of ground $\varphi = 45.00^\circ$
 Cohesion of ground $c = 0.000$ N/mm²
 Slope angle of ground surface $\beta = 0.00^\circ$
 Inclination angle of the wall backface $\theta = 0.00^\circ$
 Angle of shear resist. between ground-wall $\delta = 22.50^\circ$



Loads on soil surface

Permanent uniform load $g = 38.20$ kN/m²
 Variable uniform load $q = 2.00$ kN/m²

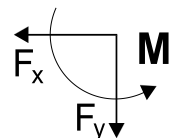
Earth pressure according to Coulomb theory

Angle of rupture plane $\rho = 45^\circ + \varphi/2 = 63.00$ 67.50 63.00°
 Coefficient of active earth pressure $K_a = 0.236$ 0.160 0.236
 Earth pressure $q(y) = q_A + \gamma \cdot y \cdot K_a$

$$K_A = \frac{\cos^2(\varphi-\theta)}{\cos^2\theta \cos(\theta+\delta) \left[1 + \sqrt{\frac{\sin(\theta+\delta)\sin(\theta-\beta)}{\cos(\theta+\delta)\cos(\theta-\beta)}} \right]^2}$$

Permanent actions

	EQU	STR	GEO
Earth pressure at the top (y=yA)	$q_A = 9.02$	6.11	9.02 kN/m ²
Earth pressure at the bottom (y=yA+ 1.00m)	$q_B = 12.80$	8.67	12.80 kN/m ²
Earth force $P_a = \frac{1}{2}(q_A+q_B)H$	$P_a = 10.91$	7.39	10.91 kN/m
Angle of earth force	$\alpha = 18.00$	22.50	18.00 °
Earth force in x direction	$P_{ax} = 10.08$	6.83	10.08 kN/m
Earth force in y direction	$P_{ay} = 4.18$	2.83	4.18 kN/m
Moment of earth force at top point (x=0,y=0)	$M = -27.51$	-18.64	-27.51 kNm/m
Point of application of earth force x= 0.000 m, y= 2.729 m			



Variable actions

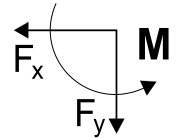
	EQU	STR	GEO
Earth pressure at the top (y=yA)	qA= 0.47	0.32	0.47 kN/m ²
Earth pressure at the bottom (y=yA+ 1.00m)	qB= 0.47	0.32	0.47 kN/m ²
Earth force Pa=½(qA+qB)H	Pa= 0.47	0.32	0.47 kN/m
Angle of earth force	α = 18.00	22.50	18.00 °
Earth force in x direction	Pax= 0.43	0.30	0.43 kN/m
Earth force in y direction	Pay= 0.18	0.12	0.18 kN/m
Moment of earth force at top point (x=0,y=0)	M = -1.16	-0.81	-1.16 kNm/m
Point of application of earth force x= 0.000 m, y= 2.700 m			

Total forces and moments

Forces and moments at bottom point B (x=0.000 m, y=3.200 m)

Permanent actions

	EQU	STR	GEO
Total horizontal earth force Fsx=	22.62	15.74	22.62 kN/m
Total vertical earth force Fsy=	8.75	6.07	8.75 kN/m
Total moment of earth force Ms =	27.15	19.14	27.15 kNm/m



Variable actions

	EQU	STR	GEO
Total horizontal earth force Fsx=	1.65	1.16	1.65 kN/m
Total vertical earth force Fsy=	0.62	0.43	0.62 kN/m
Total moment of earth force Ms =	2.78	1.96	2.78 kNm/m

Seismic loading

(EC8 EN1998-5:2004, §7.3.2, Annex E)

Horizontal seismic coefficient $k_h=0.06/1.500=0.040$

(EC8-5 Eq.7.1, T.7.1)

Vertical seismic coefficient $k_v=0.50 \times 0.040=0.020$

(EC8-5 Eq.7.2)

Soil above the water table

(EC8-5 Annex E.5)

$\tan(\omega)=k_h/(1-k_v)=0.040/(1-0.020)=0.041, \omega=2.34^\circ$

Method Mononobe-Okabe (EC8-5 Annex E.4)

for active earth force during seismic loading

Coefficient of active earth pressure, $K_e^*=0.254$

Additional earth pressure due to seismic load over STR load case $\xi=(K_e^*/K_e-1)=(0.254/0.160-1)=0.588$

$$K_E = \frac{\cos^2(\varphi-\omega-\theta)}{\cos\omega \cos^2\theta \cos(\delta+\theta+\omega) \left[1 + \sqrt{\frac{\sin(\varphi+\delta)\sin(\varphi-\omega-\beta)}{\cos(\theta+\omega+\delta)\cos(\theta-\beta)}} \right]^2}$$

Earth force due to seismic load (Permanent actions) $F_x=1.588 \times 6.83=10.85$ kN/m

Earth force due to seismic load (Variable actions) $F_x=1.588 \times 0.30= 0.48$ kN/m

3.6. Computation of passive earth pressure (Rankine theory)

3.6.1. Wall part from y=2.600 m to y=3.500 m, Hs=0.900 m

Top point A x= 1.950 m y= 2.600 m

Bottom point B x= 1.950 m y= 3.500 m

Soil properties

Soil type : Mean gravel

Unit weight of soil

$\gamma =16.00$ kN/m³

Unit weight of soil (saturated)

$\gamma_s=20.00$ kN/m³

Unit weight of water

$\gamma_w=10.00$ kN/m³

Angle of shearing resistance of ground

$\varphi=40.00^\circ$

Cohesion of ground

$c=0.000$ N/mm²

Slope angle of ground surface

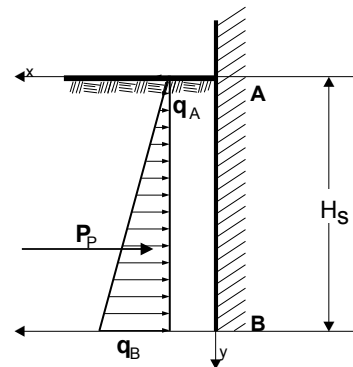
$\beta= 0.00^\circ$

Earth pressure on vertical surface

$\theta= 0.00^\circ$

Angle of shear resist. between ground-wall

$\delta= 0.00^\circ$



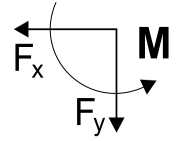
Earth pressure according to Coulomb theory

Angle of rupture plane $\rho=45^\circ-\phi/2 = 29.00$ EQU STR GEO
 Coefficient of passive earth pressure $K_p = 3.255$ 4.599 3.255
 Earth pressure $q(y)=q_A+\gamma \cdot y \cdot K_p$

$$K_p = \frac{\cos^2(\phi+\theta)}{\cos^2\theta \cos(\theta-\delta) \left[1 - \sqrt{\frac{\sin(\theta+\delta)\sin(\theta+\beta)}{\cos(\theta-\delta)\cos(\theta-\beta)}} \right]^2}$$

Permanent actions

Earth pressure at the top ($y=y_A$) $q_A = 0.00$ EQU STR GEO 0.00 kN/m²
 Earth pressure at the bottom ($y=y_A+0.90$ m) $q_B = -46.87$ -66.23 -46.87 kN/m²
 Earth force $P_a = \frac{1}{2}(q_A+q_B)H$ $P_p = 21.09$ 29.80 21.09 kN/m
 Angle of earth force $\alpha = 0.00$ 0.00 0.00 °
 Earth force in x direction $P_{px} = -21.09$ -29.80 -21.09 kN/m
 Earth force in y direction $P_{py} = 0.00$ 0.00 0.00 kN/m
 Moment of earth force at top point ($x=0, y=0$) $M = 67.49$ 95.36 67.49 kNm/m
 Point of application of earth force $x = 1.950$ m, $y = 3.200$ m

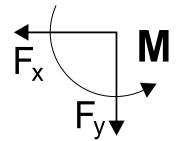


Total forces and moments

Forces and moments at bottom point B ($x=1.950$ m, $y=3.500$ m)

Permanent actions

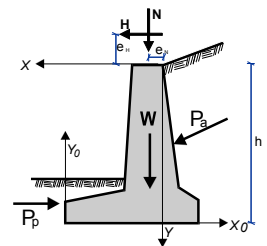
Total horizontal earth force $F_{sx} = -21.09$ -29.80 -21.09 kN/m
 Total vertical earth force $F_{sy} = 0.00$ 0.00 0.00 kN/m
 Total moment of earth force $M_s = -6.33$ -8.94 -6.33 kNm/m



3.7. Checks of wall stability (EQU)

3.7.1. Forces (driving and resisting) on the wall (EQU)

Action		y1 - y2	Fx	Fy	x	y	
			[kN/m]	[kN/m]	[kN/m]	[m]	[m]
Active earth pressure	Pa	0.00- 2.20	12.54	4.57	0.000	1.414	
Backfill surcharge (live)	Pq	0.00- 2.20	1.22	0.44	0.000	1.100	
Active earth pressure	Pa	2.20- 3.20	10.08	4.18	0.000	2.729	
Backfill surcharge (live)	Pq	2.20- 3.20	0.43	0.18	0.000	2.700	
Passive earth pressure	Pp	2.60- 3.50	-21.09	0.00	1.950	3.200	
Wall weight	W		0.00	47.85	0.494	2.237	
Backfill weight	Ws		0.00	11.14	-0.125	1.382	
Vert. load on top (dead)	Ng		0.00	3.00	0.125	0.000	
Vert. load on top (live)	Nq		0.00	2.00	0.125	0.000	

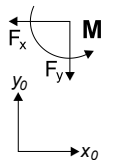


3.7.2. Check of soil bearing capacity (EQU)

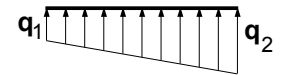
(EC7 EN1997-1-1:2004, §6.5.2)

Check for $0.90x(\text{self weight}+\text{top vertical dead load})+0.00x(\text{top vertical live load})$

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M	
			[kN/m]	[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.10	0.00- 2.20	13.79	5.03	1.950	1.786	14.84	
Backfill surcharge (live)	Pqx1.50	0.00- 2.20	1.83	0.66	1.950	2.100	2.55	
Active earth pressure	Pax1.10	2.20- 3.20	11.09	4.60	1.950	0.471	-3.74	
Backfill surcharge (live)	Pqx1.50	2.20- 3.20	0.64	0.27	1.950	0.500	-0.20	
Wall weight	W x0.90		0.00	43.06	1.456	0.963	-62.70	
Backfill weight	Ws x0.90		0.00	10.03	2.075	1.818	-20.81	
Vert. load on top (dead)	Ngx0.90		0.00	2.70	1.825	3.200	-4.93	
			Sum=	66.35			-74.99	



Sum of vertical forces = 66.35 kN/m
 Sum of moments at front toe = -74.99 kNm/m
 Sum of moments at middle of base = -2.00 kNm/m
 Eccentricity $ec = -2.00/66.35 = -0.030m$, $ec < 2.200/6 = 0.367m$
 Soil pressure $q_1 = 0.028 \text{ N/mm}^2$ $q_2 = 0.033 \text{ N/mm}^2$
 Effective footing $L = 2.200 - 2 \times 0.030 = 2.140 \text{ m}$
 Soil bearing capacity $R_d = L \cdot q_u / \gamma M = 2.140 \times (1000 \times 0.20) / 1.40 = 305.71 \text{ kN/m}$
 Bearing resistance check $V_d = 66.35 < R_d = 305.71 \text{ kN/m}$, Check is verified



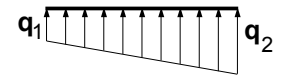
(EC7 Annex D)

(EC7 Eq.2.2, Eq.6.1)

Check for 1.10x(self weight+top vertical dead load)+1.50x(top vertical live load)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.10	0.00- 2.20	13.79	5.03	1.950	1.786	14.84	
Backfill surcharge (live)	Pqx1.50	0.00- 2.20	1.83	0.66	1.950	2.100	2.55	
Active earth pressure	Pax1.10	2.20- 3.20	11.09	4.60	1.950	0.471	-3.74	
Backfill surcharge (live)	Pqx1.50	2.20- 3.20	0.64	0.27	1.950	0.500	-0.20	
Wall weight	W x1.10		0.00	52.64	1.456	0.963	-76.64	
Backfill weight	Wsx1.10		0.00	12.25	2.075	1.818	-25.43	
Vert. load on top (dead)	Ngx1.10		0.00	3.30	1.825	3.200	-6.03	
Vert. load on top (live)	Nqx1.50		0.00	3.00	1.825	3.200	-5.48	
			Sum=	81.75			-100.13	

Sum of vertical forces = 81.75 kN/m
 Sum of moments at front toe = -100.13 kNm/m
 Sum of moments at middle of base = -10.20 kNm/m
 Eccentricity $ec = -10.20/81.75 = -0.125m$, $ec < 2.200/6 = 0.367m$
 Soil pressure $q_1 = 0.025 \text{ N/mm}^2$ $q_2 = 0.050 \text{ N/mm}^2$
 Effective footing $L = 2.200 - 2 \times 0.125 = 1.950 \text{ m}$
 Soil bearing capacity $R_d = L \cdot q_u / \gamma M = 1.950 \times (1000 \times 0.20) / 1.40 = 278.57 \text{ kN/m}$
 Bearing resistance check $V_d = 81.75 < R_d = 278.57 \text{ kN/m}$, Check is verified



(EC7 Annex D)

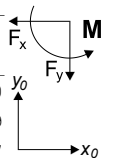
(EC7 Eq.2.2, Eq.6.1)

3.7.3. Failure check due to overturning (EQU)

(EC7 EN1997-1-1:2004, §9.7.4)

Overturning with respect to the toe ($x_o=0, y_o=0$) ($x=1.950, y=3.200$ m)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	Mo+	Mo-	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]	[kNm/m]
Active earth pressure	Pax1.10	0.00- 2.20	13.79	5.03	1.950	1.786	24.64	9.80	
Backfill surcharge (live)	Pqx1.50	0.00- 2.20	1.83	0.66	1.950	2.100	3.84	1.29	
Active earth pressure	Pax1.10	2.20- 3.20	11.09	4.60	1.950	0.471	5.23	8.97	
Backfill surcharge (live)	Pqx1.50	2.20- 3.20	0.64	0.27	1.950	0.500	0.33	0.52	
Wall weight	W x0.90		0.00	43.06	1.456	0.963	0.00	62.70	
Backfill weight	Wsx0.90		0.00	10.03	2.075	1.818	0.00	20.81	
Vert. load on top (dead)	Ngx0.90		0.00	2.70	1.825	3.200	0.00	4.93	
			Sum=				34.04	109.02	

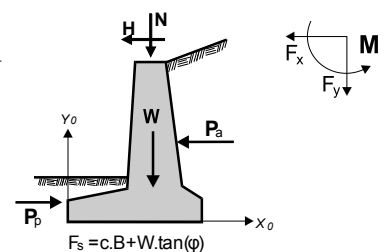


Sum of overturning moments = 34.04 kNm/m
 Sum of moments resisting overturning = 109.02 kNm/m
 Overturning check $M_{sd} = 34.04 < M_{rd} = 109.02 \text{ kNm/m}$, Check is verified

3.7.4. Failure check against sliding (EQU)

(EC7 EN1997-1-1:2004, §9.7.3, §6.5.3)

Action	(γ)	y1 - y2	Fx+	Fx-	Fy	
				[kN/m]	[kN/m]	[kN/m]
Active earth pressure	Pax1.10	0.00- 2.20	13.79	0.00	5.03	
Backfill surcharge (live)	Pqx1.50	0.00- 2.20	1.83	0.00	0.66	
Active earth pressure	Pax1.10	2.20- 3.20	11.09	0.00	4.60	
Backfill surcharge (live)	Pqx1.50	2.20- 3.20	0.64	0.00	0.27	
Passive earth pressure	Ppx0.90	2.60- 3.50	0.00	18.98	0.00	
Wall weight	W x0.90		0.00	0.00	43.06	
Backfill weight	Wsx0.90		0.00	0.00	10.03	
Vert. load on top (dead)	Ngx0.90		0.00	0.00	2.70	
			Sum=	27.35	18.98	66.35

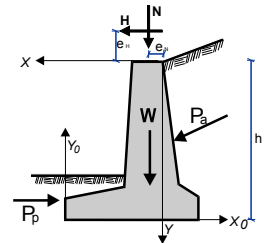


Soil friction $R_d = V_d \cdot \tan \phi / \gamma M = 66.35 \times \tan(30.00^\circ) / 1.25 = 30.65 \text{ kN/m}$
 Soil cohesion $R_d = A \cdot c_u / \gamma M = 1000 \times 2.200 \times 0.010 / 1.25 = 17.60 \text{ kN/m}$
 (resisting forces from effective cohesion are neglected) (EC7 §6.5.3. 10)
 Sum of driving forces = 27.35 kN/m
 Sum of resisting forces (18.98+30.65) = 49.63 kN/m
 Sliding resistance check $H_d = 27.35 < R_d = 49.63 \text{ kN/m}$, Check is verified

3.8. Checks of wall stability (STR)

3.8.1. Forces (driving and resisting) on the wall (STR)

Action	$y_1 - y_2$	F_x	F_y	x	y	
		[kN/m]		[kN/m]		[m]
Active earth pressure	Pa 0.00- 2.20	8.91	3.24	0.000	1.413	
Backfill surcharge (live)	Pq 0.00- 2.20	0.86	0.31	0.000	1.100	
Active earth pressure	Pa 2.20- 3.20	6.83	2.83	0.000	2.729	
Backfill surcharge (live)	Pq 2.20- 3.20	0.30	0.12	0.000	2.700	
Passive earth pressure	Pp 2.60- 3.50	-29.80	0.00	1.950	3.200	
Wall weight	W	0.00	47.85	0.494	2.237	
Backfill weight	Ws	0.00	11.14	-0.125	1.382	
Vert. load on top (dead)	Ng	0.00	3.00	0.125	0.000	
Vert. load on top (live)	Nq	0.00	2.00	0.125	0.000	

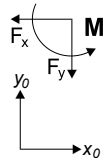


3.8.2. Check of soil bearing capacity (STR)

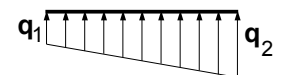
(EC7 EN1997-1-1:2004, §6.5.2)

Check for $1.00 \times (\text{self weight} + \text{top vertical dead load}) + 0.00 \times (\text{top vertical live load})$

Action	(γ)	$y_1 - y_2$	F_x	F_y	x_0	y_0	M	
			[kN/m]		[kN/m]		[m]	[kNm/m]
Active earth pressure	Pax1.35	0.00- 2.20	12.03	4.37	1.950	1.787	12.96	
Backfill surcharge (live)	Pqx1.50	0.00- 2.20	1.29	0.46	1.950	2.100	1.82	
Active earth pressure	Pax1.35	2.20- 3.20	9.22	3.82	1.950	0.471	-3.11	
Backfill surcharge (live)	Pqx1.50	2.20- 3.20	0.45	0.18	1.950	0.500	-0.12	
Wall weight	W x1.00		0.00	47.85	1.456	0.963	-69.67	
Backfill weight	Wsx1.00		0.00	11.14	2.075	1.818	-23.12	
Vert. load on top (dead)	Ngx1.00		0.00	3.00	1.825	3.200	-5.48	
			Sum=	70.82			-86.72	



Sum of vertical forces = 70.82 kN/m
 Sum of moments at front toe = -86.72 kNm/m
 Sum of moments at middle of base = -8.82 kNm/m
 Eccentricity $ec = -8.82 / 70.82 = -0.125 \text{ m}$, $ec \leq 2.200 / 6 = 0.367 \text{ m}$
 Soil pressure $q_1 = 0.021 \text{ N/mm}^2$ $q_2 = 0.043 \text{ N/mm}^2$
 Effective footing $L = 2.200 - 2 \times 0.125 = 1.951 \text{ m}$
 Soil bearing capacity $R_d = L \cdot q_u / \gamma M = 1.951 \times (1000 \times 0.20) / 1.00 = 390.20 \text{ kN/m}$
 Bearing resistance check $V_d = 70.82 < R_d = 390.20 \text{ kN/m}$, Check is verified



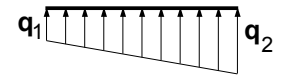
(EC7 Annex D)

(EC7 Eq.2.2, Eq.6.1)

Check for $1.35 \times (\text{self weight} + \text{top vertical dead load}) + 1.50 \times (\text{top vertical live load})$

Action	(γ)	$y_1 - y_2$	F_x	F_y	x_0	y_0	M	
			[kN/m]		[kN/m]		[m]	[kNm/m]
Active earth pressure	Pax1.35	0.00- 2.20	12.03	4.37	1.950	1.787	12.96	
Backfill surcharge (live)	Pqx1.50	0.00- 2.20	1.29	0.46	1.950	2.100	1.82	
Active earth pressure	Pax1.35	2.20- 3.20	9.22	3.82	1.950	0.471	-3.11	
Backfill surcharge (live)	Pqx1.50	2.20- 3.20	0.45	0.18	1.950	0.500	-0.12	
Wall weight	W x1.35		0.00	64.60	1.456	0.963	-94.05	
Backfill weight	Wsx1.35		0.00	15.04	2.075	1.818	-31.21	
Vert. load on top (dead)	Ngx1.35		0.00	4.05	1.825	3.200	-7.40	
Vert. load on top (live)	Nqx1.50		0.00	3.00	1.825	3.200	-5.48	
			Sum=	95.52			-126.59	

Sum of vertical forces = 95.52 kN/m
 Sum of moments at front toe = -126.59 kNm/m
 Sum of moments at middle of base = -21.52 kNm/m
 Eccentricity $ec = -21.52/95.52 = -0.225\text{m}$, $ec \leq 2.200/6 = 0.367\text{m}$
 Soil pressure $q_1 = 0.017\text{ N/mm}^2$ $q_2 = 0.070\text{ N/mm}^2$
 Effective footing $L = 2.200 - 2 \times 0.225 = 1.749\text{ m}$
 Soil bearing capacity $R_d = L \cdot q_u / \gamma_M = 1.749 \times (1000 \times 0.20) / 1.00 = 349.80\text{ kN/m}$
 Bearing resistance check $V_d = 95.52 < R_d = 349.80\text{ kN/m}$, Check is verified



(EC7 Annex D)

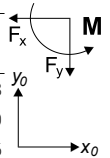
(EC7 Eq.2.2, Eq.6.1)

3.8.3. Failure check due to overturning (STR)

(EC7 EN1997-1-1:2004, §9.7.4)

Overturning with respect to the toe ($x_0=0, y_0=0$) ($x=1.950, y=3.200\text{ m}$)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	Mo+	Mo-	
			[kN/m]	[kN/m]	[kN/m]	[m]	[m]	[kNm/m]	[kNm/m]
Active earth pressure	Pax1.35	0.00- 2.20	12.03	4.37	1.950	1.787	21.49	8.53	
Backfill surcharge (live)	Pqx1.50	0.00- 2.20	1.29	0.46	1.950	2.100	2.72	0.90	
Active earth pressure	Pax1.35	2.20- 3.20	9.22	3.82	1.950	0.471	4.35	7.45	
Backfill surcharge (live)	Pqx1.50	2.20- 3.20	0.45	0.18	1.950	0.500	0.22	0.34	
Wall weight	W x1.00		0.00	47.85	1.456	0.963	0.00	69.67	
Backfill weight	Wsx1.00		0.00	11.14	2.075	1.818	0.00	23.12	
Vert. load on top (dead)	Ngx1.00		0.00	3.00	1.825	3.200	0.00	5.48	
							Sum=	28.78	115.49

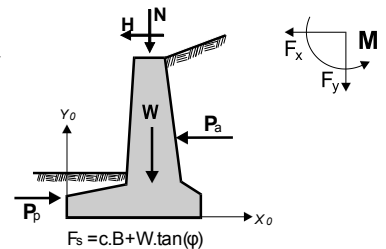


Sum of overturning moments = 28.78 kNm/m
 Sum of moments resisting overturning = 115.49 kNm/m
 Overturning check $M_{sd} = 28.78 < M_{rd} = 115.49\text{ kNm/m}$, Check is verified

3.8.4. Failure check against sliding (STR)

(EC7 EN1997-1-1:2004, §9.7.3, §6.5.3)

Action	(γ)	y1 - y2	Fx+	Fx-	Fy	
			[kN/m]	[kN/m]	[kN/m]	
Active earth pressure	Pax1.35	0.00- 2.20	12.03	0.00	4.37	
Backfill surcharge (live)	Pqx1.50	0.00- 2.20	1.29	0.00	0.46	
Active earth pressure	Pax1.35	2.20- 3.20	9.22	0.00	3.82	
Backfill surcharge (live)	Pqx1.50	2.20- 3.20	0.45	0.00	0.18	
Passive earth pressure	Ppx1.00	2.60- 3.50	0.00	29.80	0.00	
Wall weight	W x1.00		0.00	0.00	47.85	
Backfill weight	Wsx1.00		0.00	0.00	11.14	
Vert. load on top (dead)	Ngx1.00		0.00	0.00	3.00	
			Sum=	22.99	29.80	70.82



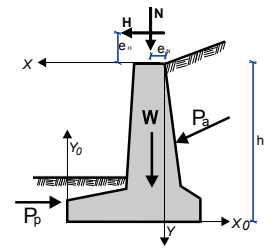
Soil friction $R_d = V_d \cdot \tan\phi / \gamma_M = 70.82 \times \tan(30.00^\circ) / 1.00 = 40.89\text{ kN/m}$
 Soil cohesion $R_d = A \cdot c_u / \gamma_M = 1000 \times 2.200 \times 0.010 / 1.00 = 22.00\text{ kN/m}$
 (resisting forces from effective cohesion are neglected)
 Sum of driving forces = 22.99 kN/m
 Sum of resisting forces (29.80+40.89) = 70.69 kN/m
 Sliding resistance check $H_d = 22.99 < R_d = 70.69\text{ kN/m}$, Check is verified

(EC7 §6.5.3. 10)

3.9. Checks of wall stability (GEO)

3.9.1. Forces (driving and resisting) on the wall (GEO)

Action		y1 - y2	Fx	Fy	x	y	
			[kN/m]	[kN/m]	[kN/m]	[m]	[m]
Active earth pressure	Pa	0.00- 2.20	12.54	4.57	0.000	1.414	
Backfill surcharge (live)	Pq	0.00- 2.20	1.22	0.44	0.000	1.100	
Active earth pressure	Pa	2.20- 3.20	10.08	4.18	0.000	2.729	
Backfill surcharge (live)	Pq	2.20- 3.20	0.43	0.18	0.000	2.700	
Passive earth pressure	Pp	2.60- 3.50	-21.09	0.00	1.950	3.200	
Wall weight	W		0.00	47.85	0.494	2.237	
Backfill weight	Ws		0.00	11.14	-0.125	1.382	
Vert. load on top (dead)	Ng		0.00	3.00	0.125	0.000	
Vert. load on top (live)	Nq		0.00	2.00	0.125	0.000	

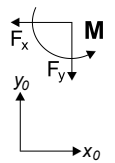


3.9.2. Check of soil bearing capacity (GEO)

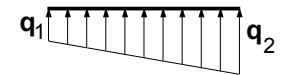
(EC7 EN1997-1-1:2004, §6.5.2)

Check for 1.00x(self weight+top vertical dead load)+0.00x(top vertical live load)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M	
			[kN/m]	[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.00	0.00- 2.20	12.54	4.57	1.950	1.786	13.49	
Backfill surcharge (live)	Pqx1.30	0.00- 2.20	1.59	0.57	1.950	2.100	2.21	
Active earth pressure	Pax1.00	2.20- 3.20	10.08	4.18	1.950	0.471	-3.40	
Backfill surcharge (live)	Pqx1.30	2.20- 3.20	0.56	0.23	1.950	0.500	-0.17	
Wall weight	W x1.00		0.00	47.85	1.456	0.963	-69.67	
Backfill weight	Wsx1.00		0.00	11.14	2.075	1.818	-23.12	
Vert. load on top (dead)	Ngx1.00		0.00	3.00	1.825	3.200	-5.48	
			Sum=	71.54			-86.14	



Sum of vertical forces = 71.54 kN/m
 Sum of moments at front toe = -86.14 kNm/m
 Sum of moments at middle of base = -7.45 kNm/m
 Eccentricity $ec = -7.45/71.54 = -0.104m$, $ec \leq 2.200/6 = 0.367m$
 Soil pressure $q_1 = 0.023 N/mm^2$ $q_2 = 0.042 N/mm^2$
 Effective footing $L = 2.200 - 2 \times 0.104 = 1.992 m$
 Soil bearing capacity $R_d = L \cdot q_u / \gamma M = 1.992 \times (1000 \times 0.20) / 1.40 = 284.57 kN/m$
 Bearing resistance check $V_d = 71.54 < R_d = 284.57 kN/m$, Check is verified



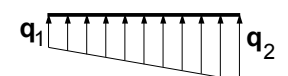
(EC7 Annex D)

(EC7 Eq.2.2, Eq.6.1)

Check for 1.00x(self weight+top vertical dead load)+1.30x(top vertical live load)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M	
			[kN/m]	[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.00	0.00- 2.20	12.54	4.57	1.950	1.786	13.49	
Backfill surcharge (live)	Pqx1.30	0.00- 2.20	1.59	0.57	1.950	2.100	2.21	
Active earth pressure	Pax1.00	2.20- 3.20	10.08	4.18	1.950	0.471	-3.40	
Backfill surcharge (live)	Pqx1.30	2.20- 3.20	0.56	0.23	1.950	0.500	-0.17	
Wall weight	W x1.00		0.00	47.85	1.456	0.963	-69.67	
Backfill weight	Wsx1.00		0.00	11.14	2.075	1.818	-23.12	
Vert. load on top (dead)	Ngx1.00		0.00	3.00	1.825	3.200	-5.48	
Vert. load on top (live)	Nqx1.30		0.00	2.60	1.825	3.200	-4.74	
			Sum=	74.14			-90.88	

Sum of vertical forces = 74.14 kN/m
 Sum of moments at front toe = -90.88 kNm/m
 Sum of moments at middle of base = -9.33 kNm/m
 Eccentricity $ec = -9.33/74.14 = -0.126m$, $ec \leq 2.200/6 = 0.367m$
 Soil pressure $q_1 = 0.022 N/mm^2$ $q_2 = 0.045 N/mm^2$
 Effective footing $L = 2.200 - 2 \times 0.126 = 1.948 m$
 Soil bearing capacity $R_d = L \cdot q_u / \gamma M = 1.948 \times (1000 \times 0.20) / 1.40 = 278.29 kN/m$
 Bearing resistance check $V_d = 74.14 < R_d = 278.29 kN/m$, Check is verified



(EC7 Annex D)

(EC7 Eq.2.2, Eq.6.1)

3.9.3. Failure check due to overturning (GEO)

(EC7 EN1997-1-1:2004, §9.7.4)

Overturning with respect to the toe ($x_0=0, y_0=0$) ($x=1.950, y=3.200$ m)

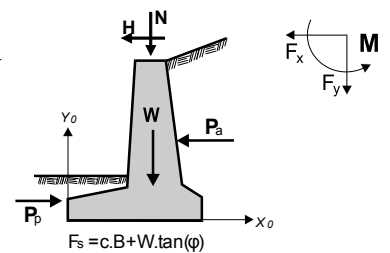
Action	(γ)	$y_1 - y_2$	F_x	F_y	x_0	y_0	M_{o+}	M_{o-}		
			[kN/m]	[kN/m]	[m]	[m]	[kNm/m]	[kNm/m]		
Active earth pressure	$P_{ax}1.00$	0.00- 2.20	12.54	4.57	1.950	1.786	22.40	8.91		
Backfill surcharge (live)	$P_{qx}1.30$	0.00- 2.20	1.59	0.57	1.950	2.100	3.33	1.12		
Active earth pressure	$P_{ax}1.00$	2.20- 3.20	10.08	4.18	1.950	0.471	4.75	8.15		
Backfill surcharge (live)	$P_{qx}1.30$	2.20- 3.20	0.56	0.23	1.950	0.500	0.29	0.45		
Wall weight	$W \times 1.00$		0.00	47.85	1.456	0.963	0.00	69.67		
Backfill weight	$W_{sx}1.00$		0.00	11.14	2.075	1.818	0.00	23.12		
Vert. load on top (dead)	$N_{gx}1.00$		0.00	3.00	1.825	3.200	0.00	5.48		
							Sum=	30.77		116.90

Sum of overturning moments = 30.77 kNm/m
 Sum of moments resisting overturning = 116.90 kNm/m
 Overturning check $M_{sd}=30.77 < M_{rd}=116.90$ kNm/m, Check is verified

3.9.4. Failure check against sliding (GEO)

(EC7 EN1997-1-1:2004, §9.7.3, §6.5.3)

Action	(γ)	$y_1 - y_2$	F_{x+}	F_{x-}	F_y	
			[kN/m]	[kN/m]	[kN/m]	
Active earth pressure	$P_{ax}1.00$	0.00- 2.20	12.54	0.00	4.57	
Backfill surcharge (live)	$P_{qx}1.30$	0.00- 2.20	1.59	0.00	0.57	
Active earth pressure	$P_{ax}1.00$	2.20- 3.20	10.08	0.00	4.18	
Backfill surcharge (live)	$P_{qx}1.30$	2.20- 3.20	0.56	0.00	0.23	
Passive earth pressure	$P_{px}1.00$	2.60- 3.50	0.00	21.09	0.00	
Wall weight	$W \times 1.00$		0.00	0.00	47.85	
Backfill weight	$W_{sx}1.00$		0.00	0.00	11.14	
Vert. load on top (dead)	$N_{gx}1.00$		0.00	0.00	3.00	
			Sum=	24.77	21.09	71.54



Soil friction $R_d = V_d \cdot \tan\phi / \gamma_M = 71.54 \times \tan(30.00^\circ) / 1.25 = 33.04$ kN/m
 Soil cohesion $R_d = A \cdot c_u / \gamma_M = 1000 \times 2.200 \times 0.010 / 1.25 = 17.60$ kN/m
 (resisting forces from effective cohesion are neglected)
 Sum of driving forces = 24.77 kN/m
 Sum of resisting forces (21.09+33.04) = 54.13 kN/m
 Sliding resistance check $H_d=24.77 < R_d=54.13$ kN/m, Check is verified

(EC7 §6.5.3. 10)

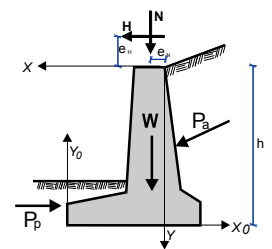
3.10. Seismic design

(EC8 EN1998-5:2004)

Checks of wall stability (with seismic loading)

3.10.1. Forces (driving and resisting) on the wall

Action		$y_1 - y_2$	F_x	F_y	x	y
			[kN/m]	[kN/m]	[m]	[m]
Active earth pressure	P_a	0.00- 2.20	8.91	3.24	0.000	1.413
Backfill surcharge (live)	P_q	0.00- 2.20	0.86	0.31	0.000	1.100
Active earth pressure	P_a	2.20- 3.20	6.83	2.83	0.000	2.729
Backfill surcharge (live)	P_q	2.20- 3.20	0.30	0.12	0.000	2.700
Passive earth pressure	P_p	2.60- 3.50	-29.80	0.00	1.950	3.200
Wall weight	W		0.00	47.85	0.494	2.237
Backfill weight	W_s		0.00	11.14	-0.125	1.382
Vert. load on top (dead)	N_g		0.00	3.00	0.125	0.000
Vert. load on top (live)	N_q		0.00	2.00	0.125	0.000



3.10.2. Additional forces due to seismic load

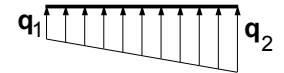
Action		y1 - y2	Fx	Fy	x	y
				[kN/m]	[kN/m]	[m]
Active earth pressure	Pa	0.00- 2.20	2.20	4.56	0.000	1.413
Backfill surcharge (live)	Pq	0.00- 2.20	2.20	0.44	0.000	1.100
Active earth pressure	Pa	2.20- 3.20	3.20	4.02	0.000	2.729
Backfill surcharge (live)	Pq	2.20- 3.20	3.20	0.18	0.000	2.700
Wall weight	W			1.91	-0.96	0.494
Backfill weight	Ws			0.45	-0.22	-0.125
Vert. load on top (dead)	Ng			0.12	-0.06	0.125
Vert. load on top (live)	Nq			0.08	-0.04	0.125

3.10.3. Check of soil bearing capacity (with seismic loading)

(EC7 §6.5.2)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M
				[kN/m]	[kN/m]	[m]	[m]
Active earth pressure	Pax1.00	0.00- 2.20	2.20	13.47	3.24	1.950	1.787
Backfill surcharge (live)	Pqx1.00	0.00- 2.20	2.20	1.30	0.31	1.950	2.100
Active earth pressure	Pax1.00	2.20- 3.20	3.20	10.85	2.83	1.950	0.471
Backfill surcharge (live)	Pqx1.00	2.20- 3.20	3.20	0.48	0.12	1.950	0.500
Wall weight	W x1.00			1.91	46.89	1.456	0.963
Backfill weight	Wsx1.00			0.45	10.92	2.075	1.818
Vert. load on top (dead)	Ngx1.00			0.12	2.94	1.825	3.200
Vert. load on top (live)	Nqx1.00			0.08	1.96	1.825	3.200
				Sum=	69.21		

Sum of vertical forces = 69.21 kN/m
 Sum of moments at front toe = -77.10 kNm/m
 Sum of moments at middle of base = -0.97 kNm/m
 Eccentricity $ec = -0.97/69.21 = -0.014m$, $ec \leq 2.200/6 = 0.367m$
 Soil pressure $q_1 = 0.030$ N/mm² $q_2 = 0.033$ N/mm²
 Effective footing $L = 2.200 - 2 \times 0.014 = 2.172$ m
 Soil bearing capacity $Rd = L \cdot q_u / \gamma_M = 2.172 \times (1000 \times 0.20) / 1.00 = 434.40$ kN/m
 Bearing resistance check $Vd = 69.21 < Rd = 434.40$ kN/m, Check is verified



(EC7 Annex D)

(EC7 Eq.2.2, Eq.6.1)

3.10.4. Failure check due to overturning (with seismic loading)

(EC7 §9.7.4)

Overturning with respect to the toe ($x_o = 0, y_o = 0$) ($x = 1.950, y = 3.200$ m)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	Mo+	Mo-
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.00	0.00- 2.20	2.20	13.47	3.24	1.950	1.787	24.07
Backfill surcharge (live)	Pqx1.00	0.00- 2.20	2.20	1.30	0.31	1.950	2.100	2.74
Active earth pressure	Pax1.00	2.20- 3.20	3.20	10.85	2.83	1.950	0.471	5.11
Backfill surcharge (live)	Pqx1.00	2.20- 3.20	3.20	0.48	0.12	1.950	0.500	0.24
Wall weight	W x1.00			1.91	46.89	1.456	0.963	3.24
Backfill weight	Wsx1.00			0.45	10.92	2.075	1.818	1.27
Vert. load on top (dead)	Ngx1.00			0.12	2.94	1.825	3.200	0.49
Vert. load on top (live)	Nqx1.00			0.08	1.96	1.825	3.200	0.33
							Sum=	37.49

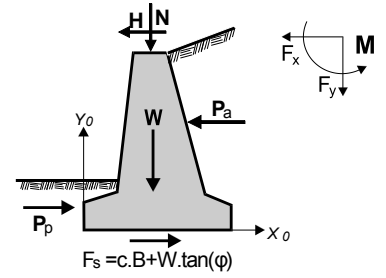
(*moments of negative seismic vertical loads, are added to the overturning moments)

Sum of overturning moments = 37.49 kNm/m
 Sum of moments resisting overturning = 114.59 kNm/m
 Overturning check $Msd = 37.49 < Mrd = 114.59$ kNm/m, Check is verified

3.10.5. Failure check against sliding (with seismic loading)

(EC7 §9.7.3, §6.5.3)

Action	(γ)	y1 - y2	Fx+	Fx-	Fy
			[kN/m]	[kN/m]	[kN/m]
Active earth pressure	Pax1.00	0.00- 2.20	13.47	0.00	3.24
Backfill surcharge (live)	Pqx1.00	0.00- 2.20	1.30	0.00	0.31
Active earth pressure	Pax1.00	2.20- 3.20	10.85	0.00	2.83
Backfill surcharge (live)	Pqx1.00	2.20- 3.20	0.48	0.00	0.12
Passive earth pressure	Ppx1.00	2.60- 3.50	0.00	29.80	0.00
Wall weight	W x1.00		1.91	0.00	46.89
Backfill weight	Wsx1.00		0.45	0.00	10.92
Vert. load on top (dead)	Ngx1.00		0.12	0.00	2.94
Vert. load on top (live)	Nqx1.00		0.08	0.00	1.96
		Sum=	28.66	29.80	69.21



Soil friction $Rd = Vd \cdot \tan\phi / \gamma M = 69.21 \times \tan(30.00^\circ) / 1.00 = 39.96$ kN/m

Soil cohesion $Rd = A \cdot cu / \gamma M = 1000 \times 2.200 \times 0.010 / 1.00 = 22.00$ kN/m

(resisting forces from effective cohesion are neglected)

(EC7 §6.5.3. 10)

Sum of driving forces = 28.66 kN/m

Sum of resisting forces (29.80+39.96) = 69.76 kN/m

Sliding resistance check $Hd = 28.66 < Rd = 69.76$ kN/m, Check is verified

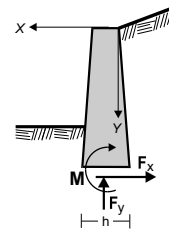
3.11. Design of wall steam

(EC2 EN1992-1-1:2004)

3.11.1. Loading 1.35x(permanent unfavourable)+1.00x(permanent favourable)+1.50x(variable unfav.)

Forces (at cross section centroid) at wall steam

y	h	Fx	Fy	M
[m]	[m]	[kN/m]	[kN/m]	[kNm/m]
0.50	0.287	1.23	6.80	0.06
1.00	0.324	3.50	11.45	0.84
1.50	0.361	6.85	16.96	2.86
2.00	0.398	11.26	23.31	6.60
2.70	0.450	17.76	33.29	15.46



3.11.2. Design of wall steam in bending

(EC2 §9.6, §6.1)

Concrete-Steel class: C25/30-S500, Concrete cover: $C_{nom} = 25$ mm

(§3, §4.4.1.1)

Vertical reinforcement minimum: $0.0020A_c$, maximum: $0.0400A_c$

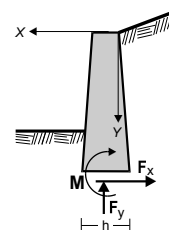
(EC2 §9.6.2)

y	Msd	Nsd	d	Kd	x/d	ec/es	Ks	As	min reinf.
[m]	[kN/m]	[kN]	[mm]						[cm ² /m]
0.50	0.06	-6.80	257	28.20	0.01	0.2/20.0	2.31	0.00	(2.87)
1.00	0.84	-11.45	294	19.19	0.01	0.3/20.0	2.31	0.00	(3.24)
1.50	2.86	-16.96	331	14.24	0.02	0.4/20.0	2.31	0.00	(3.61)
2.00	6.60	-23.31	368	11.34	0.02	0.5/20.0	2.32	0.13	(3.98)
2.70	15.46	-33.29	420	8.96	0.03	0.6/20.0	2.32	0.45	(4.50)

3.11.3. Loading 1.00x(permanent unfav.)+1.00x(permanent favour.)+1.00x(variable)+1.00x(seismic)

Forces (at cross section centroid) at wall steam (with seismic loading)

y	h	Fx	Fy	M
[m]	[m]	[kN/m]	[kN/m]	[kNm/m]
0.50	0.287	1.73	6.80	0.28
1.00	0.324	4.39	11.45	1.46
1.50	0.361	8.28	16.96	4.14
2.00	0.398	13.37	23.31	8.89
2.70	0.450	20.72	33.29	19.17



3.11.4. Design of wall steam in bending (with seismic loading)

(EC2 §9.6, §6.1)
(§3, §4.4.1.1)
(EC2 §9.6.2)

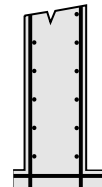
Concrete-Steel class: C25/30-S500, Concrete cover: Cnom=25 mm
Vertical reinforcement minimum: 0.0020Ac, maximum: 0.0400Ac

y	Msd	Nsd	d	Kd	x/d	ec/es	Ks	As	min reinf.
[m]	[kN/m]	[kN]	[mm]						[cm ² /m] [cm ² /m]
0.50	0.28	-6.80	257	25.08	0.01	0.2/20.0	2.31	0.00	(2.87)
1.00	1.46	-11.45	294	17.06	0.02	0.3/20.0	2.31	0.00	(3.24)
1.50	4.14	-16.96	331	12.79	0.02	0.4/20.0	2.32	0.08	(3.61)
2.00	8.89	-23.31	368	10.28	0.03	0.6/20.0	2.32	0.27	(3.98)
2.70	19.17	-33.29	420	8.29	0.03	0.7/20.0	2.33	0.66	(4.50)

3.11.5. Reinforcement of wall steam

Reinforcement at back steam face Ø10/17.0 (4.62cm²/m)
Secondary transverse reinforcement Ø8/50.0 (1.01cm²/m)

Reinforcement at front steam face Ø10/17.0 (4.62cm²/m)
Secondary transverse reinforcement Ø8/50.0 (1.01cm²/m)



3.11.6. Anchorage of wall steam reinforcement

(EC2 §8.4)

Basic required anchorage length $l_{b,rqd} = (\Phi/4) (\sigma_{sd}/f_{bd}) = (10/4) \times (62/1.89) = 82\text{mm}$
 $\sigma_{sd} = 435.00 \times 66 / 462 = 62\text{MPa}$ $f_{bd} = 2.25 \times 0.70 \times (f_{ctk} \times 0.05 / \gamma_c) = 1.89\text{MPa}$
 Design anchorage length $l_{bd} = 1.00 \times 82 = 82\text{mm}$, $C_{nom} = 25\text{mm} < 3\Phi = 30\text{mm}$
 Minimum anchorage length $l_{b,min} = \max(0.30 l_{b,rqd}, 10\Phi, 100\text{mm}) = 100\text{mm}$
 Necessary bend 100mm at lower bar end for anchorage

(EC2 Eq.8.3)
(EC2 §8.4.2)
(EC2 §8.4.4, T.8.2)

3.11.7. Shear check of wall steam

(EC2 EN1992-1-1:2004, §6.2.2)

Concrete-Steel class: C25/30-S500, Concrete cover: Cnom=25 mm
 The earth pressure load variation is linear, so the variation of shear force is parabolic. The variation of steam cross section is linear.
 The most unfavourable place for shear check is the base of the steam.

(§3, §4.4.1.1)

$V_{sd} = 17.76\text{ kN/m}$, $V_{sd (+seismic)} = 20.72\text{ kN/m}$, $N_{sd} = -33.29\text{ kN/m}$

Shear capacity without shear reinforcement V_{rdc}

(EC2 §6.2.2)

$V_{rdc} = [C_{rdc} \cdot k \cdot (100\rho_l \cdot f_{ck})^{0.333} + k_l \cdot \sigma_{cp}] \cdot b_w \cdot d$

(EC2 Eq.6.2.a)

$V_{rdc} >= (v_{min} + k_l \cdot \sigma_{cp}) \cdot b_w \cdot d$

(EC2 Eq.6.2.b)

$C_{rdc} = 0.18 / \gamma_c = 0.18 / 1.50 = 0.120$, $f_{ck} = 25.00\text{MPa}$

$k = 1 + (200/d)^{1/2} \leq 2$, $k = 1.69$, $k_l = 0.15$

$\rho_l = A_{s1} / (b_w \cdot d) = 462 / (1000 \times 420) = 0.0011$

$\sigma_{cp} = N_{sd} / A_c = 1000 \times 33.29 / 450000 = 0.07\text{N/mm}^2$

$v_{min} = 0.035 \cdot k^{1.50} \cdot f_{ck}^{1/2} = 0.38\text{N/mm}^2$

(EC2 Eq.6.3N)

$V_{rd,c(min)} = 0.001 \times (0.38 + 0.15 \times 0.07) \times 1000 \times 420 = 164.01\text{kN/m}$

$V_{rdc} = 0.001 \times [0.120 \times 1.69 \times (0.11 \times 25.00)^{0.333} + 0.15 \times 0.07] \times 1000 \times 420 = 123.74$, $V_{rdc} = V_{rdc(min)} = 164.01\text{kN/m}$

$V_{sd} = 20.72\text{ kN/m} \leq V_{rdc} = 164.01\text{ kN/m}$, shear OK

3.12. Design of wall footing and reinforcement

(EC2 EN1992-1-1:2004)

3.12.1. Design of front toe x=1.950 m to x=0.450 m

Sum of vertical forces = 95.52 kN/m

Sum of moments at middle of base = -21.52 kNm/m

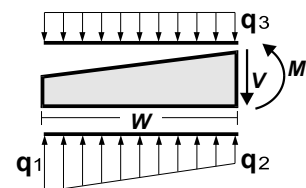
$q_1 = 0.017\text{ N/mm}^2$, $q_2 = 0.053\text{ N/mm}^2$, $w = 1.500\text{ m}$

pressure from self weight $q_3 = 0.013\text{ N/mm}^2$

$M = 17.85\text{ kNm/m}$, $V = 32.89\text{ kN/m}$

V at distance $d = 425\text{mm}$ from the face of the steam = 18.06 kN/m

$M_{sd} = 17.85\text{ kNm/m}$, $V_{sd} = 18.06\text{ kN/m}$



3.12.2. Design of front toe x=1.950 m to x=0.450 m (with seismic loading)

Sum of vertical forces = 69.21 kN/m
 Sum of moments at middle of base = -0.97 kNm/m
 $q_1 = 0.030 \text{ N/mm}^2$, $q_2 = 0.032 \text{ N/mm}^2$, $w = 1.500 \text{ m}$
 pressure from self weight $q_3 = 0.013 \text{ N/mm}^2$
 $M = 20.03 \text{ kNm/m}$, $V = 27.11 \text{ kN/m}$
 V at distance $d = 425 \text{ mm}$ from the face of the stem = 19.16 kN/m
 $M_{sd} = 20.03 \text{ kNm/m}$, $V_{sd} = 19.16 \text{ kN/m}$

3.12.3. Design of wall footing in bending

(EC2 EN1992-1-1:2004, §6.1)

Concrete-Steel class: C25/30-S500, Concrete cover: $C_{nom} = 75 \text{ mm}$
 $M_{sd} = 20.03 \text{ kNm/m}$, $d = 419 \text{ mm}$, $K_d = 9.36$ $x/d = 0.03$ $\epsilon_c/\epsilon_{cs} = 0.6/20.0$ $k_s = 2.32$,
 Minimum reinforcement $A_s \geq 0.26bd \cdot f_{ctm}/f_{yk}$ ($A_s = 5.66 \text{ cm}^2/\text{m}$)
 Minimum reinforcement $\phi 12/19.5$ ($5.79 \text{ cm}^2/\text{m}$)

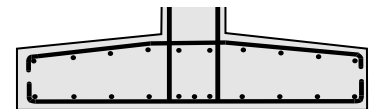
$A_s = 1.11 \text{ cm}^2$

(§3, §4.4.1.1)

(EC2 §9.3.1)

3.12.4. Reinforcement of wall footing

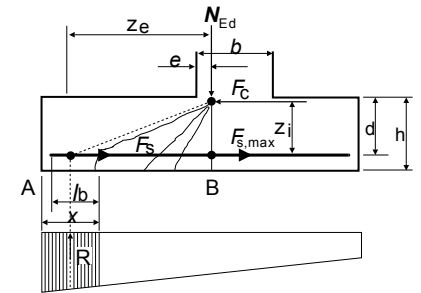
Footing reinforcement at bottom $\phi 12/19.5$ ($5.79 \text{ cm}^2/\text{m}$)
Secondary transverse reinforcement $\phi 12/40.0$ ($2.82 \text{ cm}^2/\text{m}$)



3.12.5. Anchorage of footing reinforcement

(EC2 EN1992-1-1:2004, §9.8.2.2, §8.4)

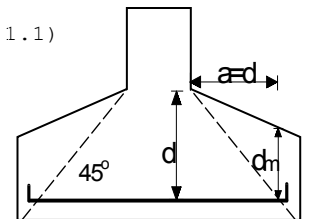
$x = h/2 = 0.175 \text{ m}$, $R = 1000 \times 0.053 \times 0.175 = 9.27 \text{ kN/m}$
 $e = 0.15b = 0.067 \text{ m}$ $z_e = 1.480 \text{ m}$, $z_i = 0.900d = 0.377 \text{ m}$
 $F_s = R \cdot z_e / z_i = 9.27 \times 1.480 / 0.377 = 36.38 \text{ kN/m}$
 $\sigma_{sd} = F_s / A_s = 1000 \times 36.38 / 579 = 63 \text{ MPa}$
 Basic required anchorage length (EC2 Eq.8.3)
 $l_{b, reqd} = (\phi/4) (\sigma_{sd} / f_{bd}) = (12/4) \times (63 / 2.70) = 70 \text{ mm}$
 $f_{bd} = 2.25 \times 1.00 \times (f_{ctk} / 0.05 / \gamma_c) = 2.70 \text{ MPa}$ (EC2 §8.4.2)
 Design anchorage length (EC2 §8.4.4, T.8.2)
 $l_{bd} = 0.70 \times 70 = 49 \text{ mm}$, $C_{nom} = 75 \text{ mm} > 3\phi = 36 \text{ mm}$
 Minimum anchorage length $l_{b, min} = \max(0.30 l_{b, reqd}, 10\phi, 100 \text{ mm}) = 120 \text{ mm}$
 Necessary anchorage length of longitudinal reinforcement $L_{bd} = 120 \text{ mm} = 0.120 \text{ m}$
 $l_{bd} = 120 \text{ mm} > (x - C_{nom}) = 100.00$. Necessary bends 60mm at bar ends for anchorage



3.12.6. Design of wall footing for shear and punching shear

(EC2 EN1992-1-1:2004, §6.2.2)

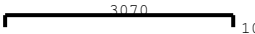
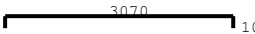
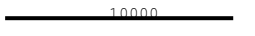
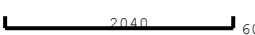
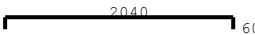
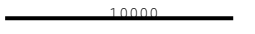
Concrete-Steel class: C25/30-S500, Concrete cover: $C_{nom} = 75 \text{ mm}$ (§3, §4.4.1.1)
Punching shear capacity without shear reinforcement V_{rdc} (EC2 §6.4.4)
 $V_{rdc} = [C_{rdc} \cdot k \cdot (100\rho_1 \cdot f_{ck})^{0.333} \cdot (2d/a)] \cdot b_w \cdot d$ (EC2 Eq.6.50)
 $V_{rdc} > [v_{min} \cdot 2d/a] \cdot b_w \cdot d$, $d = d_m = 377 \text{ mm}$, $a = 419 \text{ mm}$
 $C_{rdc} = 0.18 / \gamma_c = 0.18 / 1.50 = 0.120$, $f_{ck} = 25.00 \text{ MPa}$
 $k = 1 + (200/d)^{1/4} \leq 2$, $k = 1.73$
 $\rho_1 = A_{s1} / (b_w \cdot d) = 579 / (1000 \times 377) = 0.0015$
 $v_{min} = 0.035 \cdot k^{1.50} \cdot f_{ck}^{1/2} = 0.40 \text{ N/mm}^2$ (EC2 Eq.6.3N)
 $V_{rd, c (min)} = 0.001 \times (0.40 \times 2 \times 377 / 419) \times 1000 \times 377 = 271.51 \text{ kN/m}$
 $V_{rdc} = 0.001 \times [0.120 \times 1.73 \times (0.15 \times 25.00)^{0.333} \times 2 \times 377 / 419] \times 1000 \times 377 = 218.93$, $V_{rdc} = V_{rdc (min)} = 271.51 \text{ kN/m}$
 $V_{sd} = 19.16 \text{ kN/m} \leq V_{rdc} = 271.51 \text{ kN/m}$, shear and punching shear OK

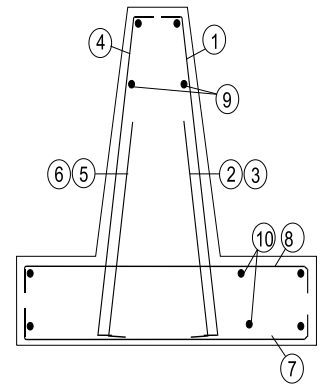


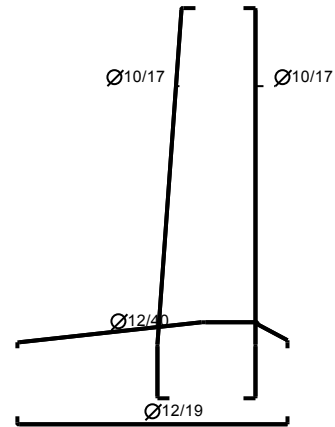
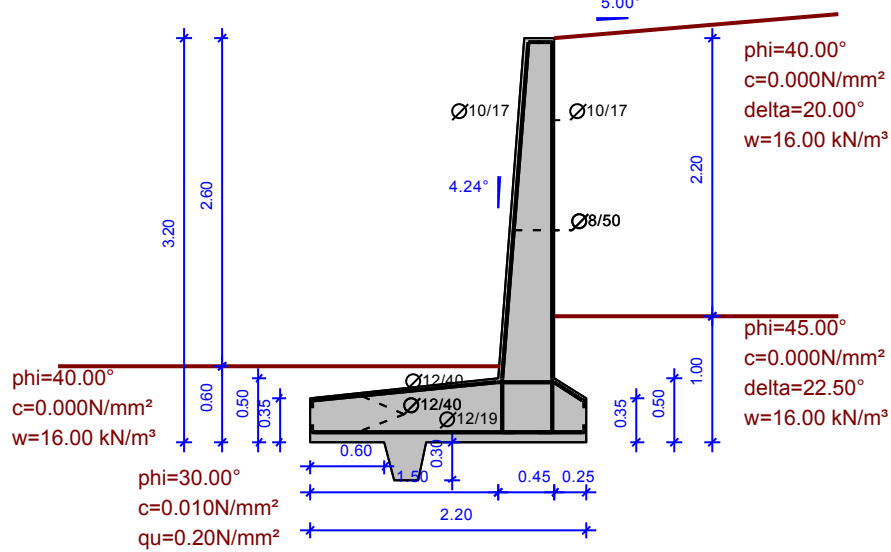
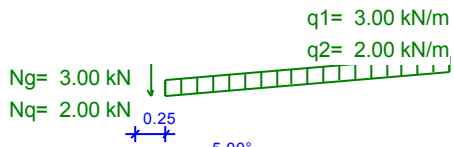
3.13. Material estimate

Concrete per meter of wall length 1.914 m³/m
 Reinforcing steel per meter of wall 52.005 kg/m
 Total concrete of wall 10.000x 1.914 = 19.137 m³
 Total reinforcing steel of wall 10.000x 52.005 = 520.050 kg

3.14. Reinforcing bar schedule

Num	type	reinforcing bar [mm]	items	∅	g/m [kg/m]	length [m]	weight [kg]
1	1	100 	59	10	0.617	3.270	119.04
2	4	100 	59	10	0.617	3.270	119.04
3	9		12	8	0.395	10.000	47.40
4	7	60 	51	12	0.888	2.160	97.82
5	8	60 	25	12	0.888	2.160	47.95
6	10		10	12	0.888	10.000	88.80
Total weight [kg]							520.05





General information

Wall type : Cantilever wall
 Concrete and steel class
 Steam :C25/30-S500
 Footing :C25/30-S500

Design codes

Eurocode 0 EN1991-1-1, Basis of structural design
 Eurocode 1 EN1991-1-1, Actions on structures
 Eurocode 2 EN1992-1-1, Design of concrete structures
 Eurocode 7 EN1997-1-1, Geotechnical design
 Eurocode 8 EN1998-5, Earthquake design

Loads

Vertical : dead Ng=3.00kN, live Nq=2.00kN
 Horizontal: dead Hg=0.00kN, live Hq=0.00kN
 Surcharge : dead g=3.00kN/m², live q=2.00kN/m²
 Seismic coefficients
 Design ground acceleration ratio a =0.060
 Coefficient for horizontal seismic force kh=0.040

Reinforcing bar schedule

Coefficient for vertical seismic force kv=0.020

#		reinforcing bar [mm]	items	Ø [mm]	g/m [kg/m]	length [m]	weight [kg]
1	W1	3070	59	10	0.617	3.270	119.04
2	W4	3070	59	10	0.617	3.270	119.04
3	W9	10000	12	8	0.395	10.000	47.40
4	W7	2040	51	12	0.888	2.160	97.82
5	W8	2040	25	12	0.888	2.160	47.95
6	W10	10000	10	12	0.888	10.000	88.80
Total weight [kg]							520.05

Soil properties back-1

phi=40.00°
 c=0.000N/mm²
 delta=20.00°
 w=16.00 kN/m³

Soil properties back-2

phi=45.00°
 c=0.000N/mm²
 delta=22.50°
 w=16.00 kN/m³

Soil properties front

phi=40.00°
 c=0.000N/mm²
 w=16.00 kN/m³

Foundation soil properties

phi=30.00°
 c=0.010N/mm²
 qu=0.20N/mm²

Concrete volume V= 19.14 [m³]

Reinforcement weight G=520.05 [kg]

Project: Example of retaining walls

C. WALL-001

Scale : 1:60

Date: 12/03/2007

Designer:

Draw.No.:

Filename: Example of retaining wall Sign:

RUNET Norway as

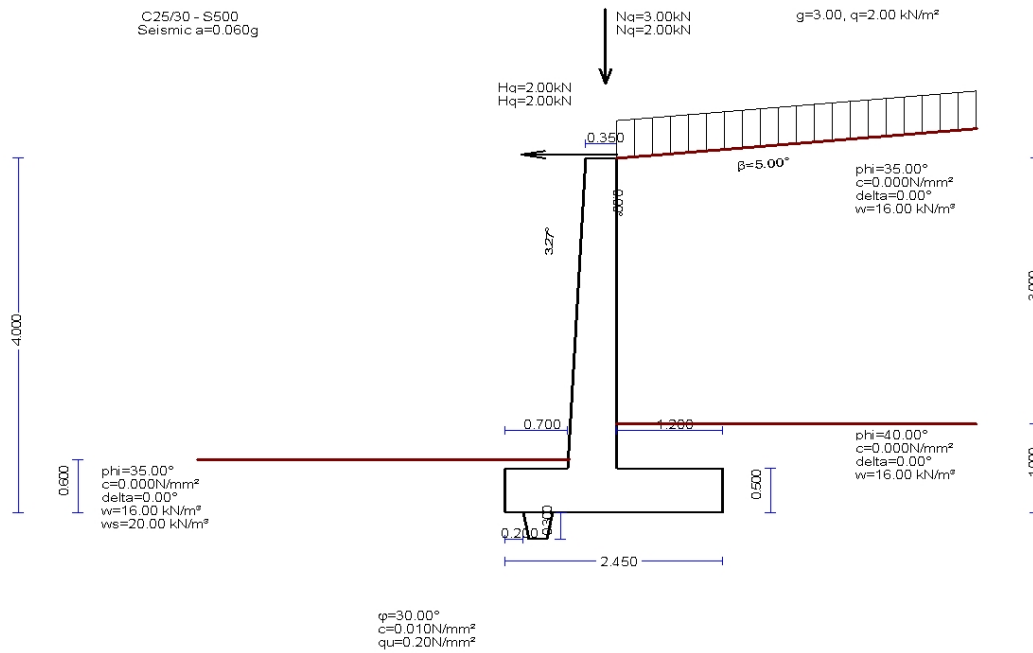
BETONexpress

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4. C. WALL-002

Cantilever concrete wall

(EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002, EC7 EN1997-1-1:2004, EC8 EN1998-5:2004)



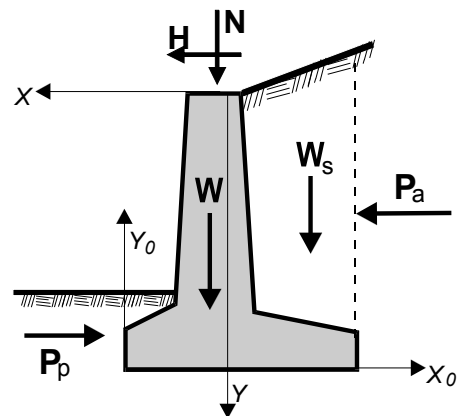
4.1. Wall properties-Parameters-Code requirements

Dimensions

Height of wall	$h = 4.000\text{ m}$
Transverse length of wall	$L = 10.000\text{ m}$
Steam thickness at top	$B1 = 0.350\text{ m}$
Steam thickness at bottom	$B2 = 0.550\text{ m}$
Width of wall base	$B = 2.450\text{ m}$
Width of wall toe	0.700 m
Width of wall heel	1.200 m
Height of wall steam	3.500 m
Thickness of wall footing	0.500 m
Front thickness of wall toe	0.500 m
Back thickness of wall heel	0.500 m
Slope (batter) at frontface	$3.270^\circ (1:17.5)$
Slope (batter) at backface	$0.000^\circ (0:1)$
Height of wall base key	0.300 m

Loads on wall top

Vertical permanent load	$N_g = 3.00\text{ kN/m}$
Vertical variable load	$N_q = 2.00\text{ kN/m}$
Eccentricity of vertical load	$e_N = 0.13\text{ kN/m}$
Horizontal permanent load	$H_g = 2.00\text{ kN/m}$
Horizontal variable load	$H_q = 2.00\text{ kN/m}$
Eccentricity of horizontal load	$e_H = 0.00\text{ kN/m}$



Weight of wall

Unit weight of wall material $\gamma_g=25.000 \text{ kN/m}^3$
 Cross section area of wall $A= 2.800 \text{ m}^2$
 Self weight per meter of wall $W= 2.800 \times 25.000 = 70.00 \text{ kN/m}$
 Center of gravity of wall at $x=0.140 \text{ m}$, $y=2.698 \text{ m}$ ($x_o=1.110 \text{ m}$, $y_o=1.302 \text{ m}$)

Wall materials

Steam : Concrete-Steel class: C25/30-S500 (EN1992-1-1, §3)
 : Concrete cover: $C_{nom}=25 \text{ mm}$ (EN1992-1-1, §4.4.1)
 Footing : Concrete-Steel class: C25/30-S500
 : Concrete cover: $C_{nom}=75 \text{ mm}$

Weight of backfill

Weight of backfill per meter $W_s=70.22 \text{ kN/m}$
 Center of gravity of backfill $x=-0.600 \text{ m}$, $y=1.776 \text{ m}$

4.2. Partial factors for actions and soil properties

(EC7 Tables A.1-A.4, EC8-5 §3.1)

				Equilibrium limit state (EQU), Structural limit state (STR), Geotechnical limit state (GEO)			
				(EQU)	(STR)	(GEO)	(SEISMIC)
Actions	Permanent Unfavourable	γ_{Gdst}	1.10	1.35	1.00	1.00	
	Permanent Favourable	γ_{Gstb}	0.90	1.00	1.00	1.00	
	Variable Unfavourable	γ_{Qdst}	1.50	1.50	1.30	1.00	
	Variable Favourable	γ_{Qstb}	0.00	0.00	0.00	0.00	
Soil parameters	Angle of shearing resistance	γ_ϕ	1.25	1.00	1.25	1.25	
	Effective cohesion	γ_c	1.25	1.00	1.25	1.25	
	Undrained shear strength	γ_{cu}	1.40	1.00	1.40	1.40	
	Unconfined strength	γ_{qu}	1.40	1.00	1.40	1.40	
	Weight density	γ_w	1.00	1.00	1.00	1.00	

4.3. Properties of foundation soil

Bearing capacity of foundation soil $q_u=0.20 \text{ N/mm}^2$
 Friction angle between wall footing and soil $\phi=30.00^\circ$, friction coefficient $\tan(\phi)=0.577$
 Cohesion between wall footing and soil $c=0.010 \text{ N/mm}^2$

4.4. Seismic coefficients

(EC8 EN1998-5:2004, §7.3.2)

Design ground acceleration ratio $g_h=a_x g$, $a=0.06$ (EC8-5 §7.3.2)
 Reduction factor for seismic coefficient $r=1.50$ (EC8-5 Table 7.1)
 Coefficient for horizontal seismic force $k_h=0.06/1.500=0.040$ (EC8-5 Eq.7.1)
 Coefficient for vertical seismic force $k_v=0.50 \times 0.040=0.020$ (EC8-5 Eq.7.2)

Forces due to seismic load (except from earth pressure)

Horizontal seismic force due to self weight $F_{wx}= 70.00 \times 0.040 = 2.80 \text{ kN/m}$
 Vertical seismic force due to self weight $F_{wy}= 70.00 \times 0.020 = 1.40 \text{ kN/m}$
 Horizontal seismic force of top loading N_g $F_{gx}= 3.00 \times 0.040 = 0.12 \text{ kN/m}$
 Vertical seismic force of top loading N_g $F_{gy}= 3.00 \times 0.020 = 0.06 \text{ kN/m}$
 Horizontal seismic force of top loading N_q $F_{qx}= 2.00 \times 0.040 = 0.08 \text{ kN/m}$
 Vertical seismic force of top loading N_q $F_{qy}= 2.00 \times 0.020 = 0.04 \text{ kN/m}$
 Horizontal seismic force of backfill $F_{wsx}= 70.22 \times 0.040 = 2.81 \text{ kN/m}$
 Vertical seismic force of backfill $F_{wsy}= 70.22 \times 0.020 = 1.40 \text{ kN/m}$

4.5. Computation of active earth pressure (Rankine theory)

4.5.1. Wall part from y=-0.105 m to y=3.000 m, Hs=3.105 m

Top point A x=-1.200 m y=-0.105 m
 Bottom point B x=-1.200 m y= 3.000 m

Soil properties

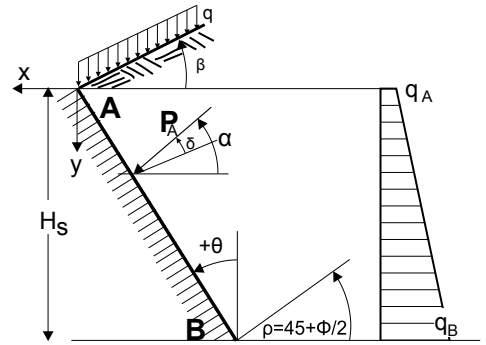
Soil type : Thin gravel
 Unit weight of soil $\gamma = 16.00 \text{ kN/m}^3$
 Unit weight of soil (saturated) $\gamma_s = 20.00 \text{ kN/m}^3$
 Unit weight of water $\gamma_w = 10.00 \text{ kN/m}^3$
 Angle of shearing resistance of ground $\phi = 35.00^\circ$
 Cohesion of ground $c = 0.000 \text{ N/mm}^2$
 Slope angle of ground surface $\beta = 5.00^\circ$
 Earth pressure on vertical surface $\theta = 0.00^\circ$
 Angle of shear resist. between ground-wall $\delta = 0.00^\circ$

Loads on soil surface

Permanent uniform load $g = 3.00 \text{ kN/m}^2$
 Variable uniform load $q = 2.00 \text{ kN/m}^2$

Earth pressure according to Coulomb theory

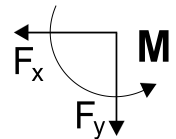
	EQU	STR	GEO
Angle of rupture plane $\rho = 45^\circ + \phi/2$	= 59.00	62.50	59.00°
Coefficient of active earth pressure K_a	= 0.382	0.284	0.382
Earth pressure $q(y) = q_A + \gamma \cdot y \cdot K_a$			



$$K_A = \frac{\cos^2(\phi - \theta)}{\cos^2\theta \cos(\theta + \delta) \left[1 + \sqrt{\frac{\sin(\theta + \delta) \sin(\theta - \beta)}{\cos(\theta + \delta) \cos(\theta - \beta)}} \right]^2}$$

Permanent actions

	EQU	STR	GEO
Earth pressure at the top (y=yA)	qA= 1.15	0.85	1.15 kN/m ²
Earth pressure at the bottom (y=yA+ 3.10m)	qB= 20.13	14.96	20.13 kN/m ²
Earth force $Pa = \frac{1}{2}(qA + qB)H$	Pa= 33.04	24.55	33.04 kN/m
Angle of earth force $\alpha =$	0.00	0.00	0.00°
Earth force in x direction	Pax= 33.04	24.55	33.04 kN/m
Earth force in y direction	Pay= 0.00	0.00	0.00 kN/m
Moment of earth force at top point (x=0, y=0)	M = -63.07	-46.87	-63.07 kNm/m
Point of application of earth force x= -1.200 m, y= 1.909 m			



Variable actions

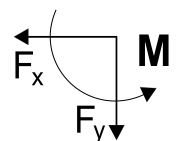
	EQU	STR	GEO
Earth pressure at the top (y=yA)	qA= 0.76	0.57	0.76 kN/m ²
Earth pressure at the bottom (y=yA+ 3.10m)	qB= 0.76	0.57	0.76 kN/m ²
Earth force $Pa = \frac{1}{2}(qA + qB)H$	Pa= 2.36	1.77	2.36 kN/m
Angle of earth force $\alpha =$	0.00	0.00	0.00°
Earth force in x direction	Pax= 2.36	1.77	2.36 kN/m
Earth force in y direction	Pay= 0.00	0.00	0.00 kN/m
Moment of earth force at top point (x=0, y=0)	M = -3.41	-2.56	-3.41 kNm/m
Point of application of earth force x= -1.200 m, y= 1.447 m			

Total forces and moments

Forces and moments at bottom point B (x=-1.200 m, y=3.000 m)

Permanent actions

	EQU	STR	GEO
Total horizontal earth force F_{sx}	= 33.04	24.55	33.04 kN/m
Total vertical earth force F_{sy}	= 0.00	0.00	0.00 kN/m
Total moment of earth force M_s	= 36.05	26.78	36.05 kNm/m



Variable actions

	EQU	STR	GEO
Total horizontal earth force Fsx=	2.36	1.77	2.36 kN/m
Total vertical earth force Fsy=	0.00	0.00	0.00 kN/m
Total moment of earth force Ms =	3.67	2.75	3.67 kNm/m

Seismic loading

(EC8 EN1998-5:2004, §7.3.2, Annex E)

Horizontal seismic coefficient $k_h=0.06/1.500=0.040$ (EC8-5 Eq.7.1, T.7.1)
 Vertical seismic coefficient $k_v=0.50 \times 0.040=0.020$ (EC8-5 Eq.7.2)
 Soil above the water table (EC8-5 Annex E.5)
 $\tan(\omega)=k_h/(1-k_v)=0.040/(1-0.020)=0.041, \omega=2.34^\circ$

Method Mononobe-Okabe (EC8-5 Annex E.4)
 for active earth force during seismic loading
 Coefficient of active earth pressure, $K_e^*=0.405$
 Additional earth pressure due to seismic load over STR load case $\xi=(K_e^*/K_e-1)=(0.405/0.284-1)=0.426$

$$K_E = \frac{\cos^2(\varphi-\omega-\theta)}{\cos\omega \cos^2\theta \cos(\delta+\theta+\omega) \left[1 + \sqrt{\frac{\sin(\varphi+\delta)\sin(\varphi-\omega-\beta)}{\cos(\theta+\omega+\delta)\cos(\theta-\beta)}} \right]^2}$$

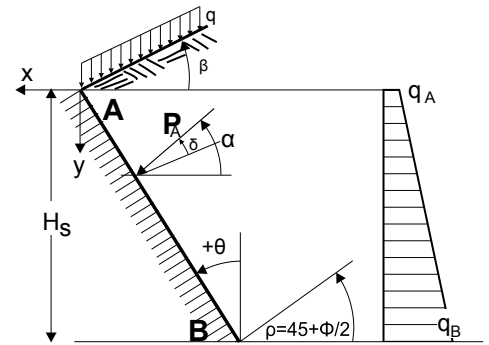
Earth force due to seismic load (Permanent actions) $F_x=1.426 \times 24.55=35.01$ kN/m
 Earth force due to seismic load (Variable actions) $F_x=1.426 \times 1.77=2.52$ kN/m

4.5.2. Wall part from y=3.000 m to y=4.000 m, Hs=1.000 m

Top point A x=-1.200 m y= 3.000 m
 Bottom point B x=-1.200 m y= 4.000 m

Soil properties

Soil type : Mean gravel	
Unit weight of soil	$\gamma = 16.00$ kN/m ³
Unit weight of soil (saturated)	$\gamma_s = 20.00$ kN/m ³
Unit weight of water	$\gamma_w = 10.00$ kN/m ³
Angle of shearing resistance of ground	$\varphi = 40.00^\circ$
Cohesion of ground	$c = 0.000$ N/mm ²
Slope angle of ground surface	$\beta = 0.00^\circ$
Earth pressure on vertical surface	$\theta = 0.00^\circ$
Angle of shear resist. between ground-wall	$\delta = 0.00^\circ$



Loads on soil surface

Permanent uniform load	$g = 52.68$ kN/m ²
Variable uniform load	$q = 2.00$ kN/m ²

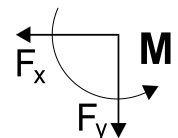
Earth pressure according to Coulomb theory

	EQU	STR	GEO
Angle of rupture plane $\rho=45^\circ+\varphi/2$	= 61.00	65.00	61.00°
Coefficient of active earth pressure K_a =	0.307	0.217	0.307
Earth pressure $q(y)=q_A+\gamma \cdot y \cdot K_a$			

$$K_A = \frac{\cos^2(\varphi-\theta)}{\cos^2\theta \cos(\theta+\delta) \left[1 + \sqrt{\frac{\sin(\theta+\delta)\sin(\theta-\beta)}{\cos(\theta+\delta)\cos(\theta-\beta)}} \right]^2}$$

Permanent actions

	EQU	STR	GEO
Earth pressure at the top (y=yA)	$q_A = 16.17$	11.43	16.17 kN/m ²
Earth pressure at the bottom (y=yA+ 1.00m)	$q_B = 21.08$	14.90	21.08 kN/m ²
Earth force $P_a = \frac{1}{2}(q_A+q_B)H$	$P_a = 18.62$	13.16	18.62 kN/m
Angle of earth force	$\alpha = 0.00$	0.00	0.00°
Earth force in x direction	$P_{ax} = 18.62$	13.16	18.62 kN/m
Earth force in y direction	$P_{ay} = 0.00$	0.00	0.00 kN/m
Moment of earth force at top point (x=0,y=0)	$M = -65.58$	-46.35	-65.58 kNm/m
Point of application of earth force x= -1.200 m, y= 3.522 m			

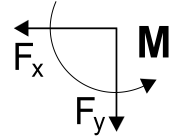


Variable actions

	EQU	STR	GEO
Earth pressure at the top (y=yA)	qA= 0.61	0.43	0.61 kN/m ²
Earth pressure at the bottom (y=yA+ 1.00m)	qB= 0.61	0.43	0.61 kN/m ²
Earth force Pa=½(qA+qB)H	Pa= 0.61	0.43	0.61 kN/m
Angle of earth force	α = 0.00	0.00	0.00 °
Earth force in x direction	Pax= 0.61	0.43	0.61 kN/m
Earth force in y direction	Pay= 0.00	0.00	0.00 kN/m
Moment of earth force at top point (x=0,y=0)	M = -2.13	-1.50	-2.13 kNm/m
Point of application of earth force x= -1.200 m, y= 3.500 m			

Total forces and moments

Forces and moments at bottom point B (x=-1.200 m, y=4.000 m)



Permanent actions

	EQU	STR	GEO
Total horizontal earth force Fsx=	51.66	37.71	51.66 kN/m
Total vertical earth force Fsy=	0.00	0.00	0.00 kN/m
Total moment of earth force Ms =	77.99	57.62	77.99 kNm/m

Variable actions

	EQU	STR	GEO
Total horizontal earth force Fsx=	2.97	2.20	2.97 kN/m
Total vertical earth force Fsy=	0.00	0.00	0.00 kN/m
Total moment of earth force Ms =	6.34	4.74	6.34 kNm/m

Seismic loading

(EC8 EN1998-5:2004, §7.3.2, Annex E)

Horizontal seismic coefficient kh=0.06/1.500=0.040

(EC8-5 Eq.7.1, T.7.1)

Vertical seismic coefficient kv=0.50x0.040=0.020

(EC8-5 Eq.7.2)

Soil above the water table

(EC8-5 Annex E.5)

tan(ω)=kh/(1-kv)=0.040/(1-0.020)=0.041, ω=2.34°

Method Mononobe-Okabe (EC8-5 Annex E.4)

for active earth force during seismic loading

Coefficient of active earth pressure, Ke*= 0.326

Additional earth pressure due to seismic load over STR load case ξ=(Ke*/Ke-1)=(0.326/0.217-1)=0.502

$$K_E = \frac{\cos^2(\varphi - \omega - \theta)}{\cos \omega \cos^2 \theta \cos(\delta + \theta + \omega) \left[1 + \sqrt{\frac{\sin(\varphi + \delta) \sin(\varphi - \omega - \beta)}{\cos(\theta + \omega + \delta) \cos(\theta - \beta)}} \right]^2}$$

Earth force due to seismic load (Permanent actions) Fx=1.502x13.16=19.77 kN/m

Earth force due to seismic load (Variable actions) Fx=1.502x 0.43= 0.65 kN/m

4.6. Computation of passive earth pressure (Rankine theory)

4.6.1. Wall part from y=3.400 m to y=4.300 m, Hs=0.900 m

Top point A x= 1.250 m y= 3.400 m

Bottom point B x= 1.250 m y= 4.300 m

Soil properties

Soil type : Thin gravel

Unit weight of soil γ =16.00 kN/m³

Unit weight of soil (saturated) γs=20.00 kN/m³

Unit weight of water γw=10.00 kN/m³

Soil under the water table lever

Soil weight suspended in water γo=10.00 kN/m³

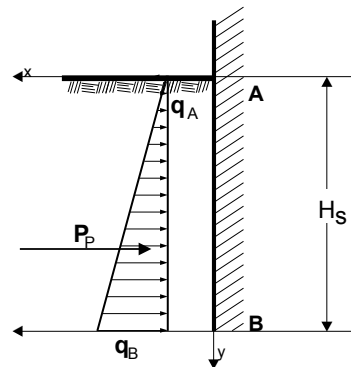
Angle of shearing resistance of ground φ=35.00°

Cohesion of ground c=0.000 N/mm²

Slope angle of ground surface β= 0.00°

Earth pressure on vertical surface θ= 0.00°

Angle of shear resist. between ground-wall δ= 0.00°



Loads on soil surface

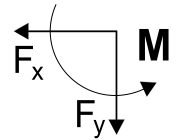
Permanent uniform load $g = 0.00 \text{ kN/m}^2$
 Variable uniform load $q = 0.00 \text{ kN/m}^2$
 Water pressure at the top $q_w = 0.00 \text{ kN/m}^2$

Earth pressure according to Coulomb theory

Angle of rupture plane $\rho = 45^\circ - \varphi/2 = 31.00$ EQU STR GEO 31.00°
 Coefficient of passive earth pressure $K_p = \frac{\cos^2(\varphi + \theta)}{\cos^2\theta \cos(\theta - \delta)} \left[\frac{1 - \sqrt{\frac{\sin(\theta + \delta)\sin(\theta + \beta)}{\cos(\theta - \delta)\cos(\theta - \beta)}}}{2} \right]^2$
 Earth pressure $q(y) = q_A + \gamma \cdot y \cdot K_p$

Permanent actions

	EQU	STR	GEO
Earth pressure at the top ($y=y_A$)	$q_A = 0.00$	0.00	0.00 kN/m^2
Earth pressure at the bottom ($y=y_A + 0.90\text{m}$)	$q_B = -24.93$	-33.21	-24.93 kN/m^2
Earth force $P_a = \frac{1}{2}(q_A + q_B)H$	$P_p = 11.22$	14.94	11.22 kN/m
Angle of earth force	$\alpha = 0.00$	0.00	0.00°
Earth force in x direction	$P_{px} = -11.22$	-14.94	-11.22 kN/m
Earth force in y direction	$P_{py} = 0.00$	0.00	0.00 kN/m
Moment of earth force at top point ($x=0, y=0$)	$M = 44.88$	59.76	44.88 kNm/m
Point of application of earth force	$x = 1.250 \text{ m}, y = 4.000 \text{ m}$		



Hydrostatic pressure

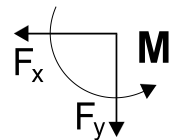
Hydrostatic pressure $q_w = q_wA + \gamma_w \cdot H_w / \cos\theta$
 Hydrostatic pressure at the top ($y=y_A$) $q_wA = 0.00 \text{ kN/m}^2$
 Hydrostatic pressure at the bottom ($y=y_A + 0.90\text{m}$) $q_wB = 9.00 \text{ kN/m}^2$
 Hydrostatic force $P_w = \frac{1}{2}(q_wA + q_wB)H$ $P_w = 4.05 \text{ kN/m}$
 Angle of hydrostatic force $\alpha = 0.00^\circ$
 Hydrostatic force in x direction $P_{wx} = 4.05 \text{ kN/m}$
 Hydrostatic force in y direction $P_{wy} = 0.00 \text{ kN/m}$
 Moment of hydrostatic force at top point ($x=0, y=0$) $M = -16.20 \text{ kNm/m}$
 Point of application of hydrostatic force $x = 1.250 \text{ m}, y = 4.000 \text{ m}$

Total forces and moments

Forces and moments at bottom point B ($x=1.250 \text{ m}, y=4.300 \text{ m}$)

Permanent actions

	EQU	STR	GEO
Total horizontal earth force F_{sx}	-11.22	-14.94	-11.22 kN/m
Total vertical earth force F_{sy}	0.00	0.00	0.00 kN/m
Total moment of earth force M_s	-3.37	-4.48	-3.37 kNm/m



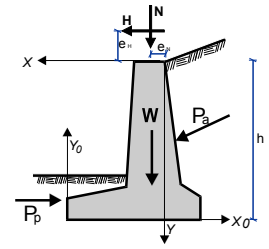
Hydrostatic pressure

Total horizontal hydrostatic force $F_{wx} = 4.05 \text{ kN/m}$
 Total vertical hydrostatic force $F_{wy} = 0.00 \text{ kN/m}$
 Total moment of hydrostatic force $M_w = 1.22 \text{ kNm/m}$

4.7. Checks of wall stability (EQU)

4.7.1. Forces (driving and resisting) on the wall (EQU)

Action		y1 - y2	Fx	Fy	x	y	
			[kN/m]		[kN/m]	[m]	[m]
Active earth pressure	Pa	-0.10- 3.00	33.04	0.00	0.00	-1.200	1.909
Backfill surcharge (live)	Pq	-0.10- 3.00	2.36	0.00	0.00	-1.200	1.447
Active earth pressure	Pa	3.00- 4.00	18.62	0.00	0.00	-1.200	3.522
Backfill surcharge (live)	Pq	3.00- 4.00	0.61	0.00	0.00	-1.200	3.500
Passive earth pressure	Pp	3.40- 4.30	-11.22	0.00	0.00	1.250	4.000
Wall weight	W		0.00	70.00	0.140		2.698
Backfill weight	Ws		0.00	70.22	-0.600		1.776
Backf. surcharge (dead)	Wsg		0.00	3.60	-0.600		0.000
Backf. surcharge (live)	Wsq		0.00	2.40	-0.600		0.000
Vert. load on top (dead)	Ng		0.00	3.00	0.125		0.000
Vert. load on top (live)	Nq		0.00	2.00	0.125		0.000
Horiz. load on top (dead)	Hg		2.00	0.00	0.175		0.000
Horiz. load on top (live)	Hq		2.00	0.00	0.175		0.000

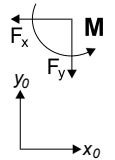


4.7.2. Check of soil bearing capacity (EQU)

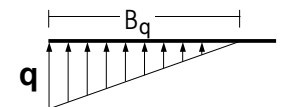
(EC7 EN1997-1-1:2004, §6.5.2)

Check for $0.90 \times (\text{self weight} + \text{top vertical dead load}) + 0.00 \times (\text{top vertical live load})$

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M	
			[kN/m]		[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.10	-0.10- 3.00	36.34	0.00	0.00	2.450	2.091	76.00
Backfill surcharge (live)	Pqx1.50	-0.10- 3.00	3.54	0.00	0.00	2.450	2.553	9.04
Active earth pressure	Pax1.10	3.00- 4.00	20.48	0.00	0.00	2.450	0.478	9.79
Backfill surcharge (live)	Pqx1.50	3.00- 4.00	0.92	0.00	0.00	2.450	0.500	0.46
Wall weight	W x0.90		0.00	63.00	1.110	1.302		-69.93
Backfill weight	Wsx0.90		0.00	63.20	1.850	2.224		-116.92
Backf. surcharge (dead)	Wsgx0.90		0.00	3.24	1.850	4.000		-5.99
Vert. load on top (dead)	Ngx0.90		0.00	2.70	1.125	4.000		-3.04
Horiz. load on top (dead)	Hgx1.10		2.20	0.00	1.075	4.000		8.80
Horiz. load on top (live)	Hqx1.50		3.00	0.00	1.075	4.000		12.00
			Sum=	132.14				-79.79



Sum of vertical forces = 132.14 kN/m
 Sum of moments at front toe = -79.79 kNm/m
 Sum of moments at middle of base = 82.08 kNm/m
 Eccentricity $ec = 82.08 / 132.14 = 0.621\text{m}$, $ec > 2.450 / 6 = 0.408\text{m}$
 Soil pressure $q = 0.146 \text{ N/mm}^2$ $Bq = 1.812 \text{ m}$
 Effective footing $L = 2.450 - 2 \times 0.621 = 1.208 \text{ m}$
 Soil bearing capacity $Rd = L \cdot qu / \gamma M = 1.208 \times (1000 \times 0.20) / 1.40 = 172.57 \text{ kN/m}$
 Bearing resistance check $Vd = 132.14 < Rd = 172.57 \text{ kN/m}$, Check is verified



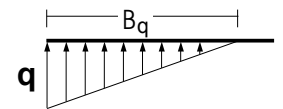
(EC7 Annex D)

(EC7 Eq.2.2, Eq.6.1)

Check for 1.10x(self weight+top vertical dead load)+1.50x(top vertical live load)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.10	-0.10-	3.00	36.34	0.00	2.450	2.091	76.00
Backfill surcharge (live)	Pqx1.50	-0.10-	3.00	3.54	0.00	2.450	2.553	9.04
Active earth pressure	Pax1.10	3.00-	4.00	20.48	0.00	2.450	0.478	9.79
Backfill surcharge (live)	Pqx1.50	3.00-	4.00	0.92	0.00	2.450	0.500	0.46
Wall weight	W x1.10			0.00	77.00	1.110	1.302	-85.47
Backfill weight	Wsx1.10			0.00	77.24	1.850	2.224	-142.90
Backf. surcharge (dead)	Wsgx0.90			0.00	3.24	1.850	4.000	-5.99
Backf. surcharge (live)	Wsqx1.50			0.00	3.60	1.850	4.000	-6.66
Vert. load on top (dead)	Ngx1.10			0.00	3.30	1.125	4.000	-3.72
Vert. load on top (live)	Nqx1.50			0.00	3.00	1.125	4.000	-3.38
Horiz. load on top (dead)	Hgx1.10			2.20	0.00	1.075	4.000	8.80
Horiz. load on top (live)	Hqx1.50			3.00	0.00	1.075	4.000	12.00
				Sum=	167.38			-132.03

Sum of vertical forces = 167.38 kN/m
 Sum of moments at front toe = -132.03 kNm/m
 Sum of moments at middle of base = 73.01 kNm/m
 Eccentricity $ec=73.01/167.38=0.436m$, $ec>2.450/6=0.408m$
 Soil pressure $q=0.141$ N/mm² $Bq=2.366$ m
 Effective footing $L=2.450-2x0.436= 1.578$ m
 Soil bearing capacity $Rd=L \cdot qu/\gamma M=1.578x(1000x0.20)/1.40= 225.43$ kN/m
 Bearing resistance check $Vd=167.38 < Rd=225.43$ kN/m, Check is verified



(EC7 Annex D)

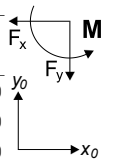
(EC7 Eq.2.2, Eq.6.1)

4.7.3. Failure check due to overturning (EQU)

(EC7 EN1997-1-1:2004, §9.7.4)

Overturning with respect to the toe ($xo=0, yo=0$) ($x=1.250, y=4.000$ m)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	Mo+	Mo-	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]	[kNm/m]
Active earth pressure	Pax1.10	-0.10-	3.00	36.34	0.00	2.450	2.091	76.00	0.00
Backfill surcharge (live)	Pqx1.50	-0.10-	3.00	3.54	0.00	2.450	2.553	9.04	0.00
Active earth pressure	Pax1.10	3.00-	4.00	20.48	0.00	2.450	0.478	9.79	0.00
Backfill surcharge (live)	Pqx1.50	3.00-	4.00	0.92	0.00	2.450	0.500	0.46	0.00
Wall weight	W x0.90			0.00	63.00	1.110	1.302	0.00	69.93
Backfill weight	Wsx0.90			0.00	63.20	1.850	2.224	0.00	116.92
Backf. surcharge (dead)	Wsgx0.90			0.00	3.24	1.850	4.000	0.00	5.99
Vert. load on top (dead)	Ngx0.90			0.00	2.70	1.125	4.000	0.00	3.04
Horiz. load on top (dead)	Hgx1.10			2.20	0.00	1.075	4.000	8.80	0.00
Horiz. load on top (live)	Hqx1.50			3.00	0.00	1.075	4.000	12.00	0.00
						Sum=		116.09	195.88

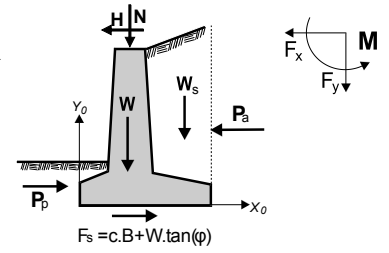


Sum of overturning moments = 116.09 kNm/m
 Sum of moments resisting overturning = 195.88 kNm/m
 Overturning check $Msd=116.09 < Mrd=195.88$ kNm/m, Check is verified

4.7.4. Failure check against sliding (EQU)

(EC7 EN1997-1-1:2004, §9.7.3, §6.5.3)

Action	(γ)	y1 - y2	Fx+	Fx-	Fy	
			[kN/m]		[kN/m]	[kN/m]
Active earth pressure	Pax1.10	-0.10- 3.00	3.00	36.34	0.00	0.00
Backfill surcharge (live)	Pqx1.50	-0.10- 3.00	3.00	3.54	0.00	0.00
Active earth pressure	Pax1.10	3.00- 4.00	4.00	20.48	0.00	0.00
Backfill surcharge (live)	Pqx1.50	3.00- 4.00	4.00	0.92	0.00	0.00
Passive earth pressure	Ppx0.90	3.40- 4.30	4.30	0.00	10.10	0.00
Wall weight	W x0.90			0.00	0.00	63.00
Backfill weight	Wsx0.90			0.00	0.00	63.20
Backf. surcharge (dead)	Wsgx0.90			0.00	0.00	3.24
Vert. load on top (dead)	Ngx0.90			0.00	0.00	2.70
Horiz. load on top (dead)	Hgx1.10			2.20	0.00	0.00
Horiz. load on top (live)	Hqx1.50			3.00	0.00	0.00
Sum=				66.48	10.10	132.14



Soil friction $Rd = Vd \cdot \tan\phi / \gamma M = 132.14 \times \tan(30.00^\circ) / 1.25 = 61.03 \text{ kN/m}$

Soil cohesion $Rd = A \cdot cu / \gamma M = 1000 \times 1.812 \times 0.010 / 1.25 = 14.49 \text{ kN/m}$

(resisting forces from effective cohesion are neglected)

(EC7 §6.5.3. 10)

Sum of driving forces = 66.48 kN/m

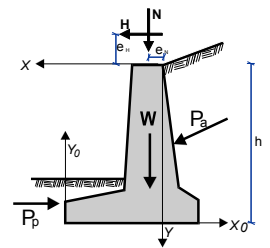
Sum of resisting forces (10.10+61.03) = 71.13 kN/m

Sliding resistance check $Hd = 66.48 < Rd = 71.13 \text{ kN/m}$, Check is verified

4.8. Checks of wall stability (STR)

4.8.1. Forces (driving and resisting) on the wall (STR)

Action		y1 - y2	Fx	Fy	x	y
			[kN/m]		[m]	[m]
Active earth pressure	Pa	-0.10- 3.00	3.00	24.55	0.00	-1.200
Backfill surcharge (live)	Pq	-0.10- 3.00	3.00	1.77	0.00	-1.200
Active earth pressure	Pa	3.00- 4.00	4.00	13.16	0.00	-1.200
Backfill surcharge (live)	Pq	3.00- 4.00	4.00	0.43	0.00	-1.200
Passive earth pressure	Pp	3.40- 4.30	4.30	-14.94	0.00	1.250
Wall weight	W			0.00	70.00	0.140
Backfill weight	Ws			0.00	70.22	-0.600
Backf. surcharge (dead)	Wsg			0.00	3.60	-0.600
Backf. surcharge (live)	Wsq			0.00	2.40	-0.600
Vert. load on top (dead)	Ng			0.00	3.00	0.125
Vert. load on top (live)	Nq			0.00	2.00	0.125
Horiz. load on top (dead)	Hg			2.00	0.00	0.175
Horiz. load on top (live)	Hq			2.00	0.00	0.175

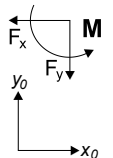


4.8.2. Check of soil bearing capacity (STR)

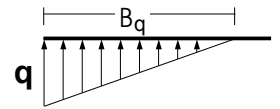
(EC7 EN1997-1-1:2004, §6.5.2)

Check for $1.00 \times (\text{self weight} + \text{top vertical dead load}) + 0.00 \times (\text{top vertical live load})$

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M
			[kN/m]		[m]	[m]	[kNm/m]
Active earth pressure	Pax1.35	-0.10- 3.00	3.00	33.14	0.00	2.450	2.091
Backfill surcharge (live)	Pqx1.50	-0.10- 3.00	3.00	2.66	0.00	2.450	2.553
Active earth pressure	Pax1.35	3.00- 4.00	4.00	17.77	0.00	2.450	0.478
Backfill surcharge (live)	Pqx1.50	3.00- 4.00	4.00	0.64	0.00	2.450	0.500
Wall weight	W x1.00			0.00	70.00	1.110	1.302
Backfill weight	Wsx1.00			0.00	70.22	1.850	2.224
Backf. surcharge (dead)	Wsgx1.00			0.00	3.60	1.850	4.000
Vert. load on top (dead)	Ngx1.00			0.00	3.00	1.125	4.000
Horiz. load on top (dead)	Hgx1.35			2.70	0.00	1.075	4.000
Horiz. load on top (live)	Hqx1.50			3.00	0.00	1.075	4.000
Sum=				146.82			-109.95



Sum of vertical forces = 146.82 kN/m
 Sum of moments at front toe = -109.95 kNm/m
 Sum of moments at middle of base = 69.90 kNm/m
 Eccentricity $ec=69.90/146.82=0.476m$, $ec>2.450/6=0.408m$
 Soil pressure $q=0.131 \text{ N/mm}^2$ $Bq=2.247 \text{ m}$
 Effective footing $L=2.450-2 \times 0.476= 1.498 \text{ m}$
 Soil bearing capacity $Rd=L \cdot qu/\gamma M=1.498 \times (1000 \times 0.20)/1.00= 299.60 \text{ kN/m}$
 Bearing resistance check $Vd=146.82 < Rd=299.60 \text{ kN/m}$, Check is verified



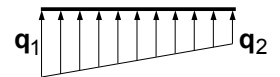
(EC7 Annex D)

(EC7 Eq.2.2, Eq.6.1)

Check for 1.35x(self weight+top vertical dead load)+1.50x(top vertical live load)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.35	-0.10- 3.00	33.14	0.00	2.450	2.091	69.30	
Backfill surcharge (live)	Pqx1.50	-0.10- 3.00	2.66	0.00	2.450	2.553	6.78	
Active earth pressure	Pax1.35	3.00- 4.00	17.77	0.00	2.450	0.478	8.49	
Backfill surcharge (live)	Pqx1.50	3.00- 4.00	0.64	0.00	2.450	0.500	0.33	
Wall weight	W x1.35		0.00	94.50	1.110	1.302	-104.90	
Backfill weight	Wsx1.35		0.00	94.80	1.850	2.224	-175.38	
Backf. surcharge (dead)	Wsgx1.00		0.00	3.60	1.850	4.000	-6.66	
Backf. surcharge (live)	Wsqx1.50		0.00	3.60	1.850	4.000	-6.66	
Vert. load on top (dead)	Ngx1.35		0.00	4.05	1.125	4.000	-4.56	
Vert. load on top (live)	Nqx1.50		0.00	3.00	1.125	4.000	-3.38	
Horiz. load on top (dead)	Hgx1.35		2.70	0.00	1.075	4.000	10.80	
Horiz. load on top (live)	Hqx1.50		3.00	0.00	1.075	4.000	12.00	
			Sum=	203.55			-193.84	

Sum of vertical forces = 203.55 kN/m
 Sum of moments at front toe = -193.84 kNm/m
 Sum of moments at middle of base = 55.51 kNm/m
 Eccentricity $ec=55.51/203.55=0.273m$, $ec \leq 2.450/6=0.408m$
 Soil pressure $q1=0.139 \text{ N/mm}^2$ $q2=0.028 \text{ N/mm}^2$
 Effective footing $L=2.450-2 \times 0.273= 1.905 \text{ m}$
 Soil bearing capacity $Rd=L \cdot qu/\gamma M=1.905 \times (1000 \times 0.20)/1.00= 381.00 \text{ kN/m}$
 Bearing resistance check $Vd=203.55 < Rd=381.00 \text{ kN/m}$, Check is verified



(EC7 Annex D)

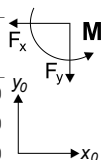
(EC7 Eq.2.2, Eq.6.1)

4.8.3. Failure check due to overturning (STR)

(EC7 EN1997-1-1:2004, §9.7.4)

Overturning with respect to the toe ($xo=0, yo=0$) ($x=1.250, y=4.000 \text{ m}$)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	Mo+	Mo-	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]	[kNm/m]
Active earth pressure	Pax1.35	-0.10- 3.00	33.14	0.00	2.450	2.091	69.30	0.00	
Backfill surcharge (live)	Pqx1.50	-0.10- 3.00	2.66	0.00	2.450	2.553	6.78	0.00	
Active earth pressure	Pax1.35	3.00- 4.00	17.77	0.00	2.450	0.478	8.49	0.00	
Backfill surcharge (live)	Pqx1.50	3.00- 4.00	0.64	0.00	2.450	0.500	0.33	0.00	
Wall weight	W x1.00		0.00	70.00	1.110	1.302	0.00	77.70	
Backfill weight	Wsx1.00		0.00	70.22	1.850	2.224	0.00	129.91	
Backf. surcharge (dead)	Wsgx1.00		0.00	3.60	1.850	4.000	0.00	6.66	
Vert. load on top (dead)	Ngx1.00		0.00	3.00	1.125	4.000	0.00	3.38	
Horiz. load on top (dead)	Hgx1.35		2.70	0.00	1.075	4.000	10.80	0.00	
Horiz. load on top (live)	Hqx1.50		3.00	0.00	1.075	4.000	12.00	0.00	
			Sum=				107.70	217.65	

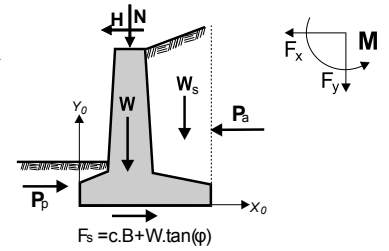


Sum of overturning moments = 107.70 kNm/m
 Sum of moments resisting overturning = 217.65 kNm/m
 Overturning check $Msd=107.70 < Mrd=217.65 \text{ kNm/m}$, Check is verified

4.8.4. Failure check against sliding (STR)

(EC7 EN1997-1-1:2004, §9.7.3, §6.5.3)

Action	(γ)	y1 - y2	Fx+	Fx-	Fy	
			[kN/m]	[kN/m]	[kN/m]	[kN/m]
Active earth pressure	Pax1.35	-0.10- 3.00	33.00	33.14	0.00	0.00
Backfill surcharge (live)	Pqx1.50	-0.10- 3.00	2.66	2.66	0.00	0.00
Active earth pressure	Pax1.35	3.00- 4.00	17.77	17.77	0.00	0.00
Backfill surcharge (live)	Pqx1.50	3.00- 4.00	0.64	0.64	0.00	0.00
Passive earth pressure	Ppx1.00	3.40- 4.30	0.00	0.00	14.94	0.00
Wall weight	W x1.00		0.00	0.00	0.00	70.00
Backfill weight	Wsx1.00		0.00	0.00	0.00	70.22
Backf. surcharge (dead)	Wsgx1.00		0.00	0.00	0.00	3.60
Vert. load on top (dead)	Ngx1.00		0.00	0.00	0.00	3.00
Horiz. load on top (dead)	Hgx1.35		2.70	2.70	0.00	0.00
Horiz. load on top (live)	Hqgx1.50		3.00	3.00	0.00	0.00
Sum=			59.91	59.91	14.94	146.82

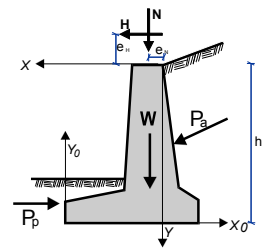


Soil friction $Rd = Vd \cdot \tan\phi / \gamma M = 146.82 \times \tan(30.00^\circ) / 1.00 = 84.77$ kN/m
 Soil cohesion $Rd = A \cdot cu / \gamma M = 1000 \times 2.247 \times 0.010 / 1.00 = 22.47$ kN/m
 (resisting forces from effective cohesion are neglected) (EC7 §6.5.3. 10)
 Sum of driving forces = 59.91 kN/m
 Sum of resisting forces (14.94+84.77) = 99.71 kN/m
 Sliding resistance check $Hd = 59.91 < Rd = 99.71$ kN/m, Check is verified

4.9. Checks of wall stability (GEO)

4.9.1. Forces (driving and resisting) on the wall (GEO)

Action		y1 - y2	Fx	Fy	x	y
			[kN/m]	[kN/m]	[m]	[m]
Active earth pressure	Pa	-0.10- 3.00	33.04	33.04	0.00	-1.200
Backfill surcharge (live)	Pq	-0.10- 3.00	2.36	2.36	0.00	-1.200
Active earth pressure	Pa	3.00- 4.00	18.62	18.62	0.00	-1.200
Backfill surcharge (live)	Pq	3.00- 4.00	0.61	0.61	0.00	-1.200
Passive earth pressure	Pp	3.40- 4.30	-11.22	-11.22	0.00	1.250
Wall weight	W		0.00	0.00	70.00	0.140
Backfill weight	Ws		0.00	0.00	70.22	-0.600
Backf. surcharge (dead)	Wsg		0.00	0.00	3.60	-0.600
Backf. surcharge (live)	Wsq		0.00	0.00	2.40	-0.600
Vert. load on top (dead)	Ng		0.00	0.00	3.00	0.125
Vert. load on top (live)	Nq		0.00	0.00	2.00	0.125
Horiz. load on top (dead)	Hg		2.00	2.00	0.00	0.175
Horiz. load on top (live)	Hq		2.00	2.00	0.00	0.175

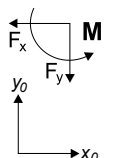


4.9.2. Check of soil bearing capacity (GEO)

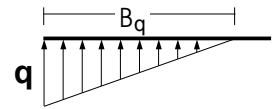
(EC7 EN1997-1-1:2004, §6.5.2)

Check for $1.00 \times (\text{self weight} + \text{top vertical dead load}) + 0.00 \times (\text{top vertical live load})$

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M
			[kN/m]	[kN/m]	[kN/m]	[m]	[kNm/m]
Active earth pressure	Pax1.00	-0.10- 3.00	33.04	33.04	0.00	2.450	2.091
Backfill surcharge (live)	Pqx1.30	-0.10- 3.00	3.07	3.07	0.00	2.450	2.553
Active earth pressure	Pax1.00	3.00- 4.00	18.62	18.62	0.00	2.450	0.478
Backfill surcharge (live)	Pqx1.30	3.00- 4.00	0.79	0.79	0.00	2.450	0.500
Wall weight	W x1.00		0.00	0.00	70.00	1.110	1.302
Backfill weight	Wsx1.00		0.00	0.00	70.22	1.850	2.224
Backf. surcharge (dead)	Wsgx1.00		0.00	0.00	3.60	1.850	4.000
Vert. load on top (dead)	Ngx1.00		0.00	0.00	3.00	1.125	4.000
Horiz. load on top (dead)	Hgx1.00		2.00	2.00	0.00	1.075	4.000
Horiz. load on top (live)	Hqgx1.30		2.60	2.60	0.00	1.075	4.000
Sum=			146.82	146.82			-113.02



Sum of vertical forces = 146.82 kN/m
 Sum of moments at front toe = -113.02 kNm/m
 Sum of moments at middle of base = 66.83 kNm/m
 Eccentricity $ec=66.83/146.82=0.455m$, $ec>2.450/6=0.408m$
 Soil pressure $q=0.127 \text{ N/mm}^2$ $Bq=2.309 \text{ m}$
 Effective footing $L=2.450-2x0.455= 1.540 \text{ m}$
 Soil bearing capacity $Rd=L \cdot qu/\gamma M=1.540x(1000x0.20)/1.40= 220.00 \text{ kN/m}$
 Bearing resistance check $Vd=146.82 < Rd=220.00 \text{ kN/m}$, Check is verified



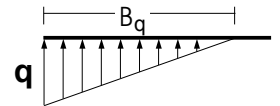
(EC7 Annex D)

(EC7 Eq.2.2, Eq.6.1)

Check for 1.00x(self weight+top vertical dead load)+1.30x(top vertical live load)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.00	-0.10- 3.00	33.04	0.00	2.450	2.091	69.09	
Backfill surcharge (live)	Pqx1.30	-0.10- 3.00	3.07	0.00	2.450	2.553	7.84	
Active earth pressure	Pax1.00	3.00- 4.00	18.62	0.00	2.450	0.478	8.90	
Backfill surcharge (live)	Pqx1.30	3.00- 4.00	0.79	0.00	2.450	0.500	0.40	
Wall weight	W x1.00		0.00	70.00	1.110	1.302	-77.70	
Backfill weight	Wsx1.00		0.00	70.22	1.850	2.224	-129.91	
Backf. surcharge (dead)	Wsgx1.00		0.00	3.60	1.850	4.000	-6.66	
Backf. surcharge (live)	Wsqx1.30		0.00	3.12	1.850	4.000	-5.77	
Vert. load on top (dead)	Ngx1.00		0.00	3.00	1.125	4.000	-3.38	
Vert. load on top (live)	Nqx1.30		0.00	2.60	1.125	4.000	-2.92	
Horiz. load on top (dead)	Hgx1.00		2.00	0.00	1.075	4.000	8.00	
Horiz. load on top (live)	Hqx1.30		2.60	0.00	1.075	4.000	10.40	
			Sum=	152.54			-121.71	

Sum of vertical forces = 152.54 kN/m
 Sum of moments at front toe = -121.71 kNm/m
 Sum of moments at middle of base = 65.15 kNm/m
 Eccentricity $ec=65.15/152.54=0.427m$, $ec>2.450/6=0.408m$
 Soil pressure $q=0.127 \text{ N/mm}^2$ $Bq=2.394 \text{ m}$
 Effective footing $L=2.450-2x0.427= 1.596 \text{ m}$
 Soil bearing capacity $Rd=L \cdot qu/\gamma M=1.596x(1000x0.20)/1.40= 228.00 \text{ kN/m}$
 Bearing resistance check $Vd=152.54 < Rd=228.00 \text{ kN/m}$, Check is verified



(EC7 Annex D)

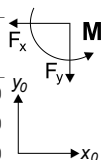
(EC7 Eq.2.2, Eq.6.1)

4.9.3. Failure check due to overturning (GEO)

(EC7 EN1997-1-1:2004, §9.7.4)

Overturning with respect to the toe ($xo=0, yo=0$) ($x=1.250, y=4.000 \text{ m}$)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	Mo+	Mo-	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]	[kNm/m]
Active earth pressure	Pax1.00	-0.10- 3.00	33.04	0.00	2.450	2.091	69.09	0.00	
Backfill surcharge (live)	Pqx1.30	-0.10- 3.00	3.07	0.00	2.450	2.553	7.84	0.00	
Active earth pressure	Pax1.00	3.00- 4.00	18.62	0.00	2.450	0.478	8.90	0.00	
Backfill surcharge (live)	Pqx1.30	3.00- 4.00	0.79	0.00	2.450	0.500	0.40	0.00	
Wall weight	W x1.00		0.00	70.00	1.110	1.302	0.00	77.70	
Backfill weight	Wsx1.00		0.00	70.22	1.850	2.224	0.00	129.91	
Backf. surcharge (dead)	Wsgx1.00		0.00	3.60	1.850	4.000	0.00	6.66	
Vert. load on top (dead)	Ngx1.00		0.00	3.00	1.125	4.000	0.00	3.38	
Horiz. load on top (dead)	Hgx1.00		2.00	0.00	1.075	4.000	8.00	0.00	
Horiz. load on top (live)	Hqx1.30		2.60	0.00	1.075	4.000	10.40	0.00	
			Sum=				104.63	217.65	

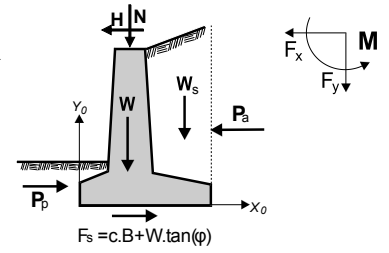


Sum of overturning moments = 104.63 kNm/m
 Sum of moments resisting overturning = 217.65 kNm/m
 Overturning check $Msd=104.63 < Mrd=217.65 \text{ kNm/m}$, Check is verified

4.9.4. Failure check against sliding (GEO)

(EC7 EN1997-1-1:2004, §9.7.3, §6.5.3)

Action	(γ)	y1 - y2	Fx+	Fx-	Fy
			[kN/m]	[kN/m]	[kN/m]
Active earth pressure	Pax1.00	-0.10- 3.00	33.04	0.00	0.00
Backfill surcharge (live)	Pqx1.30	-0.10- 3.00	3.07	0.00	0.00
Active earth pressure	Pax1.00	3.00- 4.00	18.62	0.00	0.00
Backfill surcharge (live)	Pqx1.30	3.00- 4.00	0.79	0.00	0.00
Passive earth pressure	Ppx1.00	3.40- 4.30	0.00	11.22	0.00
Wall weight	W x1.00		0.00	0.00	70.00
Backfill weight	Wsx1.00		0.00	0.00	70.22
Backf. surcharge (dead)	Wsgx1.00		0.00	0.00	3.60
Vert. load on top (dead)	Ngx1.00		0.00	0.00	3.00
Horiz. load on top (dead)	Hgx1.00		2.00	0.00	0.00
Horiz. load on top (live)	Hqgx1.30		2.60	0.00	0.00
Sum=			60.12	11.22	146.82



Soil friction $Rd = Vd \cdot \tan\phi / \gamma M = 146.82 \times \tan(30.00^\circ) / 1.25 = 67.81$ kN/m
 Soil cohesion $Rd = A \cdot cu / \gamma M = 1000 \times 2.309 \times 0.010 / 1.25 = 18.48$ kN/m
 (resisting forces from effective cohesion are neglected) (EC7 §6.5.3. 10)
 Sum of driving forces = 60.12 kN/m
 Sum of resisting forces (11.22+67.81) = 79.03 kN/m
 Sliding resistance check $Hd = 60.12 < Rd = 79.03$ kN/m, Check is verified

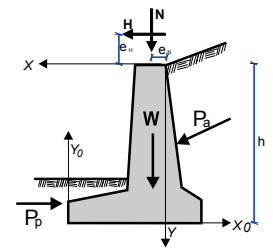
4.10. Seismic design

(EC8 EN1998-5:2004)

Checks of wall stability (with seismic loading)

4.10.1. Forces (driving and resisting) on the wall

Action	y1 - y2	Fx	Fy	x	y
		[kN/m]	[kN/m]	[m]	[m]
Active earth pressure	Pa -0.10- 3.00	24.55	0.00	-1.200	1.909
Backfill surcharge (live)	Pq -0.10- 3.00	1.77	0.00	-1.200	1.447
Active earth pressure	Pa 3.00- 4.00	13.16	0.00	-1.200	3.522
Backfill surcharge (live)	Pq 3.00- 4.00	0.43	0.00	-1.200	3.500
Passive earth pressure	Pp 3.40- 4.30	-14.94	0.00	1.250	4.000
Wall weight	W	0.00	70.00	0.140	2.698
Backfill weight	Ws	0.00	70.22	-0.600	1.776
Backf. surcharge (dead)	Wsg	0.00	3.60	-0.600	0.000
Backf. surcharge (live)	Wsq	0.00	2.40	-0.600	0.000
Vert. load on top (dead)	Ng	0.00	3.00	0.125	0.000
Vert. load on top (live)	Nq	0.00	2.00	0.125	0.000
Horiz. load on top (dead)	Hg	2.00	0.00	0.175	0.000
Horiz. load on top (live)	Hq	2.00	0.00	0.175	0.000



4.10.2. Additional forces due to seismic load

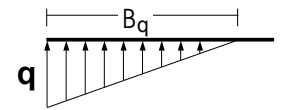
Action	y1 - y2	Fx	Fy	x	y
		[kN/m]	[kN/m]	[m]	[m]
Active earth pressure	Pa -0.10- 3.00	10.46	0.00	-1.200	1.909
Backfill surcharge (live)	Pq -0.10- 3.00	0.75	0.00	-1.200	1.447
Active earth pressure	Pa 3.00- 4.00	6.61	0.00	-1.200	3.522
Backfill surcharge (live)	Pq 3.00- 4.00	0.22	0.00	-1.200	3.500
Wall weight	W	2.80	-1.40	0.140	2.698
Backfill weight	Ws	2.81	-1.40	-0.600	1.776
Backf. surcharge (dead)	Wsg	0.14	-0.07	-0.600	0.000
Backf. surcharge (live)	Wsq	0.10	-0.05	-0.600	0.000
Vert. load on top (dead)	Ng	0.12	-0.06	0.125	0.000
Vert. load on top (live)	Nq	0.08	-0.04	0.125	0.000

4.10.3. Check of soil bearing capacity (with seismic loading)

(EC7 §6.5.2)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	M	
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.00	-0.10- 3.00	3.00	35.01	0.00	2.450	2.091	73.20
Backfill surcharge (live)	Pqx1.00	-0.10- 3.00	3.00	2.52	0.00	2.450	2.553	6.45
Active earth pressure	Pax1.00	3.00- 4.00	4.00	19.77	0.00	2.450	0.478	9.45
Backfill surcharge (live)	Pqx1.00	3.00- 4.00	4.00	0.65	0.00	2.450	0.500	0.33
Wall weight	W x1.00			2.80	68.60	1.110	1.302	-72.50
Backfill weight	Wsx1.00			2.81	68.82	1.850	2.224	-121.07
Backf. surcharge (dead)	Wsgx1.00			0.14	3.53	1.850	4.000	-5.97
Backf. surcharge (live)	Wsqx1.00			0.10	2.35	1.850	4.000	-3.95
Vert. load on top (dead)	Ngx1.00			0.12	2.94	1.125	4.000	-2.83
Vert. load on top (live)	Nqgx1.00			0.08	1.96	1.125	4.000	-1.89
Horiz. load on top (dead)	Hgx1.00			2.00	0.00	1.075	4.000	8.00
Horiz. load on top (live)	Hqgx1.00			2.00	0.00	1.075	4.000	8.00
				Sum=	148.20			-102.78

Sum of vertical forces = 148.20 kN/m
 Sum of moments at front toe = -102.78 kNm/m
 Sum of moments at middle of base = 78.77 kNm/m
 Eccentricity $ec=78.77/148.20=0.532m$, $ec>2.450/6=0.408m$
 Soil pressure $q=0.142 N/mm^2$ $Bq=2.080 m$
 Effective footing $L=2.450-2x0.532= 1.387 m$
 Soil bearing capacity $Rd=L\cdot qu/\gamma M=1.387x(1000x0.20)/1.00= 277.40 kN/m$
 Bearing resistance check $Vd=148.20 < Rd=277.40 kN/m$, Check is verified



(EC7 Annex D)

(EC7 Eq.2.2, Eq.6.1)

4.10.4. Failure check due to overturning (with seismic loading)

(EC7 §9.7.4)

Overturning with respect to the toe ($xo=0,yo=0$) ($x=1.250,y=4.000 m$)

Action	(γ)	y1 - y2	Fx	Fy	xo	yo	Mo+	Mo-
				[kN/m]	[kN/m]	[m]	[m]	[kNm/m]
Active earth pressure	Pax1.00	-0.10- 3.00	3.00	35.01	0.00	2.450	2.091	73.20
Backfill surcharge (live)	Pqx1.00	-0.10- 3.00	3.00	2.52	0.00	2.450	2.553	6.45
Active earth pressure	Pax1.00	3.00- 4.00	4.00	19.77	0.00	2.450	0.478	9.45
Backfill surcharge (live)	Pqx1.00	3.00- 4.00	4.00	0.65	0.00	2.450	0.500	0.33
Wall weight	W x1.00			2.80	68.60	1.110	1.302	5.20
Backfill weight	Wsx1.00			2.81	68.82	1.850	2.224	8.84
Backf. surcharge (dead)	Wsgx1.00			0.14	3.53	1.850	4.000	0.69
Backf. surcharge (live)	Wsqx1.00			0.10	2.35	1.850	4.000	0.49
Vert. load on top (dead)	Ngx1.00			0.12	2.94	1.125	4.000	0.55
Vert. load on top (live)	Nqgx1.00			0.08	1.96	1.125	4.000	0.36
Horiz. load on top (dead)	Hgx1.00			2.00	0.00	1.075	4.000	8.00
Horiz. load on top (live)	Hqgx1.00			2.00	0.00	1.075	4.000	8.00
						Sum=		121.56
								224.34

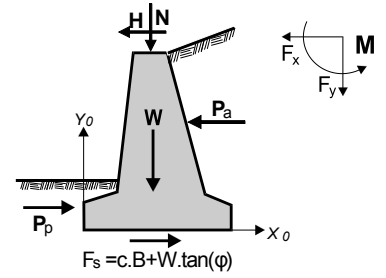
(*moments of negative seismic vertical loads, are added to the overturning moments)

Sum of overturning moments = 121.56 kNm/m
 Sum of moments resisting overturning = 224.34 kNm/m
 Overturning check $Msd=121.56 < Mrd=224.34 kNm/m$, Check is verified

4.10.5. Failure check against sliding (with seismic loading)

(EC7 §9.7.3, §6.5.3)

Action	(γ)	y1 - y2	Fx+	Fx-	Fy
			[kN/m]	[kN/m]	[kN/m]
Active earth pressure	Pax1.00	-0.10- 3.00	35.01	0.00	0.00
Backfill surcharge (live)	Pqx1.00	-0.10- 3.00	2.52	0.00	0.00
Active earth pressure	Pax1.00	3.00- 4.00	19.77	0.00	0.00
Backfill surcharge (live)	Pqx1.00	3.00- 4.00	0.65	0.00	0.00
Passive earth pressure	Ppx1.00	3.40- 4.30	0.00	14.94	0.00
Wall weight	W x1.00		2.80	0.00	68.60
Backfill weight	Wsx1.00		2.81	0.00	68.82
Backf. surcharge (dead)	Wsgx1.00		0.14	0.00	3.53
Backf. surcharge (live)	Wsqx1.00		0.10	0.00	2.35
Vert. load on top (dead)	Ngx1.00		0.12	0.00	2.94
Vert. load on top (live)	Nqgx1.00		0.08	0.00	1.96
Horiz. load on top (dead)	Hgx1.00		2.00	0.00	0.00
Horiz. load on top (live)	Hqgx1.00		2.00	0.00	0.00
Sum=			68.00	14.94	148.20



Soil friction $Rd = Vd \cdot \tan\phi / \gamma M = 148.20 \times \tan(30.00^\circ) / 1.00 = 85.56$ kN/m

Soil cohesion $Rd = A \cdot cu / \gamma M = 1000 \times 2.080 \times 0.010 / 1.00 = 20.80$ kN/m

(resisting forces from effective cohesion are neglected)

(EC7 §6.5.3. 10)

Sum of driving forces = 68.00 kN/m

Sum of resisting forces (14.94+85.56) = 100.50 kN/m

Sliding resistance check $Hd = 68.00 < Rd = 100.50$ kN/m, Check is verified

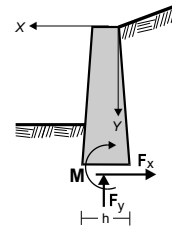
4.11. Design of wall steam

(EC2 EN1992-1-1:2004)

4.11.1. Loading 1.35x(permanent unfavourable)+1.00x(permanent favourable)+1.50x(variable unfav.)

Forces (at cross section centroid) at wall steam

y	h	Fx	Fy	M
[m]	[m]	[kN/m]	[kN/m]	[kNm/m]
0.50	0.379	8.03	7.55	3.01
1.00	0.407	11.67	12.46	7.70
1.50	0.436	16.81	17.73	14.49
2.00	0.464	23.51	23.36	24.18
2.50	0.493	31.73	29.34	37.51
3.00	0.521	41.48	35.68	55.23
3.50	0.550	50.13	42.37	77.50



4.11.2. Design of wall steam in bending

(EC2 §9.6, §6.1)

Concrete-Steel class: C25/30-S500, Concrete cover: $C_{nom} = 25$ mm

(§3, §4.4.1.1)

Vertical reinforcement minimum: $0.0020A_c$, maximum: $0.0400A_c$

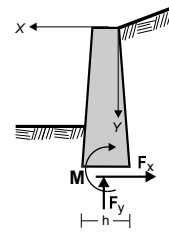
(EC2 §9.6.2)

y	Msd	Nsd	d	Kd	x/d	ec/es	Ks	As	min reinf.
[m]	[kN/m]	[kN]	[mm]						[cm ² /m]
0.50	3.01	-7.55	349	16.97	0.02	0.3/20.0	2.31	0.11	(3.79)
1.00	7.70	-12.46	377	12.01	0.02	0.5/20.0	2.32	0.32	(4.07)
1.50	14.49	-17.73	406	9.61	0.03	0.6/20.0	2.32	0.61	(4.36)
2.00	24.18	-23.36	434	8.08	0.03	0.7/20.0	2.33	1.01	(4.64)
2.50	37.51	-29.34	463	6.99	0.04	0.8/20.0	2.33	1.53	(4.93)
3.00	55.23	-35.68	491	6.17	0.05	1.0/20.0	2.34	2.20	(5.21)
3.50	77.50	-42.37	520	5.55	0.05	1.1/20.0	2.34	2.98	(5.50)

4.11.3. Loading 1.00x(permanent unfav.)+1.00x(permanent favour.)+1.00x(variable)+1.00x(seismic)

Forces (at cross section centroid) at wall steam (with seismic loading)

y [m]	h [m]	Fx [kN/m]	Fy [kN/m]	M [kNm/m]
0.50	0.379	7.46	7.55	2.62
1.00	0.407	11.83	12.46	7.19
1.50	0.436	17.81	17.73	14.27
2.00	0.464	25.45	23.36	24.69
2.50	0.493	34.72	29.34	39.24
3.00	0.521	45.61	35.68	58.74
3.50	0.550	55.09	42.37	81.93



4.11.4. Design of wall steam in bending (with seismic loading)

(EC2 §9.6, §6.1)

Concrete-Steel class: C25/30-S500, Concrete cover: Cnom=25 mm

(§3, §4.4.1.1)

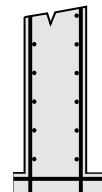
Vertical reinforcement minimum: 0.0020Ac, maximum: 0.0400Ac

(EC2 §9.6.2)

y [m]	Msd [kN/m]	Nsd [kN]	d [mm]	Kd	x/d	ec/es	Ks	As	min reinf. [cm ² /m]
0.50	2.62	-7.55	349	17.84	0.02	0.3/20.0	2.31	0.08	(3.79)
1.00	7.19	-12.46	377	12.33	0.02	0.5/20.0	2.32	0.29	(4.07)
1.50	14.27	-17.73	406	9.67	0.03	0.6/20.0	2.32	0.60	(4.36)
2.00	24.69	-23.36	434	8.01	0.03	0.7/20.0	2.33	1.04	(4.64)
2.50	39.24	-29.34	463	6.85	0.04	0.9/20.0	2.33	1.62	(4.93)
3.00	58.74	-35.68	491	6.00	0.05	1.0/20.0	2.34	2.37	(5.21)
3.50	81.93	-42.37	520	5.41	0.05	1.1/20.0	2.34	3.19	(5.50)

4.11.5. Reinforcement of wall steam

Reinforcement at back steam face $\varnothing 10/14.0$ (5.61cm²/m)
 Secondary transverse reinforcement $\varnothing 8/50.0$ (1.01cm²/m)
 Reinforcement at front steam face $\varnothing 10/14.0$ (5.61cm²/m)
 Secondary transverse reinforcement $\varnothing 8/50.0$ (1.01cm²/m)



4.11.6. Anchorage of wall steam reinforcement

(EC2 §8.4)

Basic required anchorage length $l_{b,rqd} = (\Phi/4) (c_{sd}/f_{bd}) = (10/4) \times (247/1.89) = 327\text{mm}$

(EC2 Eq.8.3)

$c_{sd} = 435.00 \times 319 / 561 = 247\text{MPa}$ $f_{bd} = 2.25 \times 0.70 \times (f_{ctk} 0.05 / \gamma_c) = 1.89\text{MPa}$

(EC2 §8.4.2)

Design anchorage length $l_{bd} = 1.00 \times 327 = 327\text{mm}$, $C_{nom} = 25\text{mm} < 3\varnothing = 30\text{mm}$

(EC2 §8.4.4, T.8.2)

Minimum anchorage length $l_{b,min} = \max(0.30 l_{b,rqd}, 10\varnothing, 100\text{mm}) = 100\text{mm}$

Necessary bend 100mm at lower bar end for anchorage

4.11.7. Shear check of wall steam

(EC2 EN1992-1-1:2004, §6.2.2)

Concrete-Steel class: C25/30-S500, Concrete cover: Cnom=25 mm

(§3, §4.4.1.1)

The earth pressure load variation is linear, so the variation of shear force is parabolic. The variation of steam cross section is linear.

The most unfavourable place for shear check is the base of the steam.

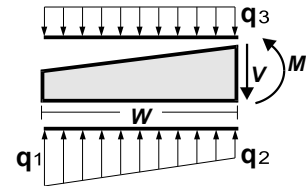
Vsd=50.13 kN/m, Vsd (+seismic)=55.09 kN/m, Nsd=-42.37 kN/m
Shear capacity without shear reinforcement Vr_{dc} (EC2 §6.2.2)
 $Vr_{dc}=[Cr_{dc} \cdot k \cdot (100\rho_1 \cdot f_{ck})^{0.333} + k_1 \cdot \sigma_{cp}] \cdot b_w \cdot d$ (EC2 Eq.6.2.a)
 $Vr_{dc} >= (v_{min} + k_1 \cdot \sigma_{cp}) \cdot b_w \cdot d$ (EC2 Eq.6.2.b)
 $Cr_{dc} = 0.18 / \gamma_c = 0.18 / 1.50 = 0.120$, $f_{ck} = 25.00 \text{ MPa}$
 $k = 1 + (200/d)^{1/2} \leq 2$, $k = 1.62$, $k_1 = 0.15$
 $\rho_1 = A_{s1} / (b_w \cdot d) = 561 / (1000 \times 520) = 0.0011$
 $\sigma_{cp} = N_{sd} / A_c = 1000 \times 42.37 / 550000 = 0.08 \text{ N/mm}^2$
 $v_{min} = 0.035 \cdot k^{1.50} \cdot f_{ck}^{1/2} = 0.36 \text{ N/mm}^2$ (EC2 Eq.6.3N)
 $Vr_{d,c}(\text{min}) = 0.001 \times (0.36 + 0.15 \times 0.08) \times 1000 \times 520 = 193.44 \text{ kN/m}$
 $Vr_{dc} = 0.001 \times [0.120 \times 1.62 \times (0.11 \times 25.00)^{0.333} + 0.15 \times 0.08] \times 1000 \times 520 = 147.87$, $Vr_{dc} = Vr_{d,c}(\text{min}) = 193.44 \text{ kN/m}$
 $Vsd = 55.09 \text{ kN/m} \leq Vr_{dc} = 193.44 \text{ kN/m}$, shear OK

4.12. Design of wall footing and reinforcement

(EC2 EN1992-1-1:2004)

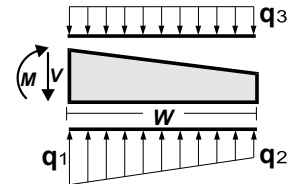
4.12.1. Design of front toe x=1.250 m to x=0.550 m

Sum of vertical forces = 203.55 kN/m
 Sum of moments at middle of base = 55.51 kNm/m
 $q_1 = 0.139 \text{ N/mm}^2$, $q_2 = 0.107 \text{ N/mm}^2$, $w = 0.700 \text{ m}$
 pressure from self weight $q_3 = 0.013 \text{ N/mm}^2$
 $M = 28.17 \text{ kNm/m}$, $V = 76.80 \text{ kN/m}$
 V at distance $d = 425 \text{ mm}$ from the face of the stem = 32.72 kN/m
 $M_{sd} = 28.17 \text{ kNm/m}$, $V_{sd} = 32.72 \text{ kN/m}$



4.12.2. Design of back heel x=-1.200 m to x=0.000 m

Sum of vertical forces = 203.55 kN/m
 Sum of moments at middle of base = 55.51 kNm/m
 $q_1 = 0.082 \text{ N/mm}^2$, $q_2 = 0.028 \text{ N/mm}^2$, $w = 1.200 \text{ m}$
 pressure from backfill and self weight $q_3 = 0.071 \text{ N/mm}^2$
 $M = -18.21 \text{ kNm/m}$, $V = 19.47 \text{ kN/m}$
 V at distance $d = 425 \text{ mm}$ from the face of the stem = 18.86 kN/m
 $M_{sd} = -18.21 \text{ kNm/m}$, $V_{sd} = 18.86 \text{ kN/m}$



4.12.3. Design of front toe x=1.250 m to x=0.550 m (with seismic loading)

Sum of vertical forces = 148.20 kN/m
 Sum of moments at middle of base = 78.77 kNm/m
 $q_1 = 0.142 \text{ N/mm}^2$, $q_2 = 0.095 \text{ N/mm}^2$, $w = 0.700 \text{ m}$
 pressure from self weight $q_3 = 0.013 \text{ N/mm}^2$
 $M = 27.80 \text{ kNm/m}$, $V = 73.85 \text{ kN/m}$
 V at distance $d = 425 \text{ mm}$ from the face of the stem = 32.94 kN/m
 $M_{sd} = 27.80 \text{ kNm/m}$, $V_{sd} = 32.94 \text{ kN/m}$

4.12.4. Design of back heel x=-1.200 m to x=0.000 m (with seismic loading)

Sum of vertical forces = 148.20 kN/m
 Sum of moments at middle of base = 78.77 kNm/m
 $q_1 = 0.057 \text{ N/mm}^2$, $q_2 = 0.000 \text{ N/mm}^2$, $w = 0.830 \text{ m}$
 pressure from backfill and self weight $q_3 = 0.097 \text{ N/mm}^2$
 $M = -26.98 \text{ kNm/m}$, $V = 56.94 \text{ kN/m}$
 V at distance $d = 425 \text{ mm}$ from the face of the stem = 33.74 kN/m
 $M_{sd} = -26.98 \text{ kNm/m}$, $V_{sd} = 33.74 \text{ kN/m}$

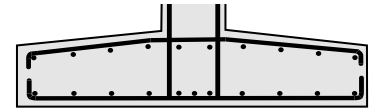
4.12.5. Design of wall footing in bending

(EC2 EN1992-1-1:2004, §6.1)

Concrete-Steel class: C25/30-S500, Concrete cover: $C_{nom} = 75 \text{ mm}$ (§3, §4.4.1.1)
 $M_{sd} = 28.17 \text{ kNm/m}$, $d = 419 \text{ mm}$, $K_d = 7.89$ $x/d = 0.04$ $\epsilon_c / \epsilon_{cs} = 0.7/20.0$ $k_s = 2.33$, **$A_s = 1.56 \text{ cm}^2$**
 $M_{sd} = -26.98 \text{ kNm/m}$, $d = 419 \text{ mm}$, $K_d = 8.07$ $x/d = 0.03$ $\epsilon_c / \epsilon_{cs} = 0.7/20.0$ $k_s = 2.33$, **$A_s = 1.50 \text{ cm}^2$**
 Minimum reinforcement $A_s \geq 0.26 b d \cdot F_{ctm} / f_{yk}$ ($A_s = 5.66 \text{ cm}^2 / \text{m}$) (EC2 §9.3.1)
 Minimum reinforcement $\emptyset 12 / 19.5$ ($5.79 \text{ cm}^2 / \text{m}$)

4.12.6. Reinforcement of wall footing

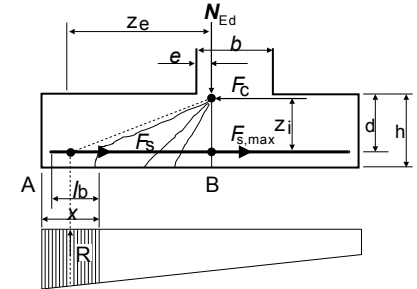
Footing reinforcement at bottom $\text{Ø}12/19.5$ (5.79cm²/m)
Footing reinforcement at top $\text{Ø}12/19.5$ (5.79cm²/m)
Secondary transverse reinforcement $\text{Ø}12/40.0$ (2.82cm²/m)



4.12.7. Anchorage of footing reinforcement

(EC2 EN1992-1-1:2004, §9.8.2.2, §8.4)

$x=h/2=0.250\text{m}$, $R=1000 \times 0.142 \times 0.250=35.50$ kN/m
 $e=0.15b=0.083\text{m}$ $z_e=1.158$ m, $z_i=0.900d=0.377\text{m}$
 $F_s=R \cdot z_e/z_i=35.50 \times 1.158/0.377=108.97$ kN/m
 $\sigma_{sd}=F_s/A_s=1000 \times 108.97/579=188$ MPa



Basic required anchorage length (EC2 Eq.8.3)

$l_{b,rqd}=(\Phi/4) \cdot (\sigma_{sd}/f_{bd})=(12/4) \times (188/2.70)=209\text{mm}$

$f_{bd}=2.25 \times 1.00 \times (f_{ctk} \cdot 0.05/\gamma_c)=2.70$ MPa (EC2 §8.4.2)

Design anchorage length (EC2 §8.4.4, T.8.2)

$l_{bd}=0.70 \times 209=146\text{mm}$, $C_{nom}=75\text{mm} > 3\Phi=36\text{mm}$

Minimum anchorage length $l_{b,min}=\max(0.30l_{brqd}, 10\Phi, 100\text{mm})=120\text{mm}$

Necessary anchorage length of longitudinal reinforcement $L_{bd}=150\text{mm} = 0.150\text{m}$

$l_{bd}=150\text{mm} < (x-C_{nom})=175.00$. Sufficient length is available

4.12.8. Design of wall footing for shear and punching shear

(EC2 EN1992-1-1:2004, §6.2.2)

Concrete-Steel class: C25/30-S500, Concrete cover: $C_{nom}=75$ mm (§3, §4.4.1.1)

Punching shear capacity without shear reinforcement $V_{rd,c}$ (EC2 §6.4.4)

$V_{rd,c}=[C_{rd,c} \cdot k \cdot (100\rho_1 \cdot f_{ck})^{0.333} \cdot (2d/a)] \cdot b \cdot d$ (EC2 Eq.6.50)

$V_{rd,c} > [v_{min} \cdot 2d/a] \cdot b \cdot d$, $d=d_m=419\text{mm}$, $a=419\text{mm}$

$C_{rd,c}=0.18/\gamma_c=0.18/1.50=0.120$, $f_{ck}=25.00\text{MPa}$

$k=1+(200/d)^{1/2} \leq 2$, $k=1.69$

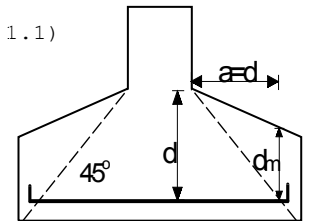
$\rho_1=A_s1/(b \cdot d)=579/(1000 \times 419)=0.0014$

$v_{min}=0.035 \cdot k^{1.50} \cdot f_{ck}^{1/2} = 0.38\text{N/mm}^2$ (EC2 Eq.6.3N)

$V_{rd,c}(min)=0.001 \times (0.38 \times 2 \times 419/419) \times 1000 \times 419=318.44\text{kN/m}$

$V_{rd,c}=0.001 \times [0.120 \times 1.69 \times (0.14 \times 25.00)^{0.333} \times 2 \times 419/419] \times 1000 \times 419=258.03$, $V_{rd,c}=V_{rd,c}(min)=318.44\text{kN/m}$

$V_{sd}=33.74$ kN/m $\leq V_{rd,c}=318.44$ kN/m, shear and punching shear OK



4.13. Material estimate

Concrete per meter of wall length 2.800 m³/m

Reinforcing steel per meter of wall 73.376 kg/m

Total concrete of wall 10.000x 2.800= 27.999 m³

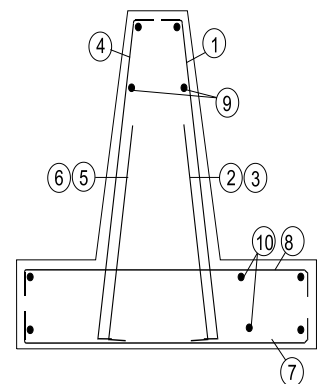
Total reinforcing steel of wall 10.000x 73.376= 733.760 kg

4.14. Reinforcing bar schedule

Num	type	reinforcing bar [mm]	items	Ø	g/m [kg/m]	length [m]	weight [kg]
7	1	100 100	71	10	0.617	4.070	178.29
8	4	100 100	71	10	0.617	4.070	178.29
9	9	10000	16	8	0.395	10.000	63.20
10	7	2290	51	12	0.888	2.290	103.71
11	8	2290	51	12	0.888	2.290	103.71
12	10	10000	12	12	0.888	10.000	106.56

Total weight [kg]

733.76



General information

Wall type : Cantilever wall

Concrete and steel class

Steam :C25/30-S500

Footing :C25/30-S500

Design codes

Eurocode 0 EN1991-1-1, Basis of structural design

Eurocode 1 EN1991-1-1, Actions on structures

Eurocode 2 EN1992-1-1, Design of concrete structures

Eurocode 7 EN1997-1-1, Geotechnical design

Eurocode 8 EN1998-5, Earthquake design

Loads

Vertical : dead Ng=3.00kN, live Nq=2.00kN

Horizontal: dead Hg=2.00kN, live Hq=2.00kN

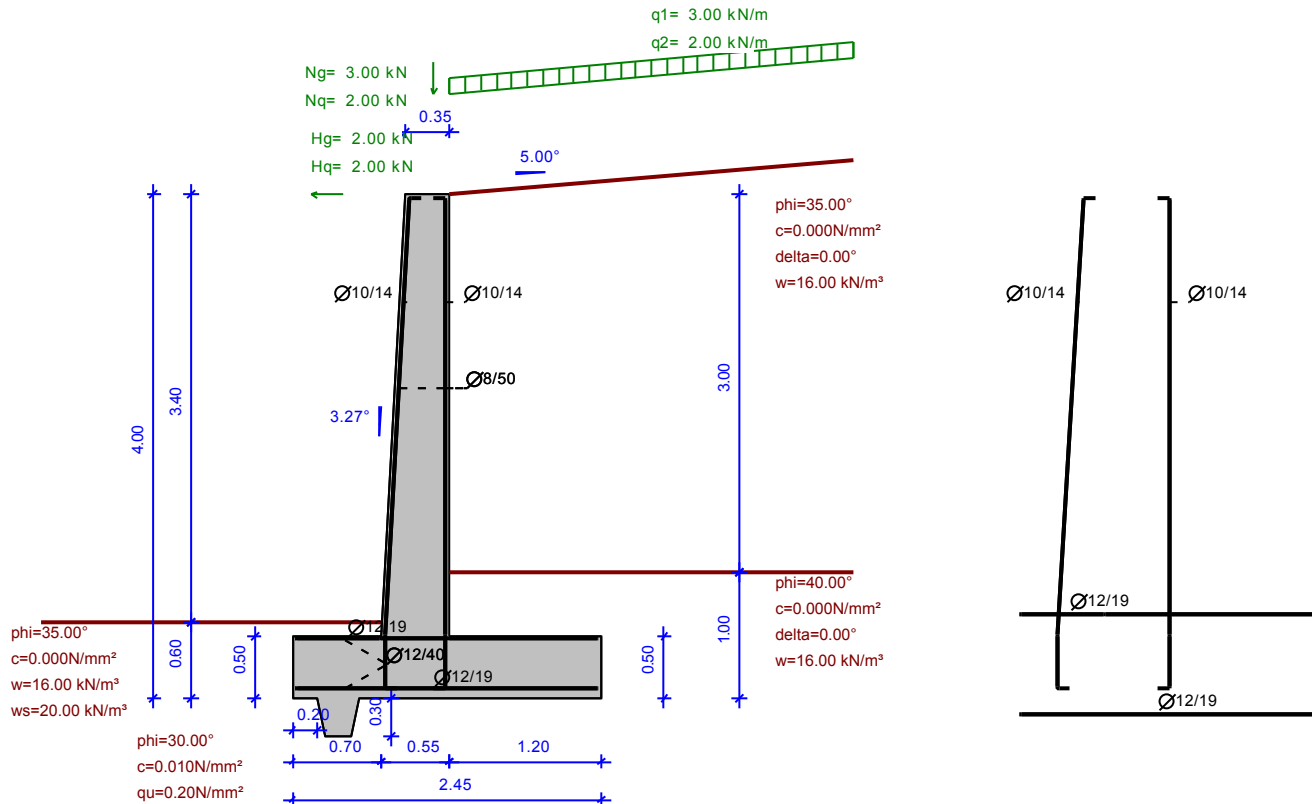
Surcharge : dead g=3.00kN/m², live q=2.00kN/m²

Seismic coefficients

Design ground acceleration ratio a =0.060

Coefficient for horizontal seismic force kh=0.040

Coefficient for vertical seismic force kv=0.020



Soil properties back-1

phi=35.00°
c=0.000N/mm²
delta=0.00°
w=16.00 kN/m³

Soil properties back-2

phi=40.00°
c=0.000N/mm²
delta=0.00°
w=16.00 kN/m³

Soil properties front

phi=35.00°
c=0.000N/mm²
w=16.00 kN/m³
ws=20.00 kN/m³

Foundation soil properties

phi=30.00°
c=0.010N/mm²
qu=0.20N/mm²

Concrete volume V= 28.00 [m³]

Reinforcement weight G=733.76 [kg]

Reinforcing bar schedule

#		reinforcing bar [mm]	items	∅ [mm]	g/m [kg/m]	length [m]	weight [kg]
1	(W1)	100 — 3870 — 100	71	10	0.617	4.070	178.29
2	(W4)	100 — 3870 — 100	71	10	0.617	4.070	178.29
3	(W9)	— 10000 —	16	8	0.395	10.000	63.20
4	(W7)	— 2290 —	51	12	0.888	2.290	103.71
5	(W8)	— 2290 —	51	12	0.888	2.290	103.71
6	(W10)	— 10000 —	12	12	0.888	10.000	106.56
Total weight [kg]							733.76

Project: Example of retaining walls

C. WALL-002

Scale : **1:60**

Date: 12/03/2007

Designer:

Draw.No.:

Filename: Example of retaining Sign:

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