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Example of plates

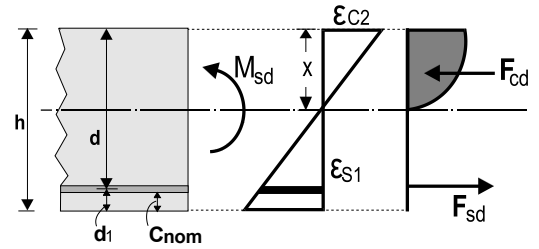
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Example of plates

1. SLAB-001

Cross section of solid slab in bending
 (EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002)

h=0.180 m, Msd=20.00 kNm
 Concrete-Steel class: C25/30-S500 (EC2 §3)
 Concrete cover : Cnom=15 mm (EC2 §4.4.1)
 $\gamma_c=1.50, \gamma_s=1.15$ (EC2 Table 2.1N)



1.1. Dimensions and loads

Slab thickness $h=0.180$ m, Bending moment $Msd=20.00$ kNm
 Effective depth of cross section $d=h-d_1$, $d_1=Cnom+\varnothing/2=15+12/2=21$ mm, $d=180-21=159$ mm

1.2. Ultimate limit state, design for bending

(EC2 EN1992-1-1:2004, §6.1, §9.3.1)

Dimensioning for bending: Allgower, G.-Avak, R. Bemessungstabeln nach Eurocode 2 für Rechteck und Plattenbalkenquerschnitte, In: Beton - und Stahlbetonbau 87 (1992)

$Msd= 20.00$ kNm/m, $d=159$ mm, $Kd=3.56$ $x/d=0.09$ $\epsilon_c/\epsilon_{s1}=1.9/20.0$ $k_s=2.38$, **$A_s= 2.99$ cm²/m**
 Minimum slab reinforcement, $A_s \geq 0.26bd \cdot F_{ctm}/f_{yk}$ ($A_s= 2.15$ cm²/m) (EC2 §9.3.1)
 minimum principal reinforcement $\varnothing 10/36.5$ (2.15 cm²/m), secondary $\varnothing 8/45.0$ (1.12 cm²/m)

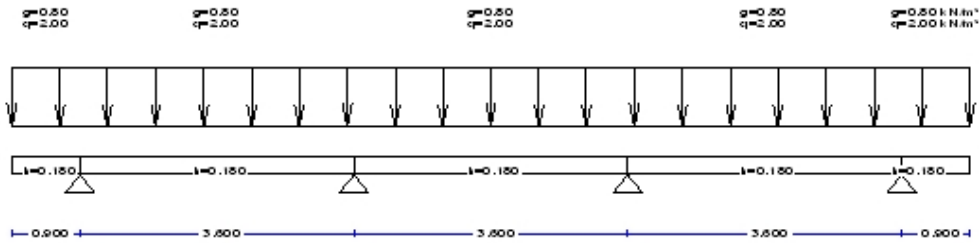
Slab principal reinforcement $\varnothing 12/37.5$ (3.01 cm²/m), secondary $\varnothing 8/45.0$ (1.12 cm²/m)

2. SLAB-002

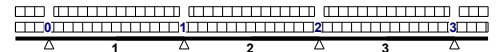
One-way continuous slab

(EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002)

C25/30 - S500



Concrete-Steel class: C25/30-S500 (EC2 §3)
 Concrete cover : Cnom=15 mm (EC2 §4.4.1)
 Concrete weight : 25.0 kN/m³
 $\gamma_c=1.50$, $\gamma_s=1.15$ (EC2 Table 2.1N)



2.1. Dimensions and loads

Continuous slab, number of spans=3, transverse length $L_y=9.00$ m

Partial safety factors for actions : $\gamma_G=1.35$, $\gamma_Q=1.50$

(EC0 Annex A1)

Combination of variable actions : $\psi_1=0.60$, $\psi_2=0.30$

Effective depth of cross section $d=h-d_1$, $d_1=Cnomc+\varnothing/2=15+10/2=20$ mm

Spans (L), thickness (h), loads on spans (g =self weight +dead, q =live)

Cant-1, $L=0.900$ m, $h=0.180$ m, $g=(4.50+0.80)\times 1.000=5.30$ kN/m², $q=2.00\times 1.000=2.00$ kN/m²

Span-1, $L=3.600$ m, $h=0.180$ m, $g=(4.50+0.80)\times 1.000=5.30$ kN/m², $q=2.00\times 1.000=2.00$ kN/m²

Span-2, $L=3.600$ m, $h=0.180$ m, $g=(4.50+0.80)\times 1.000=5.30$ kN/m², $q=2.00\times 1.000=2.00$ kN/m²

Span-3, $L=3.600$ m, $h=0.180$ m, $g=(4.50+0.80)\times 1.000=5.30$ kN/m², $q=2.00\times 1.000=2.00$ kN/m²

Cant-2, $L=0.900$ m, $h=0.180$ m, $g=(4.50+0.80)\times 1.000=5.30$ kN/m², $q=2.00\times 1.000=2.00$ kN/m²

2.2. Shearing forces and bending moments

Maximum bending moments at spans for load combinations $1.35g+1.50q$

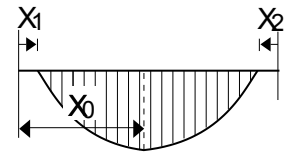
Cant-1, $M_{sd}=-4.11$ kNm/m, $x_0=0.900$ m, $x_1=0.000$ m, $x_2=0.000$ m

Span-1, $M_{sd}=10.06$ kNm/m, $x_0=1.550$ m, $x_1=0.143$ m, $x_2=0.642$ m

Span-2, $M_{sd}=5.58$ kNm/m, $x_0=1.800$ m, $x_1=0.752$ m, $x_2=0.752$ m

Span-3, $M_{sd}=10.06$ kNm/m, $x_0=2.050$ m, $x_1=0.642$ m, $x_2=0.143$ m

Cant-2, $M_{sd}=-4.11$ kNm/m, $x_0=0.000$ m, $x_1=0.000$ m, $x_2=0.000$ m



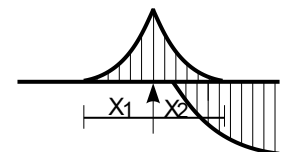
Maximum bending moments at supports for load combinations $1.35g+1.50q$

Support-0, $M_{sd}=-4.11$ kNm/m, $x_1=0.900$ m, $x_2=0.291$ m

Support-1, $M_{sd}=-14.97$ kNm/m, $x_1=0.869$ m, $x_2=1.102$ m

Support-2, $M_{sd}=-14.97$ kNm/m, $x_1=1.102$ m, $x_2=0.869$ m

Support-3, $M_{sd}=-4.11$ kNm/m, $x_1=0.291$ m, $x_2=0.900$ m



Maximum shear forces for load combinations 1.35g+1.50q

Cant-1, Vsd,left= 0.00 kN/m, Vsd,right= -9.14 kN/m
 Span-1, Vsd,left= 14.93 kN/m, Vsd,right= -21.63 kN/m
 Span-2, Vsd,left= 17.38 kN/m, Vsd,right= -19.18 kN/m
 Span-3, Vsd,left= 20.93 kN/m, Vsd,right= -15.62 kN/m
 Cant-2, Vsd,left= 9.14 kN/m, Vsd,right= 0.00 kN/m

Maximum reactions due to dead and live loads (Rg and Rq)

Support-0, Rg(x1.35)= 17.23 kN/m, Rq(x1.50)= 7.54 kN/m
 Support-1, Rg(x1.35)= 27.85 kN/m, Rq(x1.50)= 12.96 kN/m
 Support-2, Rg(x1.35)= 27.85 kN/m, Rq(x1.50)= 12.96 kN/m
 Support-3, Rg(x1.35)= 17.23 kN/m, Rq(x1.50)= 7.54 kN/m

2.3. Design actions, shearing forces and bending moments

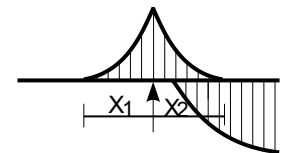
Design action values after moment redistribution by 0% (EC2 §5.5)
 Reduction of support moments to moments at support faces (bsup=0.20 m) (EC2 §5.3.2.2.3)
 Check for minimum values, (0.65ql²/8 or 0.65ql²/12) (EC2 §5.3.2.2.3N)

Maximum span bending moments and shear forces for load combinations 1.35g+1.50q

Cant-1, Msd= -3.20 kNm/m, Vsd,left= 0.00 kN/m, Vsd,right= -9.14 kN/m
 Span-1, Msd= 10.06 kNm/m, Vsd,left= 15.74 kN/m, Vsd,right= -20.81 kN/m
 Span-2, Msd= 5.58 kNm/m, Vsd,left= 18.28 kN/m, Vsd,right= -18.28 kN/m
 Span-3, Msd= 10.06 kNm/m, Vsd,left= 20.81 kN/m, Vsd,right= -15.74 kN/m
 Cant-2, Msd= -3.20 kNm/m, Vsd,left= 9.14 kN/m, Vsd,right= 0.00 kN/m

Maximum bending moments at supports for load combinations 1.35g+1.50q

Support-0, Msd= -3.20 kNm/m, x1=0.900 m, x2=0.291 m
 Support-1, Msd= -13.14 kNm/m, x1=0.869 m, x2=1.102 m
 Support-2, Msd= -13.14 kNm/m, x1=1.102 m, x2=0.869 m
 Support-3, Msd= -3.20 kNm/m, x1=0.291 m, x2=0.900 m



2.4. Ultimate limit state, design for bending

(EC2 EN1992-1-1:2004, §6.1, §9.3.1)

Reinforcement of spans

Msd1= 10.06kNm/m, d=160mm, Kd=5.05 x/d=0.06 εc/εs=1.2/20.0 ks=2.35, **As= 1.48cm²/m**
 Msd2= 5.58kNm/m, d=160mm, Kd=6.77 x/d=0.04 εc/εs=0.9/20.0 ks=2.33, **As= 0.81cm²/m**
 Msd3= 10.06kNm/m, d=160mm, Kd=5.05 x/d=0.06 εc/εs=1.2/20.0 ks=2.35, **As= 1.48cm²/m**

Reinforcement over supports

Msd0= -3.20kNm/m, d=160mm, Kd=8.95 x/d=0.03 εc/εs=0.6/20.0 ks=2.32, **As= 0.46cm²/m**
 Msd1=-13.14kNm/m, d=160mm, Kd=4.41 x/d=0.07 εc/εs=1.4/20.0 ks=2.36, **As= 1.94cm²/m**
 Msd2=-13.14kNm/m, d=160mm, Kd=4.41 x/d=0.07 εc/εs=1.4/20.0 ks=2.36, **As= 1.94cm²/m**
 Msd3= -3.20kNm/m, d=160mm, Kd=8.95 x/d=0.03 εc/εs=0.6/20.0 ks=2.32, **As= 0.46cm²/m**

2.5. Minimum reinforcement at spans

(EC2 EN1992-1-1:2004, §9.3.1)

Span-1, As>=0.26bd·Fctm/fyk (As= 2.16cm²/m) Ø10/36.0 (2.18cm²/m), second. Ø8/45.0 (1.12cm²/m)
 Span-2, As>=0.26bd·Fctm/fyk (As= 2.16cm²/m) Ø10/36.0 (2.18cm²/m), second. Ø8/45.0 (1.12cm²/m)
 Span-3, As>=0.26bd·Fctm/fyk (As= 2.16cm²/m) Ø10/36.0 (2.18cm²/m), second. Ø8/45.0 (1.12cm²/m)

2.6. Serviceability limit state, deflection control

(EC2 EN1992-1-1:2004, §7.4.2)

Cant-1, K=0.40, ρ=0.029%, L/d= 900/ 160= 5.62< 8.00 (EC2 T.7.4N)
 Span-1, K=1.50, ρ=0.092%, L/d= 3600/ 160=22.50<30.00
 Span-2, K=1.50, ρ=0.051%, L/d= 3600/ 160=22.50<30.00
 Span-3, K=1.50, ρ=0.092%, L/d= 3600/ 160=22.50<30.00
 Cant-2, K=0.40, ρ=0.029%, L/d= 900/ 160= 5.62< 8.00

2.7. Reinforcement

Span reinforcement

Cant-1	Ø10/36.0 (2.18cm ² /m) principal at top,	Ø8/45.0 (1.12cm ² /m) secondary
Span-1	Ø10/36.0 (2.18cm ² /m) principal at bottom,	Ø8/45.0 (1.12cm ² /m) secondary
Span-2	Ø10/36.0 (2.18cm ² /m) principal at bottom,	Ø8/45.0 (1.12cm ² /m) secondary
Span-3	Ø10/36.0 (2.18cm ² /m) principal at bottom,	Ø8/45.0 (1.12cm ² /m) secondary
Cant-2	Ø10/36.0 (2.18cm ² /m) principal at top,	Ø8/45.0 (1.12cm ² /m) secondary

Reinforcement over supports

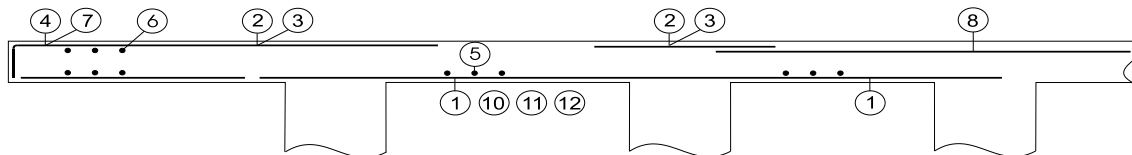
Support-0	Ø10/36.0 (2.18cm ² /m) reinforcement at top
Support-1	Ø10/36.0 (2.18cm ² /m) reinforcement at top
Support-2	Ø10/36.0 (2.18cm ² /m) reinforcement at top
Support-3	Ø10/36.0 (2.18cm ² /m) reinforcement at top

2.8. Reinforcing bar schedule

Num		type	reinforcing bar [mm]	items	Ø	g/m [kg/m]	length [m]	weight [kg]
1	(Span-1)	①	4020	25	10	0.617	4.020	62.01
2	(Span-2)	①	4020	25	10	0.617	4.020	62.01
3	(Span-3)	①	4020	25	10	0.617	4.020	62.01
4	(Cant-1)	④	2090	25	10	0.617	2.240	34.55
5	(Supp-1)	②	2550	25	10	0.617	2.550	39.33
6	(Supp-2)	②	2550	25	10	0.617	2.550	39.33
7	(Cant-2)	④	2090	25	10	0.617	2.250	34.71
8	(Cant-1)	⑤	9000	2	8	0.395	9.000	7.11
9	(Cant-1)	⑥	9000	2	8	0.395	9.000	7.11
10	(Span-1)	⑤	9000	8	8	0.395	9.000	28.44
11	(Span-2)	⑤	9000	8	8	0.395	9.000	28.44
12	(Span-3)	⑤	9000	8	8	0.395	9.000	28.44
13	(Cant-2)	⑤	9000	2	8	0.395	9.000	7.11
14	(Cant-2)	⑥	9000	2	8	0.395	9.000	7.11

Total weight [kg]

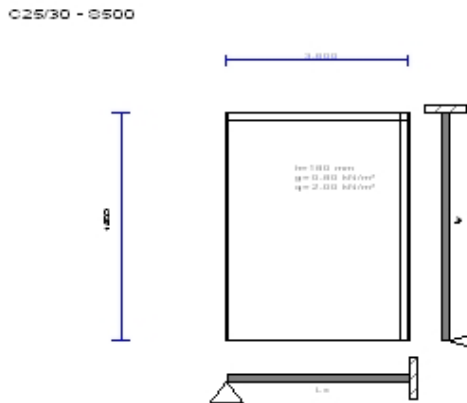
447.71



3. SLAB-003

Two-way slab

(EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002)



Concrete-Steel class: C25/30-S500 (EC2 §3)
 Concrete cover : Cnom=15 mm (EC2 §4.4.1)
 Concrete weight : 25.0 kN/m³
 $\gamma_c=1.50$, $\gamma_s=1.15$ (EC2 Table 2.1N)



3.1. Dimensions and loads

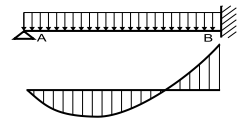
Slab thickness $h=0.180$ m, Spans $L_x=3.600$ m, $L_y=4.500$ m
 Slab loads: dead $g=(4.50+0.80)=5.30$ kN/m², live $q=2.00$ kN/m²
 Partial safety factors for actions : $\gamma_G=1.35$, $\gamma_Q=1.50$ (EC0 Annex A1)
 Combination of variable actions : $\psi_1=0.60$, $\psi_2=0.30$
 Effective depth of cross section $d=h-d_1$, $d_1=Cnomc+\varnothing/2=15+10/2=20$ mm, $d=180-20=160$ mm

Method of analysis: Czerny F., "Tafeln für vierseitig und dreiseitig gelagerte Rechteckplatten", Beton Kalender 1983, Berlin, Ernst Sohn, 1983
 $L_y/L_x=4.500/3.600=1.25$, Table 2.2.4

3.2. Ultimate limit state, design for bending (EC2 EN1992-1-1:2004, §6.1, §9.3.1)

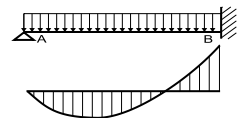
3.2.1. Direction of slab analysis x-x, $L_x=3.60$ m

Moment at support $M_{sd\sup A}=0$ kNm/m
 Moment at support $M_{sd\sup B}=(1.35 \times 5.30 + 1.50 \times 2.00) \times 3.600^2 / 11.10 = -11.86$ kNm/m
 Moment at span $M_{sd\text{span}}=(1.35 \times 5.30 + 1.50 \times 2.00) \times 3.600^2 / 28.00 = 4.70$ kNm/m
 Reactions dead, $V_{gA}= 5.30 \times 3.600 / 2.53 = 7.54$ $V_{gB}= 5.30 \times 3.600 / 1.72 = 11.09$ kN/m
 Reactions live, $V_{qA}= 2.00 \times 3.600 / 2.53 = 2.85$ $V_{qB}= 2.00 \times 3.600 / 1.72 = 4.19$ kN/m



3.2.2. Direction of slab analysis y-y, $L_y=4.50$ m

Moment at support $M_{sd\sup A}=0$ kNm/m
 Moment at support $M_{sd\sup B}=(1.35 \times 5.30 + 1.50 \times 2.00) \times 3.600^2 / 12.90 = -10.20$ kNm/m
 Moment at span $M_{sd\text{span}}=(1.35 \times 5.30 + 1.50 \times 2.00) \times 3.600^2 / 45.60 = 2.89$ kNm/m
 Reactions dead, $V_{gA}= 5.30 \times 3.600 / 2.56 = 7.45$ $V_{gB}= 5.30 \times 3.600 / 1.86 = 10.26$ kN/m
 Reactions live, $V_{qA}= 2.00 \times 3.600 / 2.56 = 2.81$ $V_{qB}= 2.00 \times 3.600 / 1.86 = 3.87$ kN/m



3.3. Ultimate limit state, design for bending

(EC2 EN1992-1-1:2004, §6.1, §9.3.1)

Msd= 4.70kNm/m, d=160mm, Kd=7.38 x/d=0.04 $\epsilon_c/\epsilon_s=0.8/20.0$ ks=2.33, **As= 0.68cm²/m**
 Msd= 2.89kNm/m, d=150mm, Kd=8.83 x/d=0.03 $\epsilon_c/\epsilon_s=0.7/20.0$ ks=2.32, **As= 0.45cm²/m**
 Msd=-11.86kNm/m, d=160mm, Kd=4.65 x/d=0.06 $\epsilon_c/\epsilon_s=1.4/20.0$ ks=2.35, **As= 1.74cm²/m**
 Msd=-10.20kNm/m, d=160mm, Kd=5.01 x/d=0.06 $\epsilon_c/\epsilon_s=1.2/20.0$ ks=2.35, **As= 1.50cm²/m**

Minimum slab reinforcement, $A_s \geq 0.26bd \cdot F_{ctm}/f_{yk}$ ($A_s = 2.16\text{cm}^2/\text{m}$) (EC2 §9.3.1)

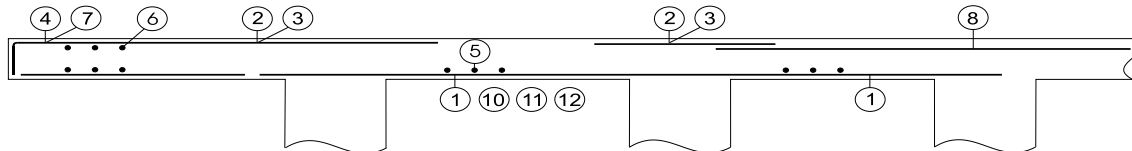
minimum principal reinforcement $\emptyset 10/36.0$ (2.18cm²/m), secondary $\emptyset 8/45.0$ (1.12cm²/m) span/eff. depth, K=1.30, $\rho=0.043\%$, L/d= 3600/ 160=22.50<26.00 (EC2 T.7.4N)

Span reinforcement: x-x $\emptyset 10/36.0$ (2.18cm²/m), (bottom layer)
 y-y $\emptyset 10/36.0$ (2.18cm²/m)
Reinforcement over supports: Left $\emptyset 8/45.0$ (1.12cm²/m)
 Right $\emptyset 10/36.0$ (2.18cm²/m)
 Bottom $\emptyset 8/45.0$ (1.12cm²/m)
 Top $\emptyset 10/36.0$ (2.18cm²/m)

3.4. Reinforcing bar schedule

Num	type	reinforcing bar [mm]	items	\emptyset	g/m [kg/m]	length [m]	weight [kg]
15	④	4020	12	10	0.617	4.020	29.76
16	①	4920	10	10	0.617	4.920	30.36
17	②	2260	10	8	0.395	2.260	8.93
18	②	2380	12	10	0.617	2.380	17.62
19	②	2710	8	8	0.395	2.710	8.56
20	②	2830	10	10	0.617	2.830	17.46

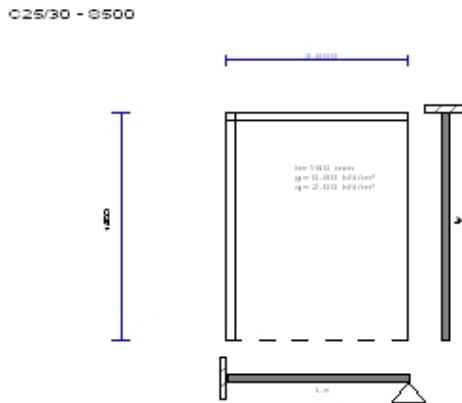
Total weight [kg] 112.69



4. SLAB-004

Two-way slab with three supported edges

(EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002)



Concrete-Steel class: C25/30-S500 (EC2 §3)
 Concrete cover : Cnom=15 mm (EC2 §4.4.1)
 Concrete weight : 25.0 kN/m³
 $\gamma_c=1.50$, $\gamma_s=1.15$ (EC2 Table 2.1N)



4.1. Dimensions and loads

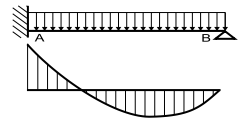
Slab thickness $h=0.180$ m, Spans $L_x=3.600$ m, $L_y=4.500$ m
 Slab loads: dead $g=(4.50+0.80)=5.30$ kN/m², live $q=2.00$ kN/m²
 Partial safety factors for actions : $\gamma_G=1.35$, $\gamma_Q=1.50$ (EC0 Annex A1)
 Combination of variable actions : $\psi_1=0.60$, $\psi_2=0.30$
 Effective depth of cross section $d=h-d_1$, $d_1=Cnomc+\varnothing/2=15+10/2=20$ mm, $d=180-20=160$ mm

Method of analysis: Czerny F., "Tafeln für vierseitig und dreiseitig gelagerte Rechteckplatten", Beton Kalender 1983, Berlin, Ernst Sohn, 1983
 $L_y/L_x=4.500/3.600=1.25$, Table 3.2.5

4.2. Ultimate limit state, design for bending (EC2 EN1992-1-1:2004, §6.1, §9.3.1)

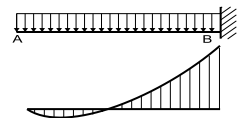
4.2.1. Direction of slab analysis x-x, $L_x=3.60$ m

Moment at support $M_{sdsupA}=(1.35 \times 5.30 + 1.50 \times 2.00) \times 4.500^2 / 12.42 = -16.56$ kNm/m
 Moment at support $M_{sdsupB}=0$ kNm/m
 Moment at span $M_{sdspan}=(1.35 \times 5.30 + 1.50 \times 2.00) \times 4.500^2 / 22.83 = 9.01$ kNm/m
 Reactions dead, $V_{gA}=5.30 \times 4.500 / 2.16 = 11.04$ $V_{gB}=5.30 \times 4.500 / 3.34 = 7.14$ kN/m
 Reactions live, $V_{qA}=2.00 \times 4.500 / 2.16 = 4.17$ $V_{qB}=2.00 \times 4.500 / 3.34 = 2.69$ kN/m



4.2.2. Direction of slab analysis y-y, $L_y=4.50$ m

Moment at support $M_{sdsupA}=0$ kNm/m
 Moment at support $M_{sdsupB}=(1.35 \times 5.30 + 1.50 \times 2.00) \times 4.500^2 / 19.30 = -10.66$ kNm/m
 Moment at span $M_{sdspan}=(1.35 \times 5.30 + 1.50 \times 2.00) \times 4.500^2 / 130.66 = 1.57$ kNm/m
 Reactions dead, $V_{gA}=0.00$ $V_{gB}=5.30 \times 4.500 / 2.27 = 10.51$ kN/m
 Reactions live, $V_{qA}=0.00$ $V_{qB}=2.00 \times 4.500 / 2.27 = 3.96$ kN/m



4.3. Ultimate limit state, design for bending

(EC2 EN1992-1-1:2004, §6.1, §9.3.1)

Msd= 9.01kNm/m, d=160mm, Kd=5.33 x/d=0.05 $\epsilon_c/\epsilon_s=1.2/20.0$ ks=2.34, **As= 1.32cm²/m**
 Msd= 1.57kNm/m, d=150mm, Kd=11.96 x/d=0.02 $\epsilon_c/\epsilon_s=0.5/20.0$ ks=2.32, **As= 0.24cm²/m**
 Msd=-16.56kNm/m, d=160mm, Kd=3.93 x/d=0.08 $\epsilon_c/\epsilon_s=1.7/20.0$ ks=2.37, **As= 2.45cm²/m**
 Msd=-10.66kNm/m, d=160mm, Kd=4.90 x/d=0.06 $\epsilon_c/\epsilon_s=1.3/20.0$ ks=2.35, **As= 1.56cm²/m**

Minimum slab reinforcement, $A_s \geq 0.26bd \cdot F_{ctm}/f_{yk}$ ($A_s = 2.16\text{cm}^2/\text{m}$) (EC2 §9.3.1)

minimum principal reinforcement $\varnothing 10/36.0$ (2.18cm²/m), secondary $\varnothing 8/45.0$ (1.12cm²/m) span/eff. depth, K=1.30, $\rho=0.082\%$, L/d= 3600/ 160=22.50<26.00 (EC2 T.7.4N)

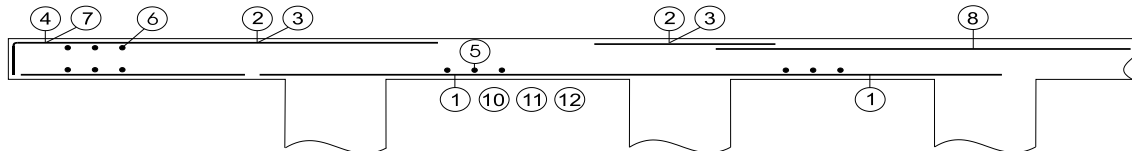
Span reinforcement: x-x $\varnothing 10/36.0$ (2.18cm²/m), (bottom layer)
 y-y $\varnothing 10/36.0$ (2.18cm²/m)
Reinforcement over supports: Left $\varnothing 10/32.0$ (2.45cm²/m)
 Right $\varnothing 8/45.0$ (1.12cm²/m)
 Bottom $\varnothing 8/45.0$ (1.12cm²/m)
 Top $\varnothing 10/36.0$ (2.18cm²/m)

4.4. Reinforcing bar schedule

Num	type	reinforcing bar [mm]	items	\varnothing	g/m [kg/m]	length [m]	weight [kg]
21	④	4020	12	10	0.617	4.020	29.76
22	①	4920	10	10	0.617	4.920	30.36
23	②	2380	14	10	0.617	2.380	20.56
24	②	2260	10	8	0.395	2.260	8.93
25	②	2710	8	8	0.395	2.710	8.56
26	⑧	1410 1410 150	10	10	0.617	2.970	18.32

Total weight [kg]

116.49

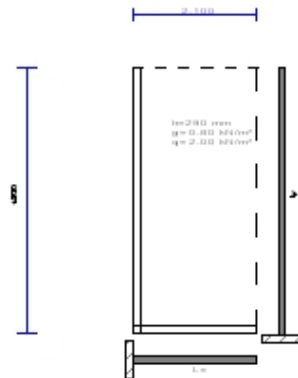


5. SLAB-005

Two-way slab with two supported edges

(EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002)

C25/30 - S500



Concrete-Steel class: C25/30-S500 (EC2 §3)
 Concrete cover : Cnom=15 mm (EC2 §4.4.1)
 Concrete weight : 25.0 kN/m³
 $\gamma_c=1.50, \gamma_s=1.15$ (EC2 Table 2.1N)



5.1. Dimensions and loads

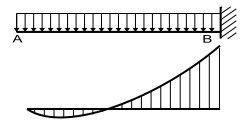
Slab thickness $h=0.290$ m, Spans $L_x=2.100$ m, $L_y=4.500$ m
 Slab loads: dead $g=(7.25+0.80)=8.05$ kN/m², live $q=2.00$ kN/m²
 Partial safety factors for actions : $\gamma_G=1.35, \gamma_Q=1.50$ (EC0 Annex A1)
 Combination of variable actions : $\psi_1=0.60, \psi_2=0.30$
 Effective depth of cross section $d=h-d_1, d_1=C_{nom}+\varnothing/2=15+12/2=21$ mm, $d=290-21=269$ mm

Method of analysis: Bares R., "Tables for the Analysis of Plates, Slabs and Diaphragms Based on the Elastic Theory", Bauverlag GmbH., Wiesbaden und Berlin 1971

5.2. Ultimate limit state, design for bending (EC2 EN1992-1-1:2004, §6.1, §9.3.1)

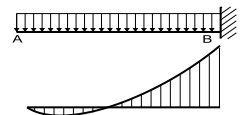
5.2.1. Direction of slab analysis x-x, $L_x=2.10$ m

Moment at span $M_{sdsp}=0.0007 \times (1.35 \times 8.05 + 1.50 \times 2.00) \times 2.100^2 = 0.04$ kNm/m
 Moment at support $M_{sdsup}=-0.4323 \times (1.35 \times 8.05 + 1.50 \times 2.00) \times 2.100^2 = -26.44$ kNm/m
 Reactions $V_{sg}=0.857 \times 8.05 \times 2.100 = 14.48$, $V_{sq}=0.857 \times 2.00 \times 2.100 = 3.60$ kN/m



5.2.2. Direction of slab analysis y-y, $L_y=4.50$ m

Moment at span $M_{sdsp}=0.0101 \times (1.35 \times 8.05 + 1.50 \times 2.00) \times 4.500^2 = 2.82$ kNm/m
 Moment at support $M_{sdsup}=-0.0724 \times (1.35 \times 8.05 + 1.50 \times 2.00) \times 4.500^2 = -20.34$ kNm/m
 Reactions $V_{sg}=0.143 \times 8.05 \times 4.500 = 5.20$, $V_{sq}=0.143 \times 2.00 \times 4.500 = 1.29$ kN/m



5.3. Ultimate limit state, design for bending

(EC2 EN1992-1-1:2004, §6.1, §9.3.1)

Msd= 0.04kNm/m, d=257mm, Kd=124.21 x/d=0.00 $\epsilon_c/\epsilon_s=0.0/20.0$ ks=2.30, **As= 0.00cm²/m**
 Msd= 2.82kNm/m, d=269mm, Kd=16.01 x/d=0.02 $\epsilon_c/\epsilon_s=0.3/20.0$ ks=2.31, **As= 0.24cm²/m**
 Msd=-26.44kNm/m, d=269mm, Kd=5.23 x/d=0.06 $\epsilon_c/\epsilon_s=1.2/20.0$ ks=2.34, **As= 2.30cm²/m**
 Msd=-20.34kNm/m, d=269mm, Kd=5.96 x/d=0.05 $\epsilon_c/\epsilon_s=1.0/20.0$ ks=2.34, **As= 1.77cm²/m**

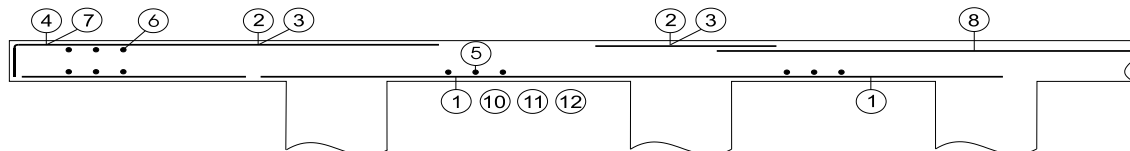
Minimum slab reinforcement, $A_s \geq 0.26bd \cdot F_{ctm}/f_{yk}$ ($A_s = 3.64\text{cm}^2/\text{m}$) (EC2 §9.3.1)
 minimum principal reinforcement $\varnothing 12/31.0$ ($3.65\text{cm}^2/\text{m}$), secondary $\varnothing 8/45.0$ ($1.12\text{cm}^2/\text{m}$)
 span/eff. depth, $K=0.40$, $\rho=0.000\%$, $L/d= 2100/ 269= 7.81 < 8.00$ (EC2 T.7.4N)

Span reinforcement: x-x $\varnothing 12/31.0$ ($3.65\text{cm}^2/\text{m}$)
 y-y $\varnothing 12/31.0$ ($3.65\text{cm}^2/\text{m}$), (bottom layer)
Reinforcement over supports: Left $\varnothing 12/31.0$ ($3.65\text{cm}^2/\text{m}$)
 Right $\varnothing 8/45.0$ ($1.12\text{cm}^2/\text{m}$)
 Bottom $\varnothing 12/31.0$ ($3.65\text{cm}^2/\text{m}$)
 Top $\varnothing 8/45.0$ ($1.12\text{cm}^2/\text{m}$)

5.4. Reinforcing bar schedule

Num	type	reinforcing bar [mm]	items	\varnothing	g/m [kg/m]	length [m]	weight [kg]
27	④	2600	15	12	0.888	2.600	34.63
28	①	5000	7	12	0.888	5.000	31.08
29	⑨	880 260 880	15	12	0.888	2.020	26.91
30	②	1510	10	8	0.395	2.650	10.47
31	⑨	1480 260 1480	7	12	0.888	3.220	20.02
32	②	2710	5	8	0.395	4.450	8.79

Total weight [kg] 131.90

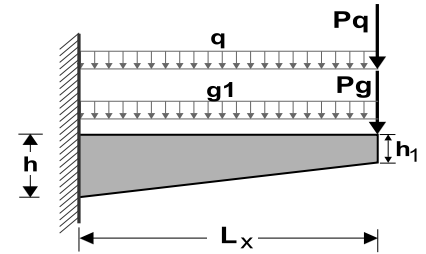


6. SLAB-006

One way cantilever slab

(EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002)

Concrete-Steel class: C25/30-S500 (EC2 §3)
 Concrete cover : Cnom=15 mm (EC2 §4.4.1)
 Concrete weight : 25.0 kN/m³
 $\gamma_c=1.50, \gamma_s=1.15$ (EC2 Table 2.1N)



6.1. Dimensions and loads

Cantilever slab, free span $L_x=1.200$ m, transverse length $L_y=4.800$ m
 Slab thickness, at support $h=0.180$ m, at free end $h_1=0.180$ m
 Slab loads: dead $g=(4.50+0.80)=5.30$ kN/m², live $q=2.00$ kN/m²
 concentrated loads at free end, $P_g=0.00$ kN/m, $P_q=0.00$ kN/m
 Partial safety factors for actions : $\gamma_G=1.35, \gamma_Q=1.50$ (EC0 Annex A1)
 Combination of variable actions : $\psi_1=0.60, \psi_2=0.30$
 Effective depth of cross section $d=h-d_1, d_1=Cnomc+\varnothing/2=15+10/2=20$ mm, $d=180-20=160$ mm

6.2. Ultimate limit state, design for bending

(EC2 EN1992-1-1:2004, §6.1, §9.3.1)

Support moment $M=-0.5 \times (1.35 \times 5.30 + 1.50 \times 2.00) \times 1.20^2 = -7.31$ kNm/m
 Shear force $V=(1.35 \times 5.30 + 1.50 \times 2.00) \times 1.20 = 12.19$ kN/m
 Reaction $V_g A = 1.35 \times 5.30 \times 1.20 = 8.59$ kN/m, $V_q A = 1.50 \times 2.00 \times 1.20 = 3.60$ kN/m

Reinforcement of slab

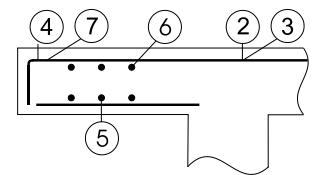
(EC2 EN1992-1-1:2004, §6.1, §9.3.1)

$M_{sd} = -7.31$ kNm/m, $d=160$ mm, $K_d=5.92$ $x/d=0.05$ $\epsilon_c/\epsilon_{s1}=1.0/20.0$ $k_s=2.34$, **$A_s = 1.07$ cm²/m**
 Minimum slab reinforcement, $A_s \geq 0.26bd \cdot F_{ctm}/f_{yk}$ ($A_s = 2.16$ cm²/m) (EC2 §9.3.1)
 minimum principal reinforcement $\varnothing 10/36.0$ (2.18 cm²/m), secondary $\varnothing 8/45.0$ (1.12 cm²/m)
 span/eff. depth, $K=0.40, \rho=0.067\%$, $L/d=1200/160=7.50 < 8.00$ (EC2 T.7.4N)

Main reinforcement $\varnothing 10/36.0$ (2.18 cm²/m) (top), secondary $\varnothing 8/45.0$ (1.12 cm²/m) (top- bottom)

6.3. Reinforcing bar schedule

Num	type	reinforcing bar [mm]	items	\varnothing	g/m [kg/m]	length [m]	weight [kg]
33	④	2660	7	10	0.617	2.810	12.14
34	②	1780	7	10	0.617	1.780	7.69
35	⑤	4770	3	8	0.395	4.770	5.65
36	⑥	4770	3	8	0.395	4.770	5.65
Total weight [kg]							31.13

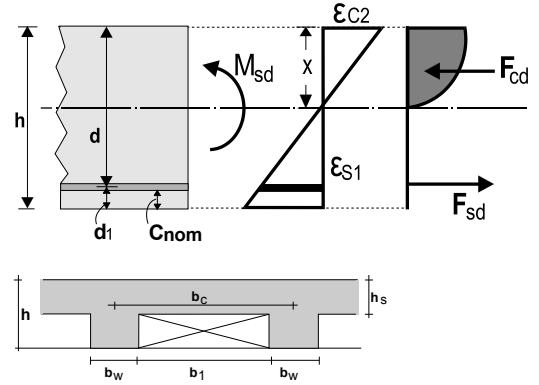


7. SLAB-007

Cross section of ribbed slab in bending
 (EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002)

**$h=0.180$ m, $h_s=0.070$ m, $M_{sd}=20.00$ kNm
 $b_w=0.150$ m, $b_1=0.500$ m**

Concrete-Steel class: C25/30-S500 (EC2 §3)
 Concrete cover : $C_{nom}=15$ mm (EC2 §4.4.1)
 $\gamma_c=1.50$, $\gamma_s=1.15$ (EC2 Table 2.1N)



7.1. Dimensions and loads

Slab thickness $h=0.180$ m, $h_s=0.070$ m, Bending moment $M_{sd}=20.00$ kNm
 Rib width $b_w=0.150$ m, clear distance between ribs $b_1=0.500$ m, rib spacing $b_c=0.650$ m
 Effective depth of cross section $d=h-d_1$, $d_1=C_{nom}c+\varnothing/2=15+10/2=20$ mm, $d=180-20=160$ mm

7.2. Ultimate limit state, design for bending

(EC2 EN1992-1-1:2004, §6.1, §9.3.1)

Dimensioning for bending: Allgower, G.-Avak, R. Bemessungstabellen nach Eurocode 2 für Rechteck und Plattenbalkenquerschnitte, In: Beton - und Stahlbetonbau 87 (1992)

$M_{sd}=20.00$ kNm/m, $d=160$ mm, $K_d=3.58$ $x/d=0.09$ $\epsilon_c/\epsilon_{cs}=1.9/20.0$ $k_s=2.38$, **$A_s=2.97$ cm²/m**

$x=0.09 \times 160=14$ mm ≤ 70 mm $=h_s$, neutral axis within the depth of top flange

Minimum slab reinforcement, $A_s \geq 0.26 b d \cdot F_{ctm} / f_{yk}$ ($A_s=0.50$ cm²/m)

(EC2 §9.3.1)

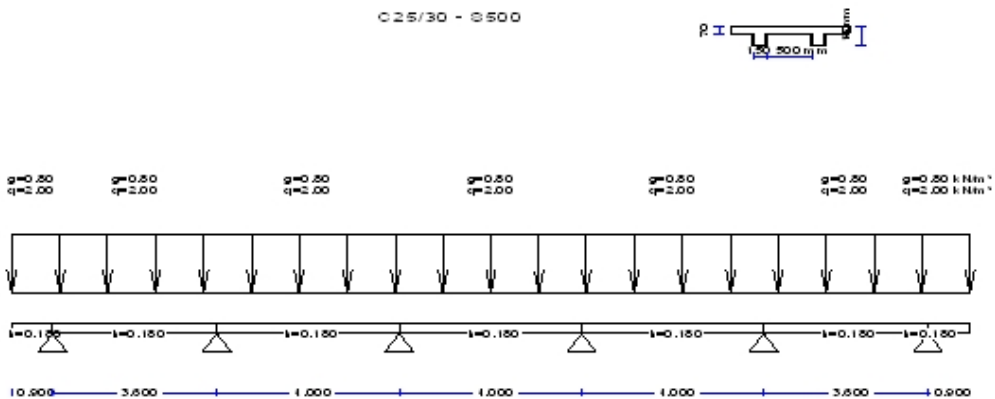
minimum principal reinforcement 1Ø10/65.0 (1.21 cm²/m)

Main slab reinforcement 2Ø12/65.0 (3.48 cm²/m)

8. SLAB-008

One-way continuous ribbed slab

(EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002)

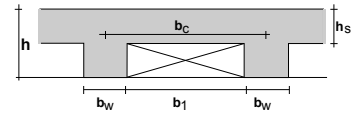


Concrete-Steel class: C25/30-S500 (EC2 §3)
 Concrete cover : Cnom=15 mm (EC2 §4.4.1)
 Concrete weight : 25.0 kN/m³
 yc=1.50, ys=1.15 (EC2 Table 2.1N)



8.1. Dimensions and loads

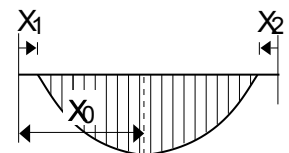
Continuous slab, number of spans=5, transverse length Ly=9.00 m
 Partial safety factors for actions : $\gamma_G=1.35, \gamma_Q=1.50$ (EC0 Annex A1)
 Combination of variable actions : $\psi_1=0.60, \psi_2=0.30$
 Thickness of top solid slab hs=0.070 m
 Rib width bw=0.150m, clear distance between ribs bl=0.500m, rib spacing bc=0.650m
 Effective depth of cross section d=h-d1, d1=Cnomc+Ø/2=15+10/2=20mm



Spans (L), thickness (h), loads on spans (g=self weight +dead, q=live)
 Cant-1, L= 0.900 m, h= 0.180 m, $g=(2.38+0.80) \times 1.000 = 3.18 \text{ kN/m}^2$, $q=2.00 \times 1.000 = 2.00 \text{ kN/m}^2$
 Span-1, L= 3.600 m, h= 0.180 m, $g=(2.38+0.80) \times 1.000 = 3.18 \text{ kN/m}^2$, $q=2.00 \times 1.000 = 2.00 \text{ kN/m}^2$
 Span-2, L= 4.000 m, h= 0.180 m, $g=(2.38+0.80) \times 1.000 = 3.18 \text{ kN/m}^2$, $q=2.00 \times 1.000 = 2.00 \text{ kN/m}^2$
 Span-3, L= 4.000 m, h= 0.180 m, $g=(2.38+0.80) \times 1.000 = 3.18 \text{ kN/m}^2$, $q=2.00 \times 1.000 = 2.00 \text{ kN/m}^2$
 Span-4, L= 4.000 m, h= 0.180 m, $g=(2.38+0.80) \times 1.000 = 3.18 \text{ kN/m}^2$, $q=2.00 \times 1.000 = 2.00 \text{ kN/m}^2$
 Span-5, L= 3.600 m, h= 0.180 m, $g=(2.38+0.80) \times 1.000 = 3.18 \text{ kN/m}^2$, $q=2.00 \times 1.000 = 2.00 \text{ kN/m}^2$
 Cant-2, L= 0.900 m, h= 0.180 m, $g=(2.38+0.80) \times 1.000 = 3.18 \text{ kN/m}^2$, $q=2.00 \times 1.000 = 2.00 \text{ kN/m}^2$

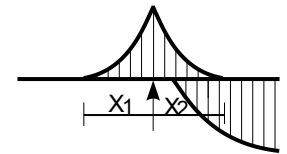
8.2. Shearing forces and bending moments

Maximum bending moments at spans for load combinations 1.35g+1.50q
 Cant-1, Msd= -2.95 kNm/m, xo=0.900 m, x1=0.000m, x2=0.000m
 Span-1, Msd= 7.40 kNm/m, xo=1.544 m, x1=0.119m, x2=0.632m
 Span-2, Msd= 6.72 kNm/m, xo=2.072 m, x1=0.714m, x2=0.570m
 Span-3, Msd= 7.58 kNm/m, xo=2.000 m, x1=0.558m, x2=0.558m
 Span-4, Msd= 6.72 kNm/m, xo=1.928 m, x1=0.570m, x2=0.714m
 Span-5, Msd= 7.40 kNm/m, xo=2.056 m, x1=0.632m, x2=0.119m
 Cant-2, Msd= -2.95 kNm/m, xo=0.000 m, x1=0.000m, x2=0.000m



Maximum bending moments at supports for load combinations 1.35g+1.50q

Support-0, Msd= -2.95 kNm/m, x1=0.900 m, x2=0.295 m
 Support-1, Msd= -12.17 kNm/m, x1=0.977 m, x2=1.002 m
 Support-2, Msd= -10.51 kNm/m, x1=0.900 m, x2=0.856 m
 Support-3, Msd= -10.51 kNm/m, x1=0.856 m, x2=0.900 m
 Support-4, Msd= -12.17 kNm/m, x1=1.002 m, x2=0.977 m
 Support-5, Msd= -2.95 kNm/m, x1=0.295 m, x2=0.900 m



Maximum shear forces for load combinations 1.35g+1.50q

Cant-1, Vsd,left= 0.00 kN/m, Vsd,right= -6.56 kN/m
 Span-1, Vsd,left= 10.23 kN/m, Vsd,right= -16.03 kN/m
 Span-2, Vsd,left= 14.22 kN/m, Vsd,right= -14.96 kN/m
 Span-3, Vsd,left= 13.78 kN/m, Vsd,right= -15.39 kN/m
 Span-4, Vsd,left= 13.37 kN/m, Vsd,right= -15.80 kN/m
 Span-5, Vsd,left= 15.17 kN/m, Vsd,right= -11.09 kN/m
 Cant-2, Vsd,left= 6.56 kN/m, Vsd,right= 0.00 kN/m

Maximum reactions due to dead and live loads (Rg and Rq)

Support-0, Rg(x1.35)= 10.07 kN/m, Rq(x1.50)= 7.58 kN/m
 Support-1, Rg(x1.35)= 18.28 kN/m, Rq(x1.50)= 13.55 kN/m
 Support-2, Rg(x1.35)= 16.73 kN/m, Rq(x1.50)= 13.62 kN/m
 Support-3, Rg(x1.35)= 16.73 kN/m, Rq(x1.50)= 13.62 kN/m
 Support-4, Rg(x1.35)= 18.28 kN/m, Rq(x1.50)= 13.55 kN/m
 Support-5, Rg(x1.35)= 10.07 kN/m, Rq(x1.50)= 7.58 kN/m

8.3. Design actions, shearing forces and bending moments

Design action values after moment redistribution by 0%

(EC2 §5.5)

Reduction of support moments to moments at support faces (bsup=0.20 m)

(EC2 §5.3.2.2.3)

Check for minimum values, (0.65ql²/8 or 0.65ql²/12)

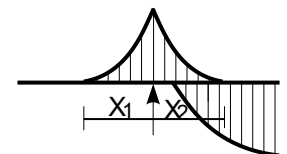
(EC2 §5.3.2.2.3N)

Maximum span bending moments and shear forces for load combinations 1.35g+1.50q

Cant-1, Msd= -2.30 kNm/m, Vsd,left= 0.00 kN/m, Vsd,right= -6.56 kN/m
 Span-1, Msd= 7.40 kNm/m, Vsd,left= 11.26 kN/m, Vsd,right= -15.00 kN/m
 Span-2, Msd= 6.72 kNm/m, Vsd,left= 15.11 kN/m, Vsd,right= -14.06 kN/m
 Span-3, Msd= 7.58 kNm/m, Vsd,left= 14.59 kN/m, Vsd,right= -14.59 kN/m
 Span-4, Msd= 6.72 kNm/m, Vsd,left= 14.06 kN/m, Vsd,right= -15.11 kN/m
 Span-5, Msd= 7.40 kNm/m, Vsd,left= 15.00 kN/m, Vsd,right= -11.26 kN/m
 Cant-2, Msd= -2.30 kNm/m, Vsd,left= 6.56 kN/m, Vsd,right= 0.00 kN/m

Maximum bending moments at supports for load combinations 1.35g+1.50q

Support-0, Msd= -2.30 kNm/m, x1=0.900 m, x2=0.295 m
 Support-1, Msd= -10.67 kNm/m, x1=0.977 m, x2=1.002 m
 Support-2, Msd= -9.10 kNm/m, x1=0.900 m, x2=0.856 m
 Support-3, Msd= -9.10 kNm/m, x1=0.856 m, x2=0.900 m
 Support-4, Msd= -10.67 kNm/m, x1=1.002 m, x2=0.977 m
 Support-5, Msd= -2.30 kNm/m, x1=0.295 m, x2=0.900 m



8.4. Ultimate limit state, design for bending

(EC2 EN1992-1-1:2004, §6.1, §9.3.1)

Reinforcement of spans

Msd1= 7.40kNm/m, d=160mm, Kd=5.88 x/d=0.05 εc/εs=1.0/20.0 ks=2.34, **As= 1.08cm²/m**
 x=0.05x160= 8mm<= 70mm=hs, neutral axis within the depth of top flange
 Msd2= 6.72kNm/m, d=160mm, Kd=6.17 x/d=0.05 εc/εs=1.0/20.0 ks=2.34, **As= 0.98cm²/m**
 x=0.05x160= 8mm<= 70mm=hs, neutral axis within the depth of top flange
 Msd3= 7.58kNm/m, d=160mm, Kd=5.81 x/d=0.05 εc/εs=1.0/20.0 ks=2.34, **As= 1.11cm²/m**
 x=0.05x160= 8mm<= 70mm=hs, neutral axis within the depth of top flange
 Msd4= 6.72kNm/m, d=160mm, Kd=6.17 x/d=0.05 εc/εs=1.0/20.0 ks=2.34, **As= 0.98cm²/m**
 x=0.05x160= 8mm<= 70mm=hs, neutral axis within the depth of top flange
 Msd5= 7.40kNm/m, d=160mm, Kd=5.88 x/d=0.05 εc/εs=1.0/20.0 ks=2.34, **As= 1.08cm²/m**
 x=0.05x160= 8mm<= 70mm=hs, neutral axis within the depth of top flange

Reinforcement over supports

Msd0= -2.30kNm/m, d=160mm, Kd=10.56 x/d=0.03 $\epsilon_c/\epsilon_s=0.5/20.0$ ks=2.32,	As= 0.33cm²/m
Msd1=-10.67kNm/m, d=160mm, Kd=4.90 x/d=0.06 $\epsilon_c/\epsilon_s=1.3/20.0$ ks=2.35,	As= 1.57cm²/m
Msd2= -9.10kNm/m, d=160mm, Kd=5.30 x/d=0.05 $\epsilon_c/\epsilon_s=1.2/20.0$ ks=2.34,	As= 1.33cm²/m
Msd3= -9.10kNm/m, d=160mm, Kd=5.30 x/d=0.05 $\epsilon_c/\epsilon_s=1.2/20.0$ ks=2.34,	As= 1.33cm²/m
Msd4=-10.67kNm/m, d=160mm, Kd=4.90 x/d=0.06 $\epsilon_c/\epsilon_s=1.3/20.0$ ks=2.35,	As= 1.57cm²/m
Msd5= -2.30kNm/m, d=160mm, Kd=10.56 x/d=0.03 $\epsilon_c/\epsilon_s=0.5/20.0$ ks=2.32,	As= 0.33cm²/m

8.5. Minimum reinforcement at spans

(EC2 EN1992-1-1:2004, §9.3.1)

Span-1, $A_s \geq 0.26bd \cdot F_{ctm}/f_{yk}$ ($A_s = 0.50\text{cm}^2/\text{m}$) minimum reinforcement 1Ø10/65.0 (1.21cm²/m)
 Span-2, $A_s \geq 0.26bd \cdot F_{ctm}/f_{yk}$ ($A_s = 0.50\text{cm}^2/\text{m}$) minimum reinforcement 1Ø10/65.0 (1.21cm²/m)
 Span-3, $A_s \geq 0.26bd \cdot F_{ctm}/f_{yk}$ ($A_s = 0.50\text{cm}^2/\text{m}$) minimum reinforcement 1Ø10/65.0 (1.21cm²/m)
 Span-4, $A_s \geq 0.26bd \cdot F_{ctm}/f_{yk}$ ($A_s = 0.50\text{cm}^2/\text{m}$) minimum reinforcement 1Ø10/65.0 (1.21cm²/m)
 Span-5, $A_s \geq 0.26bd \cdot F_{ctm}/f_{yk}$ ($A_s = 0.50\text{cm}^2/\text{m}$) minimum reinforcement 1Ø10/65.0 (1.21cm²/m)

8.6. Serviceability limit state, deflection control

(EC2 EN1992-1-1:2004, §7.4.2)

Cant-1, K=0.40, $\rho=0.021\%$, L/d= 900/ 160= 5.62 < 8.00	(EC2 T.7.4N)
Span-1, K=1.50, $\rho=0.068\%$, L/d= 3600/ 160=22.50 < 30.00	
Span-2, K=1.50, $\rho=0.061\%$, L/d= 4000/ 160=25.00 < 30.00	
Span-3, K=1.50, $\rho=0.069\%$, L/d= 4000/ 160=25.00 < 30.00	
Span-4, K=1.50, $\rho=0.061\%$, L/d= 4000/ 160=25.00 < 30.00	
Span-5, K=1.50, $\rho=0.068\%$, L/d= 3600/ 160=22.50 < 30.00	
Cant-2, K=0.40, $\rho=0.021\%$, L/d= 900/ 160= 5.62 < 8.00	

8.7. ReinforcementSpan reinforcement

Cant-1	Ø10/36.0 (2.18cm ² /m) principal at top,	Ø8/45.0 (1.12cm ² /m) secondary
Span-1	1Ø12/ 65.0 (1.74cm ² /m) principal at bottom,	2Ø12/180.0 (1.26cm ² /m) secondary
Span-2	1Ø12/ 65.0 (1.74cm ² /m) principal at bottom,	2Ø12/200.0 (1.12cm ² /m) secondary
Span-3	1Ø12/ 65.0 (1.74cm ² /m) principal at bottom,	2Ø12/200.0 (1.12cm ² /m) secondary
Span-4	1Ø12/ 65.0 (1.74cm ² /m) principal at bottom,	2Ø12/200.0 (1.12cm ² /m) secondary
Span-5	1Ø12/ 65.0 (1.74cm ² /m) principal at bottom,	2Ø12/180.0 (1.26cm ² /m) secondary
Cant-2	Ø10/36.0 (2.18cm ² /m) principal at top,	Ø8/45.0 (1.12cm ² /m) secondary

Reinforcement over supports

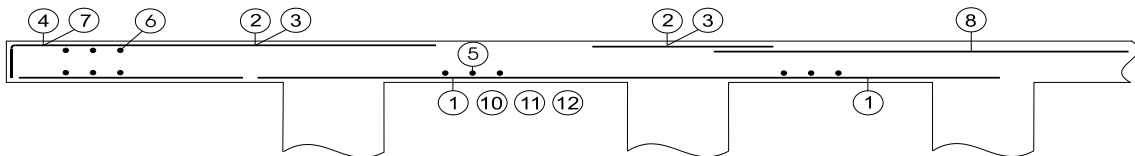
Support-0	Ø10/36.0 (2.18cm ² /m) reinforcement at top
Support-1	Ø10/36.0 (2.18cm ² /m) reinforcement at top
Support-2	Ø10/36.0 (2.18cm ² /m) reinforcement at top
Support-3	Ø10/36.0 (2.18cm ² /m) reinforcement at top
Support-4	Ø10/36.0 (2.18cm ² /m) reinforcement at top
Support-5	Ø10/36.0 (2.18cm ² /m) reinforcement at top

8.8. Reinforcing bar schedule

Num		type	reinforcing bar [mm]	items	∅	g/m [kg/m]	length [m]	weight [kg]
37	(Span-1)	①	4100	14	12	0.888	4.100	50.97
38	(Span-2)	①	4500	14	12	0.888	4.500	55.94
39	(Span-3)	①	4500	14	12	0.888	4.500	55.94
40	(Span-4)	①	4500	14	12	0.888	4.500	55.94
41	(Span-5)	①	4100	14	12	0.888	4.100	50.97
42	(Cant-1)	④	2090	25	10	0.617	2.240	34.55
43	(Supp-1)	②	2560	25	10	0.617	2.560	39.49
44	(Supp-2)	②	2580	25	10	0.617	2.580	39.80
45	(Supp-3)	②	2580	25	10	0.617	2.580	39.80
46	(Supp-4)	②	2560	25	10	0.617	2.560	39.49
47	(Cant-2)	④	2090	25	10	0.617	2.250	34.71
48	(Cant-1)	⑤	9000	2	8	0.395	9.000	7.11
49	(Cant-1)	⑥	9000	2	8	0.395	9.000	7.11
50	(Span-1)	⑤	9000	4	12	0.888	9.000	31.97
51	(Span-2)	⑤	9000	4	12	0.888	9.000	31.97
52	(Span-3)	⑤	9000	4	12	0.888	9.000	31.97
53	(Span-4)	⑤	9000	4	12	0.888	9.000	31.97
54	(Span-5)	⑤	9000	4	12	0.888	9.000	31.97
55	(Cant-2)	⑤	9000	4	8	0.395	9.000	14.22
56	(Cant-2)	⑥	9000	4	8	0.395	9.000	14.22

Total weight [kg]

700.11

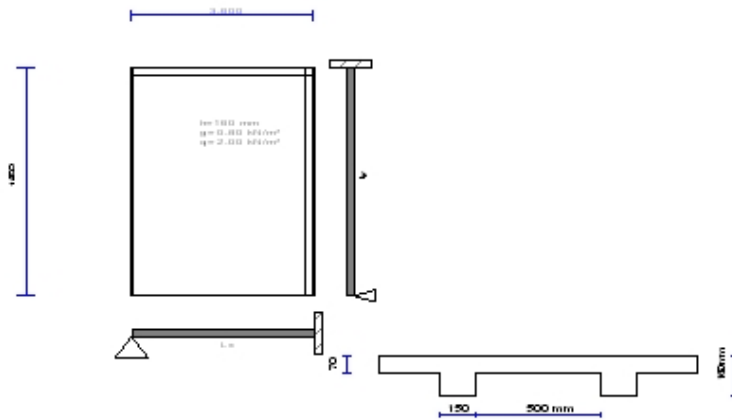


9. SLAB-009

Two-way ribbed slab

(EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002)

C25/30 - S500



Concrete-Steel class: C25/30-S500 (EC2 §3)
 Concrete cover : Cnom=15 mm (EC2 §4.4.1)
 Concrete weight : 25.0 kN/m³
 $\gamma_c=1.50$, $\gamma_s=1.15$ (EC2 Table 2.1N)



9.1. Dimensions and loads

Slab thickness $h=0.160$ m, Spans $L_x=3.600$ m, $L_y=4.500$ m

Thickness of top solid slab $h_s=0.070$ m

Rib width $b_w=0.150$ m, clear distance between ribs $b_1=0.500$ m, rib spacing $b_c=0.650$ m

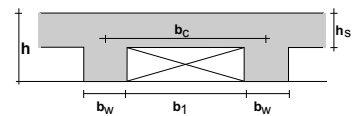
Slab loads: dead $g=(2.67+0.80)=3.47$ kN/m², live $q=2.00$ kN/m²

Partial safety factors for actions : $\gamma_G=1.35$, $\gamma_Q=1.50$

(EC0 Annex A1)

Combination of variable actions : $\psi_1=0.60$, $\psi_2=0.30$

Effective depth of cross section $d=h-d_1$, $d_1=Cnom_c+\varnothing/2=15+10/2=20$ mm, $d=160-20=140$ mm



Method of analysis: Czerny F., "Tafeln für vierseitig und dreiseitig gelagerte Rechteckplatten", Beton Kalender 1983, Berlin, Ernst Sohn, 1983

$L_y/L_x=4.500/3.600=1.25$, Table 2.2.4

9.2. Ultimate limit state, design for bending

(EC2 EN1992-1-1:2004, §6.1, §9.3.1)

9.2.1. Direction of slab analysis x-x, $L_x=3.60$ m

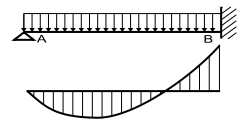
Moment at support $M_{sd\sup A}=0$ kNm/m

Moment at support $M_{sd\sup B}=(1.35 \times 3.47 + 1.50 \times 2.00) \times 3.600^2 / 11.10 = -8.97$ kNm/m

Moment at span $M_{sd\text{span}}=(1.35 \times 3.47 + 1.50 \times 2.00) \times 3.600^2 / 28.00 = 3.56$ kNm/m

Reactions dead, $V_{gA}=3.47 \times 3.600 / 2.53 = 4.94$ $V_{gB}=3.47 \times 3.600 / 1.72 = 7.26$ kN/m

Reactions live, $V_{qA}=2.00 \times 3.600 / 2.53 = 2.85$ $V_{qB}=2.00 \times 3.600 / 1.72 = 4.19$ kN/m



9.2.2. Direction of slab analysis y-y, $L_y=4.50$ m

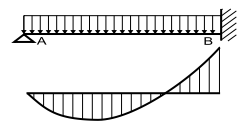
Moment at support $M_{sd\sup A}=0$ kNm/m

Moment at support $M_{sd\sup B}=(1.35 \times 3.47 + 1.50 \times 2.00) \times 3.600^2 / 12.90 = -7.72$ kNm/m

Moment at span $M_{sd\text{span}}=(1.35 \times 3.47 + 1.50 \times 2.00) \times 3.600^2 / 45.60 = 2.18$ kNm/m

Reactions dead, $V_{gA}=3.47 \times 3.600 / 2.56 = 4.88$ $V_{gB}=3.47 \times 3.600 / 1.86 = 6.71$ kN/m

Reactions live, $V_{qA}=2.00 \times 3.600 / 2.56 = 2.81$ $V_{qB}=2.00 \times 3.600 / 1.86 = 3.87$ kN/m



9.3. Ultimate limit state, design for bending

(EC2 EN1992-1-1:2004, §6.1, §9.3.1)

Msd= 3.56kNm/m, d=140mm, Kd=7.42 x/d=0.04 $\epsilon_c/\epsilon_s=0.8/20.0$ ks=2.33, **As= 0.59cm²/m**
 x=0.04x140= 6mm<= 70mm=hs, neutral axis within the depth of top flange
 Msd= 2.18kNm/m, d=130mm, Kd=8.80 x/d=0.03 $\epsilon_c/\epsilon_s=0.7/20.0$ ks=2.32, **As= 0.39cm²/m**
 x=0.03x130= 4mm<= 70mm=hs, neutral axis within the depth of top flange
 Msd= -8.97kNm/m, d=140mm, Kd=4.67 x/d=0.06 $\epsilon_c/\epsilon_s=1.3/20.0$ ks=2.35, **As= 1.51cm²/m**
 Msd= -7.72kNm/m, d=140mm, Kd=5.04 x/d=0.06 $\epsilon_c/\epsilon_s=1.2/20.0$ ks=2.35, **As= 1.29cm²/m**

Minimum slab reinforcement, As>=0.26bd·Fctm/fyk (As= 0.44cm²/m) (EC2 §9.3.1)

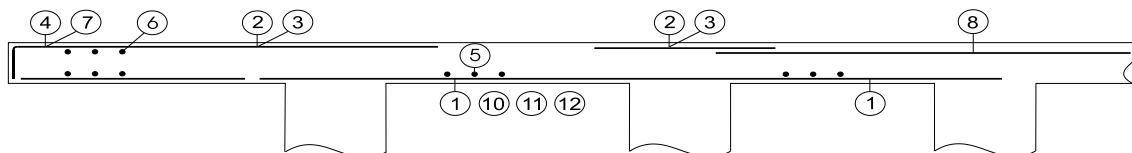
minimum principal reinforcement 1Ø10/65.0 (1.21cm²/m)
 span/eff. depth, K=1.30, $\rho=0.042\%$, L/d= 3600/ 140=25.71<26.00 (EC2 T.7.4N)

Span reinforcement: **x-x** 1Ø12/65.0 (1.74cm²/m), (bottom layer)
y-y 1Ø12/65.0 (1.74cm²/m)
Reinforcement over supports: **Left** Ø8/45.0 (1.12cm²/m)
Right Ø8/33.0 (1.52cm²/m)
Bottom Ø8/45.0 (1.12cm²/m)
Top Ø8/38.5 (1.31cm²/m)

9.4. Reinforcing bar schedule

Num	type	reinforcing bar [mm]	items	Ø	g/m [kg/m]	length [m]	weight [kg]
57	①	4100	7	12	0.888	4.100	25.49
58	①	5000	6	12	0.888	5.000	26.64
59	②	2260	10	8	0.395	2.260	8.93
60	②	2260	14	8	0.395	2.260	12.50
61	②	2710	8	8	0.395	2.710	8.56
62	②	2710	9	8	0.395	2.710	9.63

Total weight [kg] 91.75



10. SLAB-010

Moment capacity of slab section

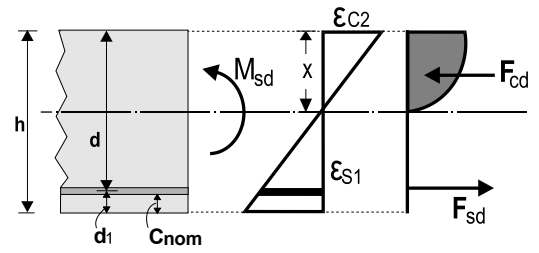
(EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002)

$h=0.180$ m, $\varnothing10/25.0$ ($3.14\text{cm}^2/\text{m}$)

Concrete-Steel class: C25/30-S500 (EC2 §3)

Concrete cover : $C_{nom}=15$ mm (EC2 §4.4.1)

$\gamma_c=1.50$, $\gamma_s=1.15$ (EC2 Table 2.1N)



10.1. Dimensions and loads

Slab thickness 0.180 m, reinforcement $\varnothing10/25.0$ ($3.14\text{cm}^2/\text{m}$)

Effective depth of cross section $d=h-d_1$, $d_1=C_{nom}c+\varnothing/2=15+10/2=20\text{mm}$, $d=180-20=160\text{mm}$

10.2. Cross section moment capacity

(EC2 EN1992-1-1:2004, §6.1)

(iterations:3). From internal force equilibrium we have:

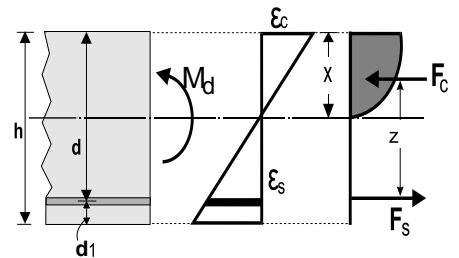
$\epsilon_c=2.00$ (o/oo), $F_c=\alpha\cdot0.85f_{cd}\cdot b\cdot x$, $\alpha=0.667$, $x=14.5\text{mm}$, $x/d=0.09$

$F_c= -\alpha\cdot0.85f_{cd}\cdot b\cdot x = 0.001\times0.667\times0.85\times16.67\times1000\times 14.5= -137\text{kN}$

$\epsilon_s=20.00$ (o/oo) $>2.17=\epsilon_y$, $F_s=A_s\cdot f_{yd}= 0.001\times 314\times435.0 = 137\text{kN}$

$z=d-K_a\cdot x$, $K_a=0.375$, $z=160-0.375\times14.46=155\text{mm}$

Moment capacity of cross section $M_d=z\cdot F_s=0.155\times137= 21.24\text{kNm}$



Ultimate moment capacity of slab cross section $M_d= 21.24$ kNm/m

11. SLAB-011

Moment capacity of slab section with FRP strengthening

(EC2 EN1992-1-1:2004, EC0 EN1990-1-1:2002)

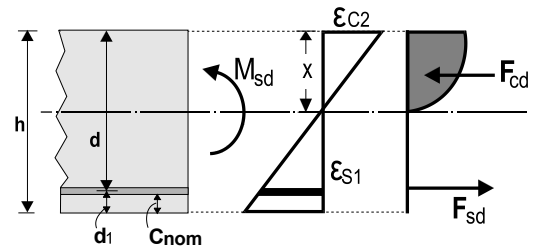
$h=0.180$ m, $\varnothing 10/25.0$ (3.14cm²/m)

FRP+epoxy, $t(\text{FRP})= 1.00$ mm

Concrete-Steel class: C25/30-S500 (EC2 §3)

Concrete cover : $C_{nom}=15$ mm (EC2 §4.4.1)

$\gamma_c=1.50$, $\gamma_s=1.15$ (EC2 Table 2.1N)



11.1. Dimensions and loads

Slab thickness 0.180 m, reinforcement $\varnothing 10/25.0$ (3.14cm²/m)

Effective depth of cross section $d=h-d_1$, $d_1=C_{nom}c+\varnothing/2=15+10/2=20$ mm, $d=180-20=160$ mm

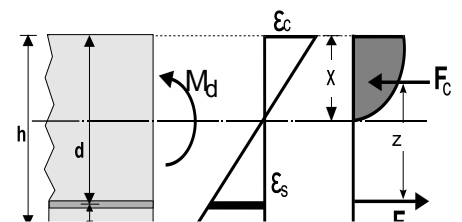
Fibre Reinforced Polymer material (FRP)

- Characteristic name : FRP+epoxy
- Total thickness : 1.00 mm
- Modulus of elasticity : 100 GPa
- Tensile strength : 1000 MPa
- Cross section area : $1000 \times 1.00 = 1000$ mm²

11.2. Cross section moment capacity, without FRP strengthening

(EC2 EN1992-1-1:2004, §6.1)

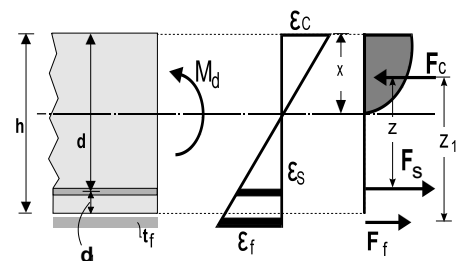
(iterations:3). From internal force equilibrium we have:
 $\epsilon_c=2.00$ (o/oo), $F_c=\alpha \cdot 0.85 f_{cd} \cdot b \cdot x$, $\alpha=0.667$, $x=14.5$ mm, $x/d=0.09$
 $F_c = -\alpha \cdot 0.85 f_{cd} \cdot b \cdot x = 0.001 \times 0.667 \times 0.85 \times 16.67 \times 1000 \times 14.5 = -137$ kN
 $\epsilon_s=20.00$ (o/oo) $> 2.17 = \epsilon_y$, $F_s = A_s \cdot f_{yd} = 0.001 \times 314 \times 435.0 = 137$ kN
 $z = d - K_a \cdot x$, $K_a = 0.375$, $z = 160 - 0.375 \times 14.46 = 155$ mm
 Moment capacity of cross section $M_d = z \cdot F_s = 0.155 \times 137 = 21.24$ kNm



11.3. Cross section moment capacity, with FRP strengthening



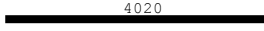
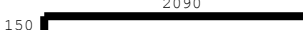
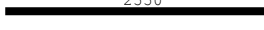
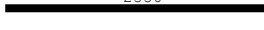



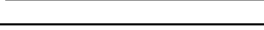
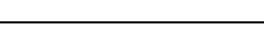
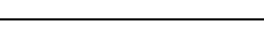

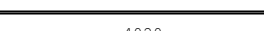
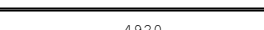
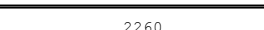
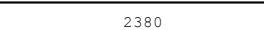


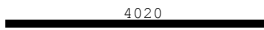
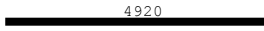
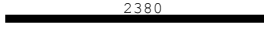
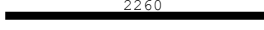
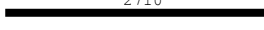
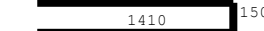


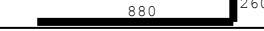
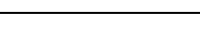
(EC2 EN1992-1-1:2004, §6.1)

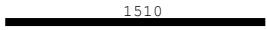
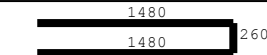
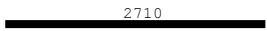
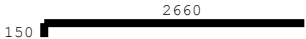
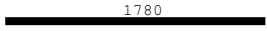
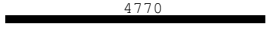
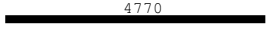
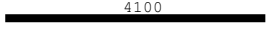


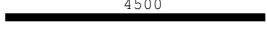
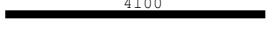
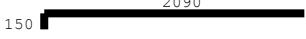
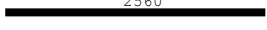
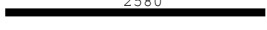
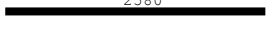
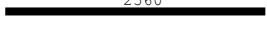
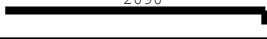
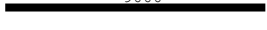












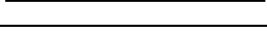

(iterations:5). From internal force equilibrium we have:
 initial deformation of bottom face $\epsilon_{fo}=0.00$ (o/oo)
 $\epsilon_c=3.50$ (o/oo), $F_c=\alpha \cdot 0.85 f_{cd} \cdot b \cdot x$, $\alpha=0.810$, $x=65.5$ mm, $x/d=0.41$
 $F_c = -\alpha \cdot 0.85 f_{cd} \cdot b \cdot x = 0.001 \times 0.810 \times 0.85 \times 16.67 \times 1000 \times 65.5 = -751$ kN
 $\epsilon_s = 5.05$ (o/oo) $> 2.17 = \epsilon_y$, $F_s = A_s \cdot f_{yd} = 0.001 \times 314 \times 435.0 = 137$ kN
 $\epsilon_f + \epsilon_{fo} = 6.15$ (o/oo), $\epsilon_f = 6.15$, $\sigma_f = E_f \cdot \epsilon_f = 100 \times 6.15 = 615$ MPa
 $\sigma_f = 615$ MPa < 1000 (tensile strength) $F_f = A_f \cdot \sigma_f = 1000 \times 615 = 615$ kN
 $z = d - K_a \cdot x$, $K_a = 0.416$, $z = 160 - 0.416 \times 65.48 = 133$ mm
 $z_1 = (z \cdot F_s + (z + d_1 + t_f/2) \cdot F_f) / (F_s + F_f) = (133 \times 137 + 153 \times 615) / (137 + 615) = 150$ mm
 Moment capacity of cross section $M_d = z_1 \cdot (F_s + F_f) = 0.150 \times (137 + 615) = 112.80$ kNm



Ultimate moment capacity of slab cross section $M_d = 112.80$ kNm/m

Reinforcing bar schedule

Num	Structure object	type	reinforcing bar [mm]	items	∅	g/m [kg/m]	length [m]	weight [kg]
1	SLAB-002 (Span-1)	P1		25	10	0.617	4.020	62.01
2	SLAB-002 (Span-2)	P1		25	10	0.617	4.020	62.01
3	SLAB-002 (Span-3)	P1		25	10	0.617	4.020	62.01
4	SLAB-002 (Cant-1)	P4		25	10	0.617	2.240	34.55
5	SLAB-002 (Supp-1)	P2		25	10	0.617	2.550	39.33
6	SLAB-002 (Supp-2)	P2		25	10	0.617	2.550	39.33
7	SLAB-002 (Cant-2)	P4		25	10	0.617	2.250	34.71
8	SLAB-002 (Cant-1)	P5		2	8	0.395	9.000	7.11
9	SLAB-002 (Cant-1)	P6		2	8	0.395	9.000	7.11
10	SLAB-002 (Span-1)	P5		8	8	0.395	9.000	28.44
11	SLAB-002 (Span-2)	P5		8	8	0.395	9.000	28.44
12	SLAB-002 (Span-3)	P5		8	8	0.395	9.000	28.44
13	SLAB-002 (Cant-2)	P5		2	8	0.395	9.000	7.11
14	SLAB-002 (Cant-2)	P6		2	8	0.395	9.000	7.11
15	SLAB-003	P1		12	10	0.617	4.020	29.76
16	SLAB-003	P1		10	10	0.617	4.920	30.36
17	SLAB-003	P2		10	8	0.395	2.260	8.93
18	SLAB-003	P2		12	10	0.617	2.380	17.62
19	SLAB-003	P2		8	8	0.395	2.710	8.56
20	SLAB-003	P2		10	10	0.617	2.830	17.46
21	SLAB-004	P1		12	10	0.617	4.020	29.76
22	SLAB-004	P1		10	10	0.617	4.920	30.36
23	SLAB-004	P2		14	10	0.617	2.380	20.56
24	SLAB-004	P2		10	8	0.395	2.260	8.93
25	SLAB-004	P2		8	8	0.395	2.710	8.56
26	SLAB-004	P9		10	10	0.617	2.970	18.32
27	SLAB-005	P1		15	12	0.888	2.600	34.63
28	SLAB-005	P1		7	12	0.888	5.000	31.08
29	SLAB-005	P9		15	12	0.888	2.020	26.91

30	SLAB-005	(P2)		10	8	0.395	2.650	10.47
31	SLAB-005	(P9)		7	12	0.888	3.220	20.02
32	SLAB-005	(P2)		5	8	0.395	4.450	8.79
33	SLAB-006	(P4)		7	10	0.617	2.810	12.14
34	SLAB-006	(P2)		7	10	0.617	1.780	7.69
35	SLAB-006	(P5)		3	8	0.395	4.770	5.65
36	SLAB-006	(P6)		3	8	0.395	4.770	5.65
37	SLAB-008 (Span-1)	(P1)		14	12	0.888	4.100	50.97
38	SLAB-008 (Span-2)	(P1)		14	12	0.888	4.500	55.94
39	SLAB-008 (Span-3)	(P1)		14	12	0.888	4.500	55.94
40	SLAB-008 (Span-4)	(P1)		14	12	0.888	4.500	55.94
41	SLAB-008 (Span-5)	(P1)		14	12	0.888	4.100	50.97
42	SLAB-008 (Cant-1)	(P4)		25	10	0.617	2.240	34.55
43	SLAB-008 (Supp-1)	(P2)		25	10	0.617	2.560	39.49
44	SLAB-008 (Supp-2)	(P2)		25	10	0.617	2.580	39.80
45	SLAB-008 (Supp-3)	(P2)		25	10	0.617	2.580	39.80
46	SLAB-008 (Supp-4)	(P2)		25	10	0.617	2.560	39.49
47	SLAB-008 (Cant-2)	(P4)		25	10	0.617	2.250	34.71
48	SLAB-008 (Cant-1)	(P5)		2	8	0.395	9.000	7.11
49	SLAB-008 (Cant-1)	(P6)		2	8	0.395	9.000	7.11
50	SLAB-008 (Span-1)	(P5)		4	12	0.888	9.000	31.97
51	SLAB-008 (Span-2)	(P5)		4	12	0.888	9.000	31.97
52	SLAB-008 (Span-3)	(P5)		4	12	0.888	9.000	31.97
53	SLAB-008 (Span-4)	(P5)		4	12	0.888	9.000	31.97
54	SLAB-008 (Span-5)	(P5)		4	12	0.888	9.000	31.97
55	SLAB-008 (Cant-2)	(P5)		4	8	0.395	9.000	14.22
56	SLAB-008 (Cant-2)	(P6)		4	8	0.395	9.000	14.22
57	SLAB-009	(P1)		7	12	0.888	4.100	25.49
58	SLAB-009	(P1)		6	12	0.888	5.000	26.64
59	SLAB-009	(P2)		10	8	0.395	2.260	8.93
60	SLAB-009	(P2)		14	8	0.395	2.260	12.50
61	SLAB-009	(P2)		8	8	0.395	2.710	8.56
62	SLAB-009	(P2)		9	8	0.395	2.710	9.63

Total weight [kg]	1631.78
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slab name	h [cm]	Lx [m]	Ly [m]	span reinforcement		support reinforcement				
				x-x	y-y	□	□	□	□	
SLAB-002 (Cant1)	□	18.0	0.90	9.00						
SLAB-002 (1)	□	18.0	3.60	9.00	∅10/36.0_	∅8/45.0				
SLAB-002 (1)	□	18.0	3.60	9.00	∅8/45.0					
SLAB-002 (2)	□	18.0	3.60	9.00	∅10/36.0_	∅8/45.0		∅10/36.0		
SLAB-002 (2)	□	18.0	3.60	9.00	∅10/36.0					
SLAB-002 (3)	□	18.0	3.60	9.00			∅10/36.0	∅8/45.0		
SLAB-002 (3)	□	18.0	3.60	9.00	∅8/45.0					
SLAB-002 (Cant2)	□	18.0	0.90	9.00			∅8/45.0			
SLAB-003	□	18.0	3.60	4.50	∅10/36.0_	∅10/36.0	∅8/45.0	∅10/36.0	∅8/45.0	∅10/36.0
SLAB-004	□	18.0	3.60	4.50	∅10/38.5	∅10/38.5_	∅8/45.0	∅8/45.0	∅10/20.0	∅8/45.0
SLAB-006	□	18.0	1.20	4.80	∅10/36.0^	∅8/45.0:		∅10/36.0		
SLAB-008 (Cant1)	□	18.0	0.90	9.00				1∅12/65.		
SLAB-008 (1)	□	18.0	3.60	9.00	1∅12/65.0_	2∅12/180.0	1∅12/65.	2∅12/180		
SLAB-008 (2)	□	18.0	4.00	9.00	1∅12/65.0_	2∅12/180.0	2∅12/180			
SLAB-008 (2)	□	18.0	4.00	9.00	1∅12/65.0_					
SLAB-008 (3)	□	18.0	4.00	9.00						
SLAB-008 (3)	□	18.0	4.00	9.00	2∅12/180.0					
SLAB-008 (4)	□	18.0	4.00	9.00						
SLAB-008 (4)	□	18.0	4.00	9.00	1∅12/65.0_					
SLAB-008 (5)	□	18.0	3.60	9.00	∅8/45.0	∅10/36.0				
SLAB-008 (5)	□	18.0	3.60	9.00	2∅12/180.0					
SLAB-008 (Cant2)	□	18.0	0.90	9.00						
SLAB-009	□	16.0	3.60	4.50	1∅12/65.0_	1∅12/65.0	∅8/45.0	∅8/31.5	∅8/45.0	∅8/36.5

(_=bottom layer of reinforcement, ^=span reinforcement at top, :=reinforcement at top and